

Gr- 125 -
GRADED BOOK

PASTY

FIELD BOOK

No. 385

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C. Tolson
6/28/27

Grade Stakes - Alley Blk. 223
SPL & TCo. bet. Sampson & Sicard

	745	88.02		80.57	Sicard Tolman	
+00 T.C. W			4.39	83.63	83.40	Cut 0.23 ✓
+00 T.C. E			3.97	84.05	83.6	Cut 0.45 ✓
+50 E			4.72	83.30	82.92	Cut 0.38 ✓
+50 W			5.20	82.82	82.75	Cut 0.07 ✓
+100 W			6.30	81.72	82.11	Fill 0.39 ✓
+100 E			5.06	82.96	82.25	Cut 0.71 ✓
+150 E			5.55	82.47	81.57	Cut 0.90 ✓
+150 W			5.78	82.24	81.46	Cut 0.78 ✓
+200 W			7.11	80.91	80.81	Cut 0.10 ✓
+200 E			6.48	81.54	80.90	Cut 0.64 ✓
TP	4.34	85.02	7.34	80.68		
+250 E			4.22	80.80	80.22	Cut 0.58 ✓
+250 W			3.47	81.53	80.17	Cut 1.36 ✓
+300 W			5.79	79.23	79.52	Fill 0.29 ✓
+300 E			4.69	80.33	79.54	Cut 0.79 ✓
T.P.	3.93	82.57	6.38	78.64		
+340 E			3.33	79.24	79.00	Cut 0.24 ✓
+340 W			3.50	79.07	79.00	Cut 0.07 ✓
+400 W			4.02	78.55	78.40	Cut 0.15 ✓
+400 E			3.44	79.13	78.40	Cut 0.73 ✓
+460 E			4.32	78.25	77.80	Cut 0.45 ✓
+460 W			4.45	78.12	77.80	Cut 0.32 ✓
+500 W			4.46	78.11	76.94	Cut 1.17 ✓
+500 E			4.02	78.55	77.0	Cut 1.55 ✓

77.80
76.80

1.00

76.94
75.80

1.14

84.57

+550E			6.74	75.83	76.0	F 0.17 ✓
+550W			6.56	76.01	75.87	C 0.14 ✓
+600 TCH			7.51	75.06	74.80	C 0.26 ✓
+600 TcbE			7.32	75.25	75.0	C 0.25 ✓
TP	4.14	79.01	7.70	74.87		
	9.92	82.96	5.97	73.24		
			2.39	80.57	80.57 ✓	

Grade Stakes - Alley 45 Sherman's
22nd + 24th K + L

	11.30	87.25		75.95	22 + L NE	
T26						
S.L			0.30	86.95		
TP	10.85	97.80	93	86.95		
+40 S			5.95	91.85	90.40	Cut 1.45
+40 N			2.50	95.30	91.60	Cut 3.70
+60 N			2.74	95.06	92.90	Cut 2.16
+60 S			5.81	91.99	91.80	Cut 0.19
+80 S			5.56	92.24	92.40	Fill 0.16
+80 N			2.85	94.95	93.40	Cut 1.55
+100 N			3.17	94.63	93.20	Cut 1.43
TP	062	95.25	3.17	94.63		
+100 S			3.14	92.11	92.2	Fill 0.09
+140 S			2.82	92.43	91.2	Cut 1.23
+120 N			1.05	94.20	92.10	Cut 2.10
+150 N			1.73	93.52	89.94	Cut 3.58
+150 S			5.54	89.71	89.03	Cut 0.68
+200 S			8.54	86.71	85.41	Cut 1.30
+200 N			7.23	88.02	86.34	Cut 1.68
+250 N			11.26	83.99	82.74	Cut 1.25
+250 S			11.52	83.73	81.79	Cut 1.94
TP	0.21	82.70	12.76	82.49		
+300 S			4.51	78.19	78.17	Cut 0.02
+300 N			2.98	79.72	79.14	Cut 0.58
+330 N			5.63	77.07	77.00	Cut 0.07
+330 S			7.62	75.08	76.00	Fill 0.92

82.70

+350 N			6.23	76.47	75.80	Cut 0.67
+350 S			8.23	74.47	74.92	Fill 0.45
TP	1.51	70.44	10.77	71.93		
			10.57	62.87 = 62.89		

Grade States - Alley Block - 247 - D.H

	Ground	Grade	C or F					
Top Web					+400 W	304.71	303.79	C 0.92 ✓
Cypress	299.77	299.75	0.0		" E	304.33	304.10	C 0.23 ✓
Top Ecb					+450 E	304.97	303.73	C 1.24 ✓
Cypress	299.83	299.83	0.0		" W	304.20	303.44	C 0.80 ✓
+20 E	304.59	301.70	C 2.89		+500 W	303.76	303.09	C 0.67 ✓
" W	305.09	301.70	C 3.39	Reset	" E	303.31	303.36	F 0.05 ✓
+40 W	305.09	303.40	C 1.69	C 1.60	+550 E	303.18	302.99	C 0.19 ✓
" E	304.85	303.40	C 1.45	C 1.15	" W	303.22	302.74	C 0.48 ✓
+60 E	305.40	304.50	C 0.90	C 0.65	+600 W	302.40	302.39	C 0.01 ✓
" W	305.55	304.40	C 1.15		" E	303.14	302.62	C 0.52 ✓
+80 W	305.76	304.90	C 0.86		+640 E	302.93	302.25	C 0.68 ✓
" E	305.54	305.10	C 0.44		" W	302.22	302.10	C 0.12 ✓
+100 E	305.50	305.30	C 0.20		+660 W	302.14	301.90	C 0.22 ✓
" W	305.62	305.10	C 0.52		" E	302.77	302.10	C 0.67 ✓
+150 W	305.34	305.31	C 0.03 ✓		+680 E	303.16	301.70	C 1.46 ✓
" E	305.76	305.66	C 0.10 ✓		" W	302.08	301.50	C 0.58 ✓
+170 E	306.57	305.80	C 0.77 ✓		Top Web	300.88	300.85	0.0
" W	304.71	305.40	F 0.69 ✓		Mythic			
+200 W	304.62	305.19	F 0.57 ✓		" Ecb	301.13	301.25	0.0
" E	306.99	305.58	C 1.41 ✓					
+250 E	305.47	305.21	C 0.26 ✓					
" W	304.39	304.84	F 0.45 ✓					
+300 W	304.77	304.49	C 0.28 ✓					
" E	304.81	304.84	F 0.03 ✓					
+350 E	305.83	304.47	C 1.36 ✓					
" W	304.65	304.14	C 0.51 ✓					

Alley Grades - Block 198 UH

Lincoln = 0+00 Univ = 6+00

	Elev	Grade	Cut	Fill
5+80 E	292.64	291.50	1.14	
" W	91.70	91.20	0.50	
5+60 W	91.81	91.60	0.21	
" E	92.68	91.90	0.78	
5+00 E	92.78	92.36	0.42	
" W	92.11	92.06	0.05	
4+50 W	91.92	92.44		0.52
" E	93.15	92.74	0.41	
4+00 E	94.65	93.13	1.52	
" W	92.36	92.83		0.47
3+50 W	93.51	93.21	0.30	
" E	93.93	93.57	0.42	
3+00 E	94.25	93.89	0.36	
" W	94.40	93.59	0.81	
2+50 W	94.23	93.97	0.26	
" E	94.26	94.27		0.01
2+00 E	94.64	94.50	0.14	
1+50 W	93.96	94.20		0.24
1+00 W	93.94	94.43		0.49
" E	94.72	94.73		0.01
150 E	95.54	95.30	0.24	
" W	95.75	95.00	0.75	
100 W	96.86	95.57	1.29	
" E	96.32	95.87	0.45	

			C	F
70 E	96.58	96.10	0.46	
" W	95.74	95.80		0.06
60 W	96.15	95.70	0.45	
" E	96.68	96.02	0.68	
40 W	95.44	95.40	0.04	
" E	97.07	95.10	1.97	
20 W	94.74	94.00	0.74	
" E	95.58	94.30	1.28	
EL	95.39	92.60	2.79	
YL	94.81	92.30	1.71	

Alley Grades - Block 9, Teralta

0+00 = N 5+71.3 = S

	Elev	Grades	Cut	Fill
0+00 E		372.45		
" W		372.65		
0+60 E	372.70	372.70	0.0	
" W	73.44	73.00	0.44	
1+00 E	72.43	72.37	0.06	
" W	73.40	72.67	0.73	
1+50 E	71.81	71.95		0.14
" W	72.47	72.25	0.22	
2+00 E	71.84	71.53	0.31	
" W	72.47	71.83	0.64	
2+50 E	71.37	71.12	0.25	
" W	71.42	71.42	0.0	
3+00 E	71.15	70.70	0.45	
" W	71.25	71.00	0.25	
3+50 E	70.75	70.08	0.67	
" W	70.62	70.38	0.24	
4+00 E	69.74	69.45	0.29	
" W	69.85	69.75	0.10	
4+50 E	69.76	68.83	0.93	
" W	69.58	69.13	0.45	
5+00 E	68.70	68.20	0.50	
" W	68.57	68.50	0.07	
5+50 E	68.51	66.90	1.61	
" W	67.90	67.20	0.70	
5+71.3 E	66.30	66.35		
" W	66.69	66.65		

Grade Stakes - Trias St. La Jolla to Moore

			Top 6 N of Trias	Book 1189	Cut	Fill
			La Jolla	Moore		
0+0	N Line	5.12	57.95	52.83		
"	12.84 West		5.44	52.51	52.70	0.19 ✓
0+6	22.84 West		5.74	52.21	52.60	0.39 ✓
"	32.84 West		6.17	51.78	52.2	0.42 ✓
1+0	42.84 West		6.54	51.41	51.7	0.29 ✓
"	52.84 West		7.0	50.95	51.0	0.05 ✓
4+50	T.P.	0.07	53.66	4.36	53.59	
"	N Line					
"	50' E Jeff		3.97	49.69	49.43	0.26 ✓
2+0	NE Trias		6.10	47.56	45.5	2.06 ✓
"	Jefferson					
"	SE T+J		5.93	47.73	46.5	1.23 ✓
"	S Line					
2+50	50' B of Jeff		2.21	51.45	50.37	1.08 ✓
"	SW Trias					
"	+ Jeff		9.06	44.60	44.5	0.10 ✓
"	NW Trias					
3+00	Jeff		10.17	43.47	43.5	0.01 ✓
"	H Line					
"	50' N Jeff		12.53	41.13	40.58	0.55 ✓
"	S Line					
3+50	50' N Jeff		12.75	40.91	41.37	0.46 ✓
"	T.P.	0.23	40.82	13.07	40.59	
"	S Line					
4+00	100' N Jeff		2.70	38.12	38.24	0.12 ✓
"	N Line					
"	100' W Jeff		3.54	37.28	37.66	0.38 ✓
"	N Line					
4+50	100' W Jeff		6.22	34.60	34.0	0.60 ✓
"	S Line					
"	100' W Jeff		6.13	34.69	34.5	0.19 ✓
"	S Line					
5+00	200' W Jeff		7.92	32.90	32.64	0.26 ✓
"	N Line					
"	200' W Jeff		6.83	33.99	32.28	1.71 ✓
"	N Line					
5+50	250' W Jeff		10.05	30.77	30.14	0.63 ✓
"	S Line					
"	250' W Jeff		10.28	30.54	30.32	0.22 ✓

Trias St.

TP	3.50	31.73	12.59	28.23
SE corner		4.38	27.35	27.00 ✓
Trias & Moore		7.56	24.17	27.00 ✓
SW corner		5.73	26.00	28.00 ✓
T&M		3.75	27.99	28.00 ✓
NW corner				
T&M				
NE corner				
T&M				

Cut. Fill

✓0.35 ✓	
✓2.83 ✓	
✓2.00 ✓	
✓Grade ✓	

MOORE ST Trias to
Ampudia

W Line		3.56	28.17	28.11 ✓
50' N. Trias				
TP	7.74	35.93	3.56	28.17
E Line		6.69	29.22	29.11 ✓
50' N Trias				
E Line		5.47	30.61	30.00 ✓
90' N Trias				
EL		4.92	31.01	30.4 ✓
110' N				
EL		4.41	31.52	30.70 ✓
130' N				
EL		4.13	31.80	30.60 ✓
150' N				
EL		4.22	31.71	30.80 ✓
170' N				
EL		4.71	31.22	30.60 ✓
190' N				
EL		4.75	31.18	30.40 ✓
210' N				
EL		5.55	30.38	29.78 ✓
250' N				
W.L		7.66	28.27	28.78 ✓
250' N				
W.L		6.50	29.43	29.4 ✓
310' N				
W.L		6.10	29.83	29.6 ✓
190' N				
W.L		6.15	29.78	29.8 ✓
170' N				
W.L		6.10	29.83	29.8 ✓
150' N				
W.L		5.70	30.23	29.7 ✓
130' N				
W.L		5.61	30.32	29.4 ✓
110' N		5.20	30.17	29.0 ✓

✓0.06 ✓	
✓0.11 ✓	
✓0.46 ✓	
✓0.61 ✓	
✓0.82 ✓	
✓1.00 ✓	
✓0.91 ✓	
✓0.62 ✓	
✓0.78 ✓	
✓0.60 ✓	
✓0.51 ✓	
✓0.03 ✓	
✓0.23 ✓	
✓0.02 ✓	
✓0.03 ✓	
✓0.53 ✓	
✓0.92 ✓	
✓1.17 ✓	

Storm Drain Grades - 12+70.6 (PC)
to 15+62.71 (PT) Hensley St. Line

SE Hensley
+K

	7.93	83.95		76.02		Cut
	5.15	86.04	3.06	80.89		
12+70.06	BC		3.93	82.11	72.96	9.15 ✓
12+75.57	± of Curve		5.46	80.58	72.57	8.01 ✓
13+70.54	EC		2.46	83.58	72.18	11.40 ✓
13+50			3.64	82.40	71.71	10.69 ✓
14+00			5.67	80.37	70.73	9.44 ✓
14+50			7.62	78.42	70.15	8.27 ✓
15+00			8.46	77.58	69.37	8.21 ✓
15+13.62	DC		10.62	75.42	69.16	6.26 ✓
	± of curve		8.78	77.26	68.78	8.48 ✓
TP	6.20	83.44	8.80	77.24		
15+62.71	FC		5.31	78.13	68.4	9.73
TP			7.43	76.01	SE Hensley +K	

Flowline grades

Stakes set SE 1/4 of E

Storm Drain Grades $0+00 = \text{Outlet}$
bet 25th & 26, Market + Island

			NEBP 25+T		Cut
	2.06	132.74		130.68	
	5.95	125.60	13.09	119.65	
	1.22	124.16	2.66	122.94	
	4.01	116.25	11.92	112.24	
0+50			5.81	110.44	108.25
1+04	Alley		5.37	110.88	106.08
1+50			9.06	107.19	104.24
2+00			9.71	106.54	102.24
TP	2.56	109.86	8.95	107.30	
2+50			4.86	105.00	100.24
2+95	Island		5.55	104.31	98.44
T.P.	2.28	106.86	5.28	104.58	
3+50			2.71	104.15	96.33
4+00			7.38	99.48	94.23
4+37.00	X		7.73	99.13	92.73
4+87	Alley		7.30	97.56	90.75
TP	5.65	103.57	8.94	97.92	
5+20.54	X		5.95	97.62	89.40
5+50			5.73	97.84	88.56
TP	5.10	102.14	6.53	97.04	
6+00			6.21	95.93	87.13
6+50			4.46	97.68	85.70
P.I. Hub	J St		5.18	96.96	
TP	7.14	107.44	1.84	100.30	
			7.09	99.85	
				99.87	

SEBP
15-2

4.005	4.005	
2.002	100	
	1600	
110.25	4005	
2.0025	436520	130.68
108.485	110.25	2.06 +
4.005	4.17	132.74
104.2425	116.08	13.09 -
2.0025		119.65
104.24	4005	5.95 +
2.0025	90	125.80
100.2375	20025	2.66 -
4.005	36025	122.94
92.2325	380	1.22 +
2.002	102.24	11.92 -
90.2305	38	112.24
	7804	4.01 +
	37.04	116.25
	4005	8.95 -
4005	12520	107.30
87	14816	2.56 +
36025	148345	109.86
32040	94.23	5.28 -
351625	1.48	102.58
14.22	94.75	2.28 +
3.56		106.86
50.67		8.94 -
	487	97.92
	4005	5.65 -
	2425	103.57
	1948	6.53 -
	19.50	77.00
	110.25	5.10 +
	19.50	102.14
	390.75	1.84
		100.30
		7.14 +
		107.00
		7.59 -
		99.85

Reset Gates 2130H

12

NE BP Vermont & Penn.

	4.15	89.09	294.73	84.48	84.40	
+20 S				46.		0.08
TP				3.13	85.65	
	4.57	89.8v				
+20 N				4.75	85.07	84.6 0.47
+40 N				4.86	84.96	85.0 0.04
+40 S				5.27	84.55	84.8 0.25
1700 S				3.40	86.4v	85.37 1.05v
1700 N				4.19	85.73	85.57 0.06v
1750 N				3.28	86.54	86.05 0.49v
1750 S				3.04	86.78	85.85 0.93v
J.P.	4.93	91.54		3.21	86.01	
2100 N				4.69	86.85	86.53 0.32v
2100 S				5.13	86.41	86.33 0.08v
2160 S				4.60	87.24	86.90 0.14v
2160 N				4.17	87.37	87.1 0.27v

Cut Fill

84.96
4.15
89.11
3.83
85.28
4.57
84.80
84.58
3.21
86.64
4.93
91.57
86.45
85.37
1.08
66
57
09
86.81
85.85
09

Grades Alley Block 61 - City Hq Hs
 Wightman - Landis Wilson - 35th

13

				NW BF	Cut	Fill	Wightman TC
Ech	5.79	53.47		347.68	Night + 30		E 50.99 W 51.29
T.P.	4.36	55.32	2.51	50.96	50.90	0.06	Landis TC
N ch			4.07	51.25	51.10	0.15	E 51.04 W 50.42
20 W			3.31	52.01	51.70	0.31 X	347.68
70 E			4.00	51.32	51.40	0.08 X	57.79
40 N			3.37	51.95	51.60	0.35 X	53.47
40 E			4.15	51.17	51.20	0.03 X	2.58
20 W			4.45	50.87			50.96
80 E			4.95	50.37			47.6
110 W			5.52	49.80	49.70	0.10 X	55.32
110 E			5.50	49.82	49.70	0.12 X	8.86
150 W			5.44	49.88	49.92	0.04 X	46.46
150 E			6.24	49.08	49.96	0.12 X	47.6
200 W			6.36	48.96	49.30	0.66 X	50.74
100 E			6.97	48.35	48.03	0.32 X	
250 W			4.79	50.53	47.33	3.20 X	
" E			7.75	47.57	47.11	0.46 X	
3 TP	428	5074	8.86	46.46			
300 W			2.60	48.14	46.36	1.78 X	
300 E			4.28	46.46	46.18	0.28 X	
350 W			5.18	45.56	45.38	0.18 X	
" E			5.32	45.42	45.26	0.16 X	
380 W			6.00	44.74	44.80	0.06 X	
" E			5.60	45.14	44.70	0.44 X	

		50.74			Cut	Fill	
440 W			7.66	43.08	43.20		51.74
" E			6.55	44.19	43.08	1.11x	7.12
TP	1.02	44.64	7.12	43.62x			43.62
500 W			3.05	41.59	41.37	0.22x	1.02
" E			3.26	41.38	41.45		44.64
5+50 W			4.62	40.02	39.85	0.27x	14.23
" E			4.95	39.69	40.10		50.41
5+60 W			4.96	39.68	39.00	0.68x	
" E			5.36	39.28	39.30		0.02x
5+70 W			5.79	38.85	37.20	1.65x	
" E			5.03	39.61	37.60	2.01x	
TP			10.28				
			3.95				
			14.23				

Culvert No 2 Sicsta Drive

Cut 1

	2.6	414.50		411.90	State on P.L. FB 1168	
0+00			0.7	413.8	406.9	6.9
0+25			4.7	409.8	402.7	7.1
0+50			7.6	406.9	398.4	8.5
T.P.	0.40	404.80	10.1	404.4		
0+75			3.9	400.9	394.1	6.8
T.P.	5.20	398.30	11.7	393.1		
1+00			8.4	389.9	390.0	Grade

Culvert No 1 Cajon Way & Madison Ave

	4.4	412.9		411.5	Field Book .1168	
cb line 0+00			5.0	415.9	411.5	4.4
0+25			3.3	415.6	408.9	6.7
0+50			6.5	414.4	406.3	8.1
0+75			10.6	410.3	403.7	6.6
T.P.	1.3	411.6	10.6	410.3		
1+00			10.6	401.0	401.0	Grade

Culvert No 3

	1.1	427.7		426.6	E Madison E 55th	
NE Hub			9.8	417.9	401.0	16.9
SE Hub			10.1	417.6	401.0	16.6
SW Hub			11.0	416.7	399.0	17.7
NW Hub			10.1	417.6	399.0	18.6

Hubs on cb line 25' on either side of $\frac{1}{2}$ of culvert

Walker
Jubilee
Knox
5-12-27

CANYON TERRACE
CANYON WAY GRADES

from Madison to Sista Dr.

Yk. Sta	Yk. Grade	Elv. Sta	Elv. Grade	Elv. Grade
256.97 south of cb PC = PC = 0400 4 = 0185 + 51.23	417.08	256.97 south of cb PC 4 = 51.23	417.60	417.60
145286	417.39	+ 51.25	417.67	417.67
145289	417.69	+ 022.50	418.14	418.14
145294	418.00	+ 153.75	418.41	418.41
24057 1/2 PC	418.30	2404 1 - 51.89	418.68	418.68
Point 1	418.20	2458.88 - cb PC	418.95	418.95
" 2	418.10	cb Curve	419.05	419.05
" 3 = EC.	418.00	cb EC. on Sista	419.15	419.15

418413 = X from P-17

Yk.	Grade	Elv.										
13701	417.18	13701	417.49	13701	417.79	13701	418.10	13701	418.40	13701	418.75	13701
13702	417.18	13702	417.49	13702	417.79	13702	418.10	13702	418.40	13702	418.75	13702
13703	417.18	13703	417.49	13703	417.79	13703	418.10	13703	418.40	13703	418.75	13703
13704	417.18	13704	417.49	13704	417.79	13704	418.10	13704	418.40	13704	418.75	13704
13705	417.18	13705	417.49	13705	417.79	13705	418.10	13705	418.40	13705	418.75	13705
13706	417.18	13706	417.49	13706	417.79	13706	418.10	13706	418.40	13706	418.75	13706
13707	417.18	13707	417.49	13707	417.79	13707	418.10	13707	418.40	13707	418.75	13707
13708	417.18	13708	417.49	13708	417.79	13708	418.10	13708	418.40	13708	418.75	13708
13709	417.18	13709	417.49	13709	417.79	13709	418.10	13709	418.40	13709	418.75	13709
13710	417.18	13710	417.49	13710	417.79	13710	418.10	13710	418.40	13710	418.75	13710
13711	417.18	13711	417.49	13711	417.79	13711	418.10	13711	418.40	13711	418.75	13711
13712	417.18	13712	417.49	13712	417.79	13712	418.10	13712	418.40	13712	418.75	13712
13713	417.18	13713	417.49	13713	417.79	13713	418.10	13713	418.40	13713	418.75	13713
13714	417.18	13714	417.49	13714	417.79	13714	418.10	13714	418.40	13714	418.75	13714
13715	417.18	13715	417.49	13715	417.79	13715	418.10	13715	418.40	13715	418.75	13715
13716	417.18	13716	417.49	13716	417.79	13716	418.10	13716	418.40	13716	418.75	13716
13717	417.18	13717	417.49	13717	417.79	13717	418.10	13717	418.40	13717	418.75	13717
13718	417.18	13718	417.49	13718	417.79	13718	418.10	13718	418.40	13718	418.75	13718
13719	417.18	13719	417.49	13719	417.79	13719	418.10	13719	418.40	13719	418.75	13719
13720	417.18	13720	417.49	13720	417.79	13720	418.10	13720	418.40	13720	418.75	13720
13721	417.18	13721	417.49	13721	417.79	13721	418.10	13721	418.40	13721	418.75	13721
13722	417.18	13722	417.49	13722	417.79	13722	418.10	13722	418.40	13722	418.75	13722
13723	417.18	13723	417.49	13723	417.79	13723	418.10	13723	418.40	13723	418.75	13723
13724	417.18	13724	417.49	13724	417.79	13724	418.10	13724	418.40	13724	418.75	13724
13725	417.18	13725	417.49	13725	417.79	13725	418.10	13725	418.40	13725	418.75	13725
13726	417.18	13726	417.49	13726	417.79	13726	418.10	13726	418.40	13726	418.75	13726
13727	417.18	13727	417.49	13727	417.79	13727	418.10	13727	418.40	13727	418.75	13727
13728	417.18	13728	417.49	13728	417.79	13728	418.10	13728	418.40	13728	418.75	13728
13729	417.18	13729	417.49	13729	417.79	13729	418.10	13729	418.40	13729	418.75	13729
13730	417.18	13730	417.49	13730	417.79	13730	418.10	13730	418.40	13730	418.75	13730
13731	417.18	13731	417.49	13731	417.79	13731	418.10	13731	418.40	13731	418.75	13731
13732	417.18	13732	417.49	13732	417.79	13732	418.10	13732	418.40	13732	418.75	13732
13733	417.18	13733	417.49	13733	417.79	13733	418.10	13733	418.40	13733	418.75	13733
13734	417.18	13734	417.49	13734	417.79	13734	418.10	13734	418.40	13734	418.75	13734
13735	417.18	13735	417.49	13735	417.79	13735	418.10	13735	418.40	13735	418.75	13735
13736	417.18	13736	417.49	13736	417.79	13736	418.10	13736	418.40	13736	418.75	13736
13737	417.18	13737	417.49	13737	417.79	13737	418.10	13737	418.40	13737	418.75	13737
13738	417.18	13738	417.49	13738	417.79	13738	418.10	13738	418.40	13738	418.75	13738
13739	417.18	13739	417.49	13739	417.79	13739	418.10	13739	418.40	13739	418.75	13739
13740	417.18	13740	417.49	13740	417.79	13740	418.10	13740	418.40	13740	418.75	13740
13741	417.18	13741	417.49	13741	417.79	13741	418.10	13741	418.40	13741	418.75	13741
13742	417.18	13742	417.49	13742	417.79	13742	418.10	13742	418.40	13742	418.75	13742
13743	417.18	13743	417.49	13743	417.79	13743	418.10	13743	418.40	13743	418.75	13743
13744	417.18	13744	417.49	13744	417.79	13744	418.10	13744	418.40	13744	418.75	13744
13745	417.18	13745	417.49	13745	417.79	13745	418.10	13745	418.40	13745	418.75	13745
13746	417.18	13746	417.49	13746	417.79	13746	418.10	13746	418.40	13746	418.75	13746
13747	417.18	13747	417.49	13747	417.79	13747	418.10	13747	418.40	13747	418.75	13747
13748	417.18	13748	417.49	13748	417.79	13748	418.10	13748	418.40	13748	418.75	13748
13749	417.18	13749	417.49	13749	417.79	13749	418.10	13749	418.40	13749	418.75	13749
13750	417.18	13750	417.49	13750	417.79	13750	418.10	13750	418.40	13750	418.75	13750
13751	417.18	13751	417.49	13751	417.79	13751	418.10	13751	418.40	13751	418.75	13751
13752	417.18	13752	417.49	13752	417.79	13752	418.10	13752	418.40	13752	418.75	13752
13753	417.18	13753	417.49	13753	417.79	13753	418.10	13753	418.40	13753	418.75	13753
13754	417.18	13754	417.49	13754	417.79	13754	418.10	13754	418.40	13754	418.75	13754
13755	417.18	13755	417.49	13755	417.79	13755	418.10	13755	418.40	13755	418.75	13755
13756	417.18	13756	417.49	13756	417.79	13756	418.10	13756	418.40	13756	418.75	13756
13757	417.18	13757	417.49	13757	417.79	13757	418.10	13757	418.40	13757	418.75	13757
13758	417.18	13758	417.49	13758	417.79	13758	418.10	13758	418.40	13758	418.75	13758
13759	417.18	13759	417.49	13759	417.79	13759	418.10	13759	418.40	13759	418.75	13759
13760	417.18	13760	417.49	13760	417.79	13760	418.10	13760	418.40	13760	418.75	13760
13761	417.18	13761	417.49	13761	417.79	13761	418.10	13761	418.40	13761	418.75	13761
13762	417.18	13762	417.49	13762	417.79	13762	418.10	13762	418.40	13762	418.75	13762
13763	417.18	13763	417.49	13763	417.79	13763	418.10	13763	418.40	13763	418.75	13763
13764	417.18	13764	417.49	13764	417.79	13764	418.10	13764	418.40	13764	418.75	13764
13765	417.18	13765	417.49	13765	417.79	13765	418.10	13765	418.40	13765	418.75	13765
13766	417.18	13766	417.49	13766	417.79	13766	418.10	13766	418.40	13766	418.75	13766
13767	417.18	13767	417.49	13767	417.79	13767	418.10	13767	418.40	13767	418.75	13767
13768	417.18	13768	417.49	13768	417.79	13768	418.10	13768	418.40	13768	418.75	13768
13769	417.18	13769	417.49	13769	417.79	13769	418.10	13769	418.40	13769	418.75	13769
13770	417.18	13770	417.49	13770	417.79	13770	418.10	13770	418.40	13770	418.75	13770
13771	417.18	13771	417.49	13771	417.79	13771	418.10	13771	418.40	13771	418.75	13771
13772	417.18	13772	417.49	13772	417.79	13772	418.10	13772	418.40	13772	418.75	13772
13773	417.18	13773	417.49	13773	417.79	1						

MARKY
To Mark
No. 109
9-12-7

CANYON TERRACE

Siesta Drive GRADES
from 55th St. West

S.W. Sta	S.W. Grade	N.E. Sta.	N.E. Grades
cb RC on 55th	431.38	cb RC on 55th	432.37
ctr Curve +10	431.89	ctr Curve +10	431.61
cb EC on Siesta	430.39	cb EC on Siesta	430.85
+65 = Bk	425.66	+65 = Bk	425.90
+85 = Bk	424.06	+85 = "	424.21
1+07.4V = RC Lt.	422.84	1+07.4V = RC	423.05
7300 2910 1992 Pl. ch 1287 12.89 16.40	2035'15" 17'30" 2050'13.5" 4'54'45" 7'10'15" (10'22'45") 8'0'33"	2057' Pl. ch 2057' east from Ch. Bk 2'09'27" Bk 2'09'57" Bk 5'08'27" Bk 2'36'38" 8'0'33" 2nd 1-25.19'	421.50 420.55 419.83 419.50 418.50 418.00 417.25 416.50 415.89 415.14 414.49 413.85 413.20 412.56 412.14 411.94 411.94 412.15 412.57 412.88
cb EC = S.E. Siesta +100	419.15	2+17.14 = Bk (2-4308) 2+16.05V app. EC on South	418.50 418.00 417.50
+52.25	417.25	3+03.3 = +100 = Bk	417.50
1+04.50 = RC Lt.	416.50	0+42.25	416.90
ctr.	415.89	+84.50 = Bk	416.39
PRC.	415.14	1+04.50 "	415.89
2 Parts to Bk central	414.49	+24.50 "	415.27
0	28'29'15"	1-56.58	413.19
1	56'59'30"	1481.25 (1-10.05)	412.88
2	85'29'45"	1491.10 = RC.	
Bk. 2	114'00' (11'55')		
	136'55'		
	159'50'		
	182'45'		
	185'36' = 2nd 500m N. Grade		
	205'40'		
	228'35'		
EC.	240'00'		

43269-7 from P.18

Sta	Grade	Sta	Grade
56 431.48	432.00	430.49	425.76
431.51	431.00	430.52	425.76
431.54	430.00	430.55	425.76
431.57	429.00	430.58	425.76
431.60	428.00	430.61	425.76
431.63	427.00	430.64	425.76
431.66	426.00	430.67	425.76
431.69	425.00	430.70	425.76
431.72	424.00	430.73	425.76
431.75	423.00	430.76	425.76
431.78	422.00	430.79	425.76
431.81	421.00	430.82	425.76
431.84	420.00	430.85	425.76
431.87	419.00	430.88	425.76
431.90	418.00	430.91	425.76
431.93	417.00	430.94	425.76
431.96	416.00	430.97	425.76
431.99	415.00	431.00	425.76
432.02	414.00	431.03	425.76
432.05	413.00	431.06	425.76
432.08	412.00	431.09	425.76
432.11	411.00	431.12	425.76
432.14	410.00	431.15	425.76
432.17	409.00	431.18	425.76
432.20	408.00	431.21	425.76
432.23	407.00	431.24	425.76
432.26	406.00	431.27	425.76
432.29	405.00	431.30	425.76
432.32	404.00	431.33	425.76
432.35	403.00	431.36	425.76
432.38	402.00	431.39	425.76
432.41	401.00	431.42	425.76
432.44	400.00	431.45	425.76
432.47	399.00	431.48	425.76
432.50	398.00	431.51	425.76
432.53	397.00	431.54	425.76
432.56	396.00	431.57	425.76
432.59	395.00	431.60	425.76
432.62	394.00	431.63	425.76
432.65	393.00	431.66	425.76
432.68	392.00	431.69	425.76
432.71	391.00	431.72	425.76
432.74	390.00	431.75	425.76
432.77	389.00	431.78	425.76
432.80	388.00	431.81	425.76
432.83	387.00	431.84	425.76
432.86	386.00	431.87	425.76
432.89	385.00	431.90	425.76
432.92	384.00	431.93	425.76
432.95	383.00	431.96	425.76
432.98	382.00	431.99	425.76
433.01	381.00	432.02	425.76
433.04	380.00	432.05	425.76
433.07	379.00	432.08	425.76
433.10	378.00	432.11	425.76
433.13	377.00	432.14	425.76
433.16	376.00	432.17	425.76
433.19	375.00	432.20	425.76
433.22	374.00	432.23	425.76
433.25	373.00	432.26	425.76
433.28	372.00	432.29	425.76
433.31	371.00	432.32	425.76
433.34	370.00	432.35	425.76
433.37	369.00	432.38	425.76
433.40	368.00	432.41	425.76
433.43	367.00	432.44	425.76
433.46	366.00	432.47	425.76
433.49	365.00	432.50	425.76
433.52	364.00	432.53	425.76
433.55	363.00	432.56	425.76
433.58	362.00	432.59	425.76
434.01	361.00	432.62	425.76
434.04	360.00	432.65	425.76
434.07	359.00	432.68	425.76
434.10	358.00	432.71	425.76
434.13	357.00	432.74	425.76
434.16	356.00	432.77	425.76
434.19	355.00	432.80	425.76
434.22	354.00	432.83	425.76
434.25	353.00	432.86	425.76
434.28	352.00	432.89	425.76
434.31	351.00	432.92	425.76
434.34	350.00	432.95	425.76
434.37	349.00	432.98	425.76
434.40	348.00	433.01	425.76
434.43	347.00	433.04	425.76
434.46	346.00	433.07	425.76
434.49	345.00	433.10	425.76
434.52	344.00	433.13	425.76
434.55	343.00	433.16	425.76
434.58	342.00	433.19	425.76
435.01	341.00	433.22	425.76
435.04	340.00	433.25	425.76
435.07	339.00	433.28	425.76
435.10	338.00	433.31	425.76
435.13	337.00	433.34	425.76
435.16	336.00	433.37	425.76
435.19	335.00	433.40	425.76
435.22	334.00	433.43	425.76
435.25	333.00	433.46	425.76
435.28	332.00	433.49	425.76
435.31	331.00	433.52	425.76
435.34	330.00	433.55	425.76
435.37	329.00	433.58	425.76
435.40	328.00	433.61	425.76
435.43	327.00	433.64	425.76
435.46	326.00	433.67	425.76
435.49	325.00	433.70	425.76
435.52	324.00	433.73	425.76
435.55	323.00	433.76	425.76
435.58	322.00	433.79	425.76
436.01	321.00	433.82	425.76
436.04	320.00	433.85	425.76
436.07	319.00	433.88	425.76
436.10	318.00	433.91	425.76
436.13	317.00	433.94	425.76
436.16	316.00	433.97	425.76
436.19	315.00	434.00	425.76
436.22	314.00	434.03	425.76
436.25	313.00	434.06	425.76
436.28	312.00	434.09	425.76
436.31	311.00	434.12	425.76
436.34	310.00	434.15	425.76
436.37	309.00	434.18	425.76
436.40	308.00	434.21	425.76
436.43	307.00	434.24	425.76
436.46	306.00	434.27	425.76
436.49	305.00	434.30	425.76
436.52	304.00	434.33	425.76
436.55	303.00	434.36	425.76
436.58	302.00	434.39	425.76
437.01	301.00	434.42	425.76
437.04	300.00	434.45	425.76
437.07	299.00	434.48	425.76
437.10	298.00	434.51	425.76
437.13	297.00	434.54	425.76
437.16	296.00	434.57	425.76
437.19	295.00	434.60	425.76
437.22	294.00	434.63	425.76
437.25	293.00	434.66	425.76
437.28	292.00	434.69	425.76
437.31	291.00	434.72	425.76
437.34	290.00	434.75	425.76
437.37	289.00	434.78	425.76
437.40	288.00	434.81	425.76
437.43	287.00	434.84	425.76
437.46	286.00	434.87	425.76
437.49	285.00	434.90	425.76
437.52	284.00	434.93	425.76
437.55	283.00	434.96	425.76
437.58	282.00	434.99	425.76
438.01	281.00	435.02	425.76
438.04	280.00	435.05	425.76
438.07	279.00	435.08	425.76
438.10	278.00	435.11	425.76
438.13	277.00	435.14	425.76
438.16	276.00	435.17	425.76
438.19	275.00	435.20	425.76
438.22	274.00	435.23	425.76
438.25	273.00	435.26	425.76
438.28	272.00	435.29	425.76
438.31	271.00	435.32	425.76
438.34	270.00	435.35	425.76
438.37	269.00	435.38	425.76
438.40	268.00	435.41	425.76
438.43	267.00	435.44	425.76
438.46	266.00	435.47	425.76
438.49	265.00	435.50	425.76
438.52	264.00	435.53	425.76
438.55	263.00	435.56	425.76
438.58	262.00	435.59	425.76
439.01	261.00	435.62	425.76
439.04	260.00	435.65	425.76
439.07	259.00	435.68	425.76
439.10	258.00	435.71	425.76
439.13	257.00	435.74	425.76
439.16	256.00	435.77	425.76
439.19	255.00	435.80	425.76
439.22	254.00	435.83	425.76
439.25	253.00	435.86	425.76
439.28	252.00	435.89	425.76
439.31	251.00	435.92	425.76
439.34	250.00	435.95	425.76
439.37	249.00	435.98	425.76
439.40	248.00	436.01	425.76
439.43	247.00	436.04	425.76
439.46	246.00	436.07	425.76
439.49	245.00	436.10	425.76
439.52	244.00	436.13	425.76

Tolson
427

Grade Stakes
Byron St. Evergreen to Locust

TP 4.13 24.80 20.67
6.85 21.31 0.34 24.46

5N BP
Roserans B
Canon

W L Locust aut

5'S φ 3.15 28.16 27.5 46

End ret 3.63 27.68 26.16 1.52

= 2775

5'S φ 2.73 28.58 27.9 68

5'N BP 2.99 28.32 27.02 86

T.P. 8.18 36.50 2.99 28.32

PL = 2750

5'N BP 8.17 28.33 27.87 46

5'S E 7.21 29.29 28.33 96

= 2400

5'S φ 6.08 29.92 29.17 75

5'N BP 7.37 29.13 28.88 145

= 1750

5'N BP 6.33 30.17 29.5 67

5'S E 5.74 31.06 30.0 106

= 1400

5'S E 3.99 32.51 30.83 168

5'N BP 5.80 30.70 30.32 22

SEE NEXT PAGE

21

= 0750

5'N BP 5.16 31.34 31.13 21

5'S E 3.41 33.09 31.67 142

= 0725

5'S φ 2.85 33.65 32.08 157

5'N BP 4.44 32.06 31.54 52

End ret on Evergreen 4.25 31.55 31.16 39

0700

5'S E 2.17 34.33 32.50 183

T.P. 4.14 34.60 6.04 3046

T.P. 3.50 28.38 9.72 2488

B.M. 7.72 (2066-2067)

28.58	33.04	33.04	33.04
4.46	4.04	5.18	5.32
33.04	28.20	27.86	27.72
	77.28	27.	26.65
	1.32	.86 out	1.07 out
	out		

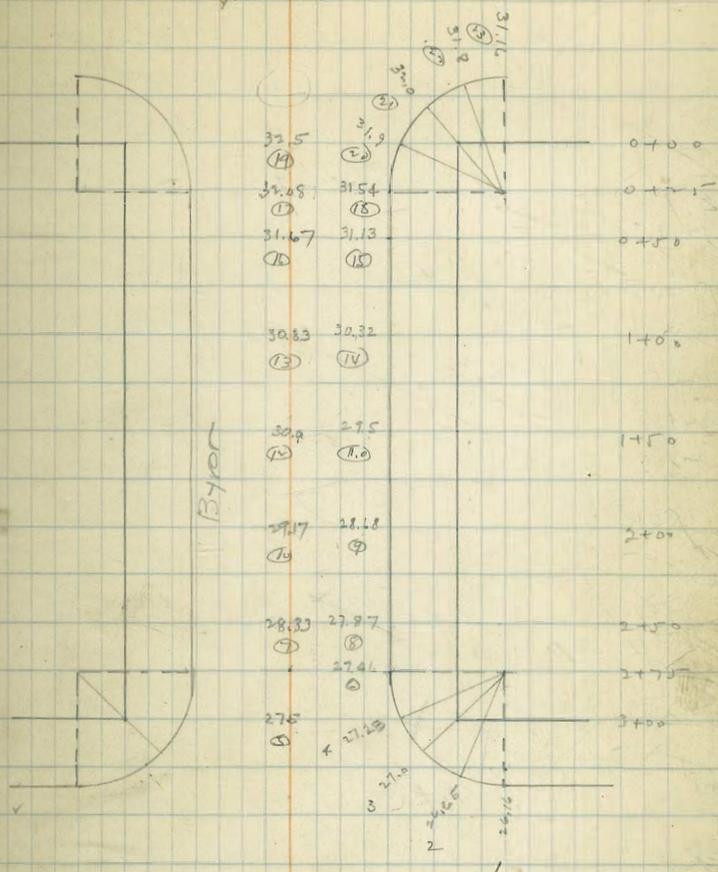
33.65	31.90	31.90	31.90
325	4.81	5.86	6.11
3670	32.09	31.02	36.77
	31.90	F.71	F.1.09
	1.19		
	out		

Grade Stakes - Byron
Evergreen to Locust

10.65 35.11 24.46 TP Page 21

1		7.86	27.25	26.16	1.09	
2		7.60	27.51	26.65	1.86	
3		7.32	27.79	27.00	.79	
4		6.62	28.49	27.28	1.21	
5		6.92	28.19	27.50	.69	
7		5.78	29.33	28.33	1.00	
6		6.53	28.58	27.46	1.12	
5		6.18	28.93	27.87	1.06	
9		5.36	29.75	28.68	1.07	
10		5.17	29.94	29.17	0.77	
11	7.16	37.72	4.55	30.56	29.50	1.06
12		4.05	31.06	30.00	1.06	
13		5.20	32.52	30.83	1.69	
14		6.19	31.53	30.32	1.21	
15		5.69	32.03	31.13	0.90	
16		4.62	33.10	31.67	1.43	
17		4.06	33.66	32.08	1.58	
18		5.43	32.29	31.54	0.75	
19		3.38	34.34	32.50	1.84	
20		4.66	33.06	31.9	1.16	
21		6.36	31.36	32.0	.64	
22		5.13	32.59	31.8	.78	
23		5.69	32.03	31.16	.87	

Evergreen



Locust

Grades - Dwight St

47th East to 47th

10.00	334.00		324.0	NW Chamounce Dwight
8.81	342.73	0.08	333.92	

S.L. Dwight

Cut

Fill

2+19.31		3.70	339.03	39.00	0.0
1+69.31	TP 5.00	3.36	339.37	38.77	0.6
1+25		3.62	340.75	38.75	2.0
0+80		4.61	339.76	38.50	1.3
0+50		5.03	339.34	37.37	1.9
0+00		6.49	337.88	35.5	2.4
5M 85' RP		5.46	338.91		

W.L. 47th

344.37

0+00		6.49	337.88	35.5	2.4 ✓
0+50	TP 3.75	6.11	338.26	35.89	2.4 ✓
1+00		5.70	338.34	36.29	2.0 ✓
1+50		4.22	337.82	36.18	1.1 ✓
1+90	Brk	4.44	337.60	37.00	0.6 ✓
2+50		6.78	335.26	34.93	0.4 ✓
3+00		8.28	333.76	33.20	0.6 ✓
3+50		10.18	331.86	31.48	0.4 ✓
4+00	TP 1.22	11.77	330.27	29.75	0.6 ✓
4+50		3.12	328.37	28.03	0.4
5+00		5.61	325.88	26.30	0.4 ✓

W.L. 47th

321.49

Cut

Fill

5150		6.06	325.43	24.57
5181.5	N.L. of Myrtle	7.32	324.17	23.50
0100	S.L. of Myrtle	10.99	320.50	21.20
T.P.	0.82	321.32	10.99	320.50
0150		2.16	319.16	18.70
1100		3.88	317.44	16.40
1150		9.88	311.44	14.10
T.P.	3.57	315.01	9.88	311.44
2100		9.91	305.10	11.8
2150		12.22	302.79	09.5

0.81

0.71 on 47 & 1/2 on Myrtle

on 47th
0.5 & 1.0 on Myrtle

0.5 ✓

1.0 ✓

2.7 ✓

6.7 ✓

6.7 ✓

E.L. 47th

T.P.	7.59	320.30	21.30	312.71
2150			6.90	313.40
2100			3.68	316.62
T.P.	9.17	325.63	3.84	316.46
1150			8.26	317.37
1100			6.21	319.42
0150			3.73	321.90
T.P.	10.53	331.83	4.33	321.30
	S.L. of Myrtle		8.21	323.63

2.9 ✓

3.8 ✓

2.3 ✓

2.0 ✓

2.2 ✓

1.6 on Myrtle & 2.0 on 47th

331.73

E.L. 474

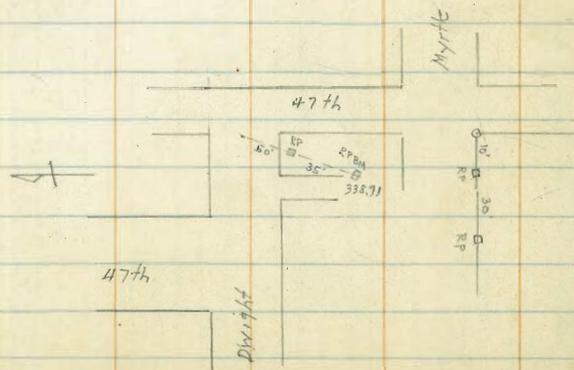
5191.5	N. 40° E Myrtle	5.33	326.50	24.5	2.0 on 474 & 2.5 on Myrtle
5150		4.51	327.32	25.41	1.9 ✓
5400		2.59	329.24	27.02	2.2 ✓
T.P.	6.58	335.02	2.99	328.84	
4150		4.85	330.57	28.63	2.0 ✓
4100		3.55	331.87	30.24	1.7 ✓
3150		1.86	333.56	31.85	1.7 ✓
T.P.	8.87	342.43	1.86	333.56	
3100		7.26	335.17	33.46	1.7 ✓
2150		5.91	336.52	35.07	1.4 ✓
1190 B.R.		4.90	337.48	37.00	0.5 ✓
1150		5.17	337.36	36.58	0.7 ✓
1100		5.85	336.58	36.05	0.5 ✓
150		6.69	335.74	35.53	0.2 ✓
T.P.	1.56	337.30	6.69	335.74	
0700		2.34	334.96	35.00	Graded
T.P.	2.72	227.53	12.49	324.81	
0-60		6.62	220.91	34.00	13.1
T.P.	12.23	339.40	0.36	227.17	
T.P. B.M. 85 R.P.	5.40	344.31	0.49	338.91	

374.31

N.4. of Dwight

0700	6.30	338.01	35.51	2.5 ✓
0750	5.00	339.31	37.38	1.9 ✓
0850 Brk	4.43	339.88	38.50	1.4 ✓
1725	3.63	340.68	39.25	1.4 ✓
1767.31			40.00	

4.35 339.96 = $\left. \begin{array}{l} \text{Book 1145} \\ 18.95 \end{array} \right\} 339.94$



Walker
McHugh
Lock
M. Hood
2-21-29

SEWER Const. 110 MEADE Ave.
Bet. MECHANIC and 33rd St.

Exist. N.H. Mechanic		1897	367.63	Flow Line
= 0+00	383.60	5.83	377.77	367.40 367.90 368.13 + 9.64
+ 45.25		5.57	378.03	368.45 368.22 + 9.58
+ 90.50		5.43	378.17	368.78 368.55 + 9.39
+ 135.75		5.18	378.42	369.10 368.87 + 9.32
+ 81-DE.		5.20	378.40	369.43 369.20 + 8.97

Book 1296-33
N.Y. B.P. Meade + Felton 381.25
383.60
385.60

Note. Flow line M.H. Const. at 367.63 = .23 Higher than shown on profile and Grade. Was raised accordingly - C.M.

Jidewalk stakes on 43rd St.

EL. Stg	Cont. From	P-66	N.L. Grades
= 0+00	346.62	EL. Grades	346.39
+ 50 = Bk.	346.81	N.L. Sts. P-66 (36.25) ³	346.46
+ 39.2	346.83	0+36.25	346.53
+ 98.4	346.86	+ 72.5	346.60
+ 137.6	346.89	1+08.75 = Bk. (39.25) ³	346.65
+ 76.8 = Bk. by Walk.	346.92	1+48	346.95
(1-49.7)	347.27	+ 87.25	347.30
2+26.5 = End. Walk.	348.68	2+26.5 = Bk. (1-135)	347.65
+ 78 = E. "	349.55	2+40 = Bk. (43.5) ²	347.98
3+09	350.38	2+83.5	349.51
+ 40 = Bk. (30) ²	351.38	3+27 = Bk. by Walk	351.03
3+70	352.38	4+26 = End. Each. Walk (2-27)	354.53
4+00 = "	353.29	4+53	355.44
2-50	355.41	+ 80 = Bk.	356.36
4+50	356.11	5+26.8 = N.L. El. Capn.	357.47

35048-8 M. P. 15

EL. Stg	Cont. From	P-66	N.L. Grades
= 0+00	346.62	EL. Grades	346.39
+ 50 = Bk.	346.81	N.L. Sts. P-66 (36.25) ³	346.46
+ 39.2	346.83	0+36.25	346.53
+ 98.4	346.86	+ 72.5	346.60
+ 137.6	346.89	1+08.75 = Bk. (39.25) ³	346.65
+ 76.8 = Bk. by Walk.	346.92	1+48	346.95
(1-49.7)	347.27	+ 87.25	347.30
2+26.5 = End. Walk.	348.68	2+26.5 = Bk. (1-135)	347.65
+ 78 = E. "	349.55	2+40 = Bk. (43.5) ²	347.98
3+09	350.38	2+83.5	349.51
+ 40 = Bk. (30) ²	351.38	3+27 = Bk. by Walk	351.03
3+70	352.38	4+26 = End. Each. Walk (2-27)	354.53
4+00 = "	353.29	4+53	355.44
2-50	355.41	+ 80 = Bk.	356.36
4+50	356.11	5+26.8 = N.L. El. Capn.	357.47

35048-8 M. P. 15

EL. Stg	Cont. From	P-66	N.L. Grades
= 0+00	346.62	EL. Grades	346.39
+ 50 = Bk.	346.81	N.L. Sts. P-66 (36.25) ³	346.46
+ 39.2	346.83	0+36.25	346.53
+ 98.4	346.86	+ 72.5	346.60
+ 137.6	346.89	1+08.75 = Bk. (39.25) ³	346.65
+ 76.8 = Bk. by Walk.	346.92	1+48	346.95
(1-49.7)	347.27	+ 87.25	347.30
2+26.5 = End. Walk.	348.68	2+26.5 = Bk. (1-135)	347.65
+ 78 = E. "	349.55	2+40 = Bk. (43.5) ²	347.98
3+09	350.38	2+83.5	349.51
+ 40 = Bk. (30) ²	351.38	3+27 = Bk. by Walk	351.03
3+70	352.38	4+26 = End. Each. Walk (2-27)	354.53
4+00 = "	353.29	4+53	355.44
2-50	355.41	+ 80 = Bk.	356.36
4+50	356.11	5+26.8 = N.L. El. Capn.	357.47

Note. Flow line M.H. Const. at 367.63 = .23 Higher than shown on profile and Grade. Was raised accordingly - C.M.

Alley Grades Block 39 La Jolla Park

0+00 Nine Silverado

Bliss

Isa bell

Morgan

10/6/67

0+00 E

0+00 W

Brk
0+52 E

0+52 W

Brk
0+52 W

1+00 E

1+00 W

1+50 E

1+50 W

1+50 W

1+50 W

1+50 W

Brk
2+00 E

2+00 E

2+00 W

2+50 E

2+50 W

2+50 W

Brk
2+80 E

2+80 E

2+80 W

2+80 W

3+00 E

3+00 W

3+50 E

3+50 W

3+50 W

4+00 E

4+00 W

4+50 E

4+50 W

5+00 E

5+00 W

Elev Grade Cut Fill

109.67

109.50 109.67

109.31 109.37

110.07 109.80 0.27 ✓

109.77 109.50 0.27

110.27 109.60 0.67

109.47 109.34 0.13 ✓

110.90 109.40 1.02 ✓

109.68 109.17 0.51 ✓

109.81 109.20 0.61 ✓

109.33 109.00 0.33

109.70 108.95 1.25 ✓

109.66 108.37 1.29

108.43 108.66 0.43 ✓

109.26 108.90 1.26 Teddy ✓

108.37 107.71 0.67 ✓

108.67 107.67 1.00 Teddy ✓

107.14 106.98 0.16 ✓

107.85 106.85 1.00 Teddy ✓

106.98 106.25 0.23

106.66 106.03 0.63 ✓

106.52 105.52 1.00 Teddy ✓

106.21 105.21 1.00 "

104.98 Paving time at

104.90 Paving time at

B.N. 105.81 S.W. Herschel & Wall

+ 3.96

+ 109.771 -

- 4.95

T.P. 105.291

+ 6.87

+ 112.167

+ 3.69

T.P. 108.47

+ 6.29

H.I. 114.71

- 5.33

109.38

Top Paving West side alley at Silverado

Grades for Sewer E.W. Morse Subdivision
 In Alley between F and G 30th and 32nd

B.M.
 P.P.
 3 East

	X	T	Elev. Grade	Elev. Stake	166.99	C	Rod
	0.39	167.38					
0+00	4.5 East of W Line 30 th		155.00	160.18	7.20 Rod	5.18	7.20
0+50			154.65	157.70	9.62 Rod	3.05	9.62
1+00			154.30	160.51	6.87 Rod	6.21	6.87
1+50			153.95	161.31	6.01 Rod	7.34	6.01
2+00			153.60	162.80	9.51 Rod	9.20	9.51
2+50			153.25	155.99	7.37 Rod	6.74	7.37
2+85	Man Hole		153.00	163.25	9.13 Rod	10.25	9.13
T.P.	3.23	164.91	6.20	161.18			
0+50			151.00	160.95	3.46 Rod	9.95	3.46
1+00			149.00	156.81	7.60 Rod	7.81	7.60
1+50			147.00	154.48	9.93	7.48	9.93
2+00			145.00	153.41	9.00	10.41	9.00
T.P.	1.27	152.93	12.75	151.66			
2+50			143.00	150.87	2.06	7.87	2.06
3+00	Man Hole		141.00	147.00	5.93	6.00	5.93
0+50			135.40	145.59	1.34	10.19	1.34
1+00			129.80	142.61	10.32	12.81	10.32
T.P.			12.46				

Void
 See Next Page

Grades for Sewer, E.W. Morse Subdivision
 In alley between FandG. 20th to 22nd.

Bliss 10/19/27	+	π	-	Elev. Stake B.M. SE Brass Plug 166.99. 20 th + F.	Elev. Grade	C.
0+00		167.38	7.20	160.18	155.00	5.18
0+50			9.68	157.70	154.65	3.05
1+00			6.87	160.51	154.30	6.21
1+50			6.07	161.31	153.95	7.36
2+00			4.58	162.80	153.60	9.20
2+50			7.39	155.99	153.25	6.74
2+85	MnHole		4.13	163.25	153.00	10.25 - 9.35
T.P.	323	164.41	6.20	161.18		
0+50			3.46	160.95	151.00	9.95 9.23
1+00			7.60	156.81	149.00	7.81 7.14
1+50			9.93	154.48	147.00	7.48
2+00			9.00	155.41	145.00	10.41
T.P.	127	152.93	12.75	151.66		
2+50			2.06	150.87	143.00	7.87
3+00	MnHole		5.93	147.00	141.00	6.00
0+50			7.34	145.59	135.40	10.19
1+00			10.32	142.61	129.80	12.81
T.P.	0.37	140.84	12.46	140.47		
1+50			1.63	139.21	124.20	15.01
2+00			12.46	128.38	118.60	9.78
T.P.	0.77	129.15	12.46	128.38		
2+30			6.97	122.18	115.24	6.94
T.P.	0.37	117.10	12.42	116.73		
0+50			2.31	114.79	109.725	5.07
1+00			7.85	109.25	104.21	5.04

0.7%

4.0%

11.2%

	+	π	-	Elev. Stone	Elev. Grad.	C
		117.10				
1+50			12.03	105.07	98.695	6.37
TP	0.74	105.81	12.03	105.07		
2+00	B.K.		4.99	100.82	93.18	7.64
2+50			10.54	95.27	89.93	5.34
TP	4.82	97.76	12.87	92.94		
3+00			7.09	90.67	86.68	3.99
3+21	14	Mn. Hole To be constructed	8.69	89.07	85.30	3.77
TP	6.60	98.79	5.57	92.19		
BN	544	Fanderson	4.67	94.12	99.157 Elev. B.M.	

Bliss
11/3/27

Grade Stakes Alley Block 74 Units

31.17

32

Between Mississippi & Alabama Meade & Monroe
Elevations

East Side of Alley

BM BP	SE Alabama	Monroe	401	324.62	460.62	C	F	Elev Stake	Elev Grade	0	F
T. Obs. in	13.00	337.62	4.01		332.90	00		9.98	333.60	0.00	
2 0+20			5.00	332.62	333.50		0.88	3.17	334.45	333.90	0.65
2 0+70	TP. 6.29	337.77	6.14	331.98	332.97	0.100		3.97	333.90	332.80	1.00
T. 1+20	TP. 4.30	335.23	6.34 7.11	330.93 330.66	331.44		0.78	2.88	332.25	331.90	0.55
3 1+60			9.58	330.65	330.6	0.05		3.23	332.00	331.00	1.00
3 2+00			3.93	331.30	330.3	1.00		4.32	330.9	330.91	0.00
T 2+40	5.48		5.23	330.00	330.0	0.00		5.53	329.70	330.82	1.12
0 2+70			5.33	329.90	329.90	0.00		4.49	330.74	330.75	0.00
3+00			6.16	329.07	329.80		0.73	4.90	330.33	330.69	0.36
3+50			5.58	329.65	329.65	0.00		5.81	329.42	330.58	1.16
4+00	TP 4.94	333.87	6.30	328.93	329.99	0.00		3.89	329.98	330.97	0.49
4+50	TP 4.94	335.73	3.08 6.60	330.70 329.73	329.33		0.20	4.85	330.88	330.36	0.52
5+00			5.55	330.18	329.18	1.00		4.20	331.50	330.24	0.29
5+20			6.07	329.66	329.12	0.54		3.57	332.16	330.20	1.96
5+60			9.73	331.0	329.00	2.00		3.73	330.00	329.50	2.50
6+00			7.38	328.35	328.35	0.00		6.93	328.8	328.8	0.00
TP	2.46	330.09	8.15	327.58							
			11.21	318.83	318.86						

SE Alabama Meade

(CANYON TERRACE)

55th St. Water Main

From a Point 200' South of St. Madison
to " " 100' North of Mrs. Sesta Dr.

Stations	H.T. from P34 = 427.91	Elev. of Aulcs	Bottom of Ditch Grades	
200' South St. Madison = 0 + 00		4.2	413.7	416.4 +7.3
+30 - 8ft		9.2	418.7	415.90 +2.8
+50 "		11.4	416.5	415.64 +0.9
+70 "		22.4	405.5	415.55 -1.00
+90 "		13.1	414.8	415.61 -0.8
1+10 "		10.2	417.7	416.53 +1.2
+30 "		9.8	418.1	417.60 +0.5
+50 "		6.8	421.1	418.83 +2.3
"				
2+00 = St. Madison N.W. MADISON T.P. 746 = 0 + 00	435.36	3.0 0.1	424.9 417.90	422.13 +2.7
+55		3.8	431.6	425.50 +6.1
1+10 = 8ft (246.67)		3.0	432.4	427.13 +5.2
1+56.67		3.4	432.0	427.70 +4.3
2+03.34 (1-36.67)		2.8	432.6	428.29 +4.3
2+40 - 35		3.0	432.4	428.76 +3.6
2+75		2.8	432.6	429.21 +3.4
3+10		2.3	433.1	429.75 +3.3
+50		1.3	434.1	430.30 +3.8
4+00		0.3	435.1	430.88 +4.2

From 200' South of St. Madison
to El Cajon See Page 35

(CANYON TERRACE)
 MADISON AVE Water Main
 (from 54th St. West.)

Stations	x		Elev. Sub	Elev. Bottom of DMH	
R.C. of Co Return					
54+6 56" 3194 = elev 2' off ditch	427.91	3.2	474.7	421.4	+3.3
① 64' 4" 47' 42"		3.4	477.5	419.9	+7.6
② " 70' 35" 24" at water main only		6.9	421.0	418.4	+2.6
③ = P.R.C. " 140' 23" 06"		8.10	419.8	416.9	+2.9
④ 0				416.30	
⑤ 0				415.70	
⑥ 0				415.10	
⑦ = R.C.	425.75	8.2	417.6	414.50	+3.1
4-51' 25"					
0-151' 25"					
1-40' 50"					
1-53' 75"					
2-1' 04"					
1-54' 88"					
2-15' 88" = opp ch R.C.					
		8.4	417.4	414.75	2.6
		8.4	417.6	415.0	+2.6
		7.8	418.0	415.3	+2.7
		7.4	418.4	415.6	+2.8
		7.5	418.3	415.83	+2.5

CANYON Box Dr.
 1/2 mi from 26
 425.75'

Radius 1/2 mi
 Madison Ave (approx)
 Street
 421.24 = B.M.
 427.91 = X

55th St. Water Main
Cont. from Page 33

Stations	HT from #33	Elev. Stub	Elev. Grade	
6100 South St. Madison	= 471.91		416.40	
= 0+00				
3-47.66				
0+47.66	39	424.0	417.10	+6.9
+95.67	14	426.5	417.80	+8.7
1+43 = Bkt.	3.4	424.5	418.50	+6.0
+63 = Bkt.	4.5	423.4	418.60	+4.8
+83 = Bkt.	5.6	422.3	418.50	+3.8
(5-53')				
8+35	7.3	420.6	417.46	+3.1
+87	8.3	419.6	416.47	+3.1
3+39	9.4	418.5	415.38	+3.3
+91	9.6	418.3	414.34	+4.0
4+43 = Bkt.	13.2	414.7	413.3	+1.4
+63 = "	15.2	412.7	413.2	-0.5
+83 = "	15.8	412.1	413.3	-1.2
(2-41.6)				
5+30.06	11.3	416.6	414.58	+2.0
5+77.12 Tee - N. North St. Gilbert	8.8	419.1	415.86	+3.3
2-50'				
6+27	7.4	420.5	417.47	+3.5
6+77.12 = End of Pipe at Kleejon	6.3	421.6	419.10	+2.5

M. J. ...
 11-7-27

(CAJON TERRACE)

Siesta Dr. Water Main
 From 55th St. West.

Sta.	H.S. from 38	Elev. Sub	Bottom Ditch Elev.	
Opp PC = 0+00	435.36	5.2	430.2	427.49 +2.7
cb PC = 0+10				
0+65 = Bk.		10.0	425.4	422.86 +2.6
+85 = "				
7R 318	425.75	11.5	423.9	421.26 +2.6
1+02.42 - PC		12.9	422.57	
		37	422.1	420.00 +2.1
0		5.3	420.5	418.67 +1.8
0		6.1	419.6	417.75 +1.8
0		6.5	419.3	417.03 +2.3
0 = EC		6.5	419.3	416.60 +2.7
Opp PC. SEC. Bed		6.8	419.0	416.05 +2.9
Top				
cb EC. opp. Siesta = 0+100		8.1	417.6	415.2 +2.4
(2-52.25)		8.6	417.1	414.35 +2.7
0+52.25				
1+04.5 = opp PC.		9.2	416.4	413.4 +3.0
2-55.95				
1+59.95		10.9	414.9	411.95 +3.5
2+15.40 = Bk.		13.2	412.6	409.3 +3.3

Marker
 8x10
 5x10
 6-20-28

Alley PAVING Grades
 Blk 74 PARK Villas

E.L. 5/10	E.L. Grades	M.L. Sta.	M.L. Grades
51. LANDIS = 0+00	302.80	51. Landis = 0+00	302.90
+20 = Brk.	302.00		
+40 = "	300.34	0+40 = Brk.	300.74
+50 = "	300.52	+50 = "	300.32
+60 = " (3-42.5)	300.35	+60 = "	300.16
1+02.5	300.13		300.00
1+45	299.97		299.83
+87.5	299.71		299.66
2+30 = Brk. (3-50')	299.50		299.50
2+80	298.74		298.66
3+30	297.97		297.83
+80 = Brk. (4-42.5)	297.20		297.00
4+22.5	295.97		295.82
+65	294.75		294.65
5+07.5	293.52		293.47
5+50 = Brk. 1-51	292.30		292.30
6+01 = M.L. DRYGANT.	292.00		291.70

Sublons Same as East

231.85 = S.E. BP LANDIS + ARNOTS

E.L.	Blk	Blk	Blk	- Blk	Blk	Blk	Blk	Blk	Blk
302.17	302.00	300.34	300.52	300.35	300.13	299.92	299.71	299.50	= Blk.
149	0.41	0.10	0.72	4.14	4.31	4.53	4.74	5.35	5.56
304.66	0.73	2.33	2.90	3.07	4.12	4.64	5.07	5.27	5.27
425	1.17	1.39	+1.24	1.12	1.64	1.28	1.34	1.34	1.34
300.71									Blk.
242									Blk.
305.64	116. 302.78	No stake	300.74	300.32	300.16	300.00	299.83	299.66	299.50
879	1.12		3.97	4.34	4.50	4.66	5.23	5.40	5.56
296.77			2.34	3.04	3.20	3.49	4.07	4.60	4.21
1204			+2.58	+1.30	-0.70	-0.83	0.84	-1.20	+1.35
297.27									
66. 298.74	297.97	297.20	295.97	294.75	293.52	292.30	291.70	291.70	
632	7.09	7.86	9.09	2.52	3.75	4.93	5.27	5.27	
563	6.49	6.72	8.82	2.45	2.90	3.90	5.26	5.26	
+0.69	+0.60	+1.14	+0.27	+0.07	+0.85	+1.03	0.01	0.01	
12. 298.66	297.83	297.00	295.82	294.65	293.47	292.30	291.70	291.70	
640	7.23	8.06	9.24	2.62	3.80	4.97	5.57	5.57	
686	5.80	7.89	6.25	2.89	4.92	4.95	5.48	5.48	
-0.46	+1.93	+0.17	+2.99	-0.27	-0.32	1.00	0.91	0.91	

Yoiker
Shaw
Rudinger
Shad: 6-20-28

Alloy PAVING GRADES
BK 75 - PARK VILLOS

Stations	E.L. Grades	stations	N.L. Grades
SL DRIGHT			
= 0+00	291.50		291.20
7-46.23			
0+46.43	290.78		290.51
+92.86	290.05		289.82
1+39.79	289.32		289.13
+85.72	288.59		288.41
2+37.15	287.86		287.75
2+78.6	287.13		287.09
3+25=BK (5-48")	286.40		286.40
3+73.	286.20		286.20
4+21	286.00		286.00
4+69	285.80		285.80
5+17	285.60		285.60
5+65=BK	285.40		285.40
+85=BK	285.20		285.10
6+00=NL Myrtle	285.00?	Y	284.40

Stations same

29727 = X from P. 37

Stations	E.L. Grades	N.L. Grades	Grades	Grades	Grades	Grades	Grades	Grades
291.12	291.50	290.78	290.05	289.32	288.59	287.86	287.13	
290	577	649	397	470	543	616	689	
286.40	585	594	321	439	504	638	669	
714	286.40	1455	1056	1031	1039	-022	1020	
29380	291.80	290.51	289.82	289.13	288.44	287.75	287.09	
	607	397	420	489	558	627	673	
	611	1.96	1.96	439	579	706	660	
	286.40	1.155	1.224	1.803	1.021	0.979	1.053	
	= BK							
	E.L. 286.40	286.20	286.00	285.80	285.60	285.40	285.20	285.00
	7.62	7.60	7.80	8.00	8.20	8.40	8.60	8.80
	7.36	6.85	6.10	4.29	5.17	6.20	6.63	7.60
	+0.26	+0.75	+1.70	+3.71	+3.08	+2.20	+1.77	+1.30
	= BK							
	N.L. 286.40	286.20	286.00	285.80	285.60	285.40	285.20	284.69
	7.62	7.60	7.80	8.00	8.20	8.40	8.70	9.15
	6.15	8.05	7.64	6.75	7.61	7.91	8.45	
	+1.47	-0.45	+0.16	+1.25	+0.59	+0.49	+0.25	

Worked
Ref. Shady
Brook 8.4.28

CONST. SEWER IN HAMMINGTON ST.
Bet HOWARD + LIDGOLD
Sewer 2-6" West of line Bet Howard + Lidg.

Exist. Sewer 25' South of Alt

0+00	352.14	9.47	342.67	339.00	+3.67
732.5		8.91	343.23	339.25	8 Left out.
765 = MH #1 = 0+100 (0+43)		8.91	343.23	339.50	+3.73
0+49		7.39	344.75	340.65	+4.10
798		6.67	345.47	341.80	+3.67
1+47		4.61	347.53	342.95	+4.58
1+96		3.23	348.91	344.10	+4.81
2+45		1.86	350.28	345.25	+5.03
2+94		0.49	351.65	346.40	+5.25
3+43	361.15	8.09	353.06	347.55	+5.51
792		6.70	354.45	348.70	+5.75
4+41		5.31	355.84	349.85	+5.99
4+90 = DE.		3.90	357.25	351.00	+6.25

SE. B.P. Polk & Arizona

329.95
10.317
340.267
0.28-
339.98 = TP
12.16+
352.147
0.49-
351.65 = TP
9.507
361.157 = K
2.50-
357.65 = TP
0.67+
358.32 = K
12.31-
346.01 = TP
0.73+
346.74 = K
12.40-
334.34 = TP
2.57+
336.91 = K
5.38-
331.53
331.51 = BM
0.02 = Error

chk on SE. B.P. Howard & Arizona

Staker
p. 28

SEWER CONST. IN LOPHO
Bet. McColl and Owen st.
" Rose crans " San Antonio sts.

0+00 = exist. sewer @ McColl st.					
= 2 MH to be const.	21.47	12.88	8.59	4.00	+4.59
0+50		12.04	9.43	5.06	+ 4.37
1+00		7.75	13.72	6.12	+ 7.60
1+50		8.36	13.11	7.18	+ 5.93
2+00	25.87	4.28	21.59	8.24	+ 13.35
2+50		4.24	21.63	9.30	+ 12.33
3+00		4.31	21.56	10.36	+ 11.20
3+50 = MH @ Nicholas st. = 0+00		5.66	20.21	11.42	+ 8.79
(4-49.9)				8.9	
0+43.9		5.55	20.32	12.31	+ 8.01
1+87.8		5.55	20.32	13.20	+ 7.12
1+31.7		4.95	20.92	14.10	+ 6.82
1+75.6 = DE. 50' W. M. San Antonio	3.40	22.47	15.00		+ 7.47
chk. on End Line Bet 12.58-9)	4.44	21.43			
		21.50 = Ground			
		0.07 = difference OK			

offset

St. B.P. Rosecrans @ McColl	→ 38.14
	0.29 =
	38.43 = T
	12.57 =
	25.86 = T.K
	6.63 =
	26.49 = T
	12.39 =
	14.10 = T.P.
	7.37 =
	21.47 = T
	1.87 =
	19.60 = T.K
	6.27 =
	25.87 = T

Walker
Mc High
Montgomery
Locky

Change in Grades MEADE Ave.
bet. E.L. 48th and VAN DYKE (See P. 76)
by Per. RMG.

SL. Sta.	SL. Grades	N.L. Sta. west end of 6th St	N.L. Grades
cb P.C. on 48th	348.10	= 8+61.5 Page 76 (1-13.5)	347.92
⊙ = cb PC	348.20	2+75.0 (1-18.5)	347.84
⊙	348.35	299.5 "	347.87
⊙ = 0+00			
⊙ = cb E.C. on Meade	348.45	3+12 "	347.98
0+50 = P.V.C. (2.5) 4	348.60	3+30.5 "	348.18
+44.5	348.75	+49 "	348.46
+68	349.00	+67.5 "	348.84
+91.5	349.50	+86 "	349.28
1+15 = E.V.C. 2-50	350.44	4+04.5 "	349.83
1+65	352.13	+23.0 "	350.45
2+15	355.82	+41.5 "	351.17
2+35 = P.V.C. SE Van Dyke out Meade	357.83		
+65 = cb PC	358.39	+60 "	351.96
⊙	358.60	+78.5 = E.V.C. (39) 7	352.85
⊙ 2 Curve	358.63	5+17.5	354.80
3 = cb E.C.	358.76	+56.5 = cb PC Page 76	356.75
End Return	358.80	⊙ def = 6'07"30"	357.13
		⊙ " = 12'15" = Bk = P.V.C. 8"11"15"	357.60
		⊙ " = 20'26"15"	357.90
		⊙ " = 28'37"30"	358.09
		⊙ " = 35'48"45"	358.10
		⊙ = 45'00" NE Van Dyke	
		⊙ = End Return = E.V.C.	357.87
		P.C. on Van Dyke	
		N.W. Cor. Meade	358.00
		⊙ def = 89'15"	358.36
		⊙ " = 16'22"30"	358.72
		⊙ " = 24'33"45"	359.08

change in location of station see P. 22

389.53 = T.P. on 8th Page 76
1199.1
351.57 - X 354.06 = X P-65
0.81 -
350.66 = TP
1110.1 N 347.92 347.84 347.87 347.98 348.18 348.46 348.84 349.28 349.83
357.76 - X
6.14 6.27 6.17 6.08 5.98 5.60 5.22 4.78 4.69
6.23 6.83 7.86 7.60 7.93 8.53 7.77 10.41 1.55
-0.3 -0.6 -1.6 -1.52 -2.05 -2.93 -2.7 -5.63 +0.13

S 349.45 348.60 348.75 349.00 349.50 350.44 = see below out
3.67 2.72 2.77 2.51 2.02 1.08
7.27 6.88 3.09 4.14 2.38 2.11
-4.00 -3.96 -0.82 -1.67 -0.36 -1.03 -0.8

N 350.45 351.17 351.76 352.85 354.80 356.75 357.13 357.50 357.90
1.07 0.34 7.80 8.91 6.96 5.01 2.63 4.96 3.86
1.18 0.57 10.16 8.92 6.36 3.92 0.47 2.32
-0.11 -0.04 -0.36 -0.01 +0.6 +0.1 -0.06 out

S 353.13 355.82 357.83 358.59
8.63 5.94 3.93 3.37
7.35 4.83 3.01 2.68
-0.72 +1.11 7.02 7.07

N 353.09 358.10 357.87 358.00 358.36 358.72 359.08
3.67 out 3.87 3.76 out 3.01
-0.24 +0.22 +3.62 +2.66

354.52 = X from P. 66
167 -
350.85 TP
71.5 -
360.9 - X
Finish stakes

N 347.84 347.87 347.98 348.18 348.46 348.84 349.28 349.83 350.45
6.68 6.75 6.54 6.34 6.06 5.68 5.24 4.69 4.07

S 348.10 348.20 348.35 348.45 348.60 348.75 349.00 349.50 350.44 352.13
6.42 6.32 6.17 6.07 5.92 5.77 5.52 5.02 4.08 1.39

N 351.17 351.96 352.85 354.80 356.75 357.13 357.50 357.90 358.09
3.35 3.56 1.67 7.29 5.34 4.96 4.59 4.19 4.00

S 355.82 357.83 358.39 358.60 358.68 358.76 358.80
6.27 4.76 3.70
6.38 3.71
6.01 3.67
E.C. 36.74

N 358.10 357.87 358.00
3.99 4.22 8.29

358.80 End cb SE Cor. Van Dyke & Meade
731
366.9 - X

MEADE 4c Cont.
from P-41

N.L. Sta	N.L. Grade
④ def = 32°45' = Bk - PVC	359.45
⑤ " = 38°52'30" = 0+00 P. 77	359.60
⑥ = E.C. 66 P. 45 =	359.80
0+7.5 = Bk	359.96
+15 = Bk = E.V.C	360.12
-148.09 = ^{sec} P. 98 77	360.65
PC	358.00
1 Δ = 17°37'	358.36
2 35°14'	358.72
3 52°51'	359.08
4 = PVC 70°26'	359.45
5 = Bk 80°14'	359.60
6 = Bk 90° = E.C.	359.80

36176 - T from P-41
See Combination Levels on 77

42

N	359.45	359.60	359.80	359.96	360.12
	731	out.	196	180	15
	02		029	022	022
	-1.9		+1.67	+1.6	+1.3

36179 = T from P-41

Finish Stakes

N	358.36	358.72	359.08	359.45	359.60	359.80	359.96	360.12	360.65
	793	757	721	684	667	649	633	577	564

SEYER Const. Tract # 1368
 10 Blks. 44, 43, 42.41
 Bet. Minna & 52nd St.

MH#1 Blk. 48					
= 0+00	384.28	14.82	369.46	364.80	+5.46
- 7-47.14					
0+07.14		10.74	373.54	364.66	+8.88
+94.28		8.04	376.24	365.33	+10.91
1+41.42		5.78	378.50	365.99	+12.51
+88.56		4.43	379.85	366.65	+13.20
2+35.70		4.30	377.98	367.31	+12.67
+82.86		5.53	378.75	367.97	+10.78
3+30 = 2 DMH#2 = 0+00	391.12			368.62	+12.59 = E+Y
6-47.2		9.91	381.21	374.00	+7.21 = North
0+47.2		7.00	384.12	368.95	+15.17
+99.4		5.77	385.55	369.28	+16.07
1+41.6		5.03	386.09	369.61	+16.48
+88.0		5.24	385.88	369.94	+15.94
2+36		5.25	385.87	370.27	+15.60
+83.2		5.85	385.27	370.60	+14.67
1-36.8		6.08	385.16	370.86	+14.30
3+20 = 1 H 16 th St	391.24			378.00 = N	+7.10
1-10.44		6.14	385.10	370.93	+14.17
3+30.44 DMH#3 = 0+00		4.68	386.56	371.00	+15.56
(1-10.44)		4.96	386.28	371.29	+14.99
0+10.44 = 1 H 16 th St		4.81	386.43	371.58	+14.85
(3-41.66)		4.76	386.48	371.87	+14.61
0+52.10		4.63	386.61	372.08	+14.53
+93.76		5.34	385.90	372.29	+13.61
1-35.42 = 1 R 15 th St		6.03	385.21	372.61	+12.60
(2-30.15)		6.32	384.92	372.93	+11.99
1+65.57 = 1 5 th St		7.90	383.34	373.50	+7.84
1+95.74 = 1 5 th St = 1 5 th St				373.25	+10.09 = W
2+40.74					+7.84 = N + South See P-46
2+85.74					
3+30.74 = MH#4 Alley Blk. 41					

45

Polys.
 Elev. Stub 1465 Book 1199-54 = 386.50
 378
 384.28
 8.65 =
 385.13-TP
 7.91
 391.12 = X
 7.19 =
 383.93
 383.94 = Stub
 0.01 = Error

From here, Used Elev. stub = 383.94
 7.35
 391.29 =

Note: For South Cut See P-48

Elev. stub 2482 = 385.27
 5.97 =

For Chk out See
 Continuation boards
 on Page 46

SKYER Const. in Alley Blk. 41
 Bot 51st + 52nd

D.E. 52' South MH#4

= 0+00	391.24	11.15	380.07	374.02	+ 6.07
+52 = MH#4 = 0+00		7.90	383.34	373.50	+ 9.84
(8-17)		5.97	385.27	373.83	+ 11.44
0+49		5.45	385.79	374.16	+ 11.63
+94		5.06	386.18	374.49	+ 11.69
1+41		5.02	386.22	374.82	+ 11.40
+88		5.25	385.99	375.15	+ 10.84
2+35		5.39	385.85	375.48	+ 10.37
+82		9.38	384.23	375.81	+ 8.42
3+29	393.61	12.14	381.47	376.13	+ 5.34
3+76 = MH#5		11.67	381.94	376.35	+ 5.59
1-32					
4+08 - D.E.					

HT₁ from Page 45 = 391.24

539-
 385.85 = TP
 2.761
 393.61 = H
 For ch. out see continuation
 Levels from MH#6 East on P-47

MH#5

LINE SYEST Above MH#5 Lot 6 Blk. 41

= 0+00	393.61	12.14	381.47	376.40	+ 5.07
0+38.33		8.20	385.41	377.93	+ 7.48
+76.66		6.63	386.98	379.46	+ 7.52
1+15 = D.E.		6.33	387.28	381.00	+ 6.28

← = (Branch) = (start line) main line 27 lower

SEWER Const. in Alley Bk. 42
 Bet #Hodens & 51st

95' N.N.L. Trojan	47				
= 0+00 = DE.	391.37	13.90	377.57	372.50	+ 4.97 + 5.07
+ 51.66		11.32	380.15 380.05	372.04	+ 8.01 + 8.11
1+03.33		8.46	383.01 382.91	371.57	+ 11.34 + 11.44
+ 55 = DMH#3 = 0+00		6.37	385.10 386.81	378.00-N	+ 14.00 ✓
7-50.43		4.66	386.71	378.55	+ 7.10 370.93 Elev. Flon E-W
0+50.43		4.10	387.37 387.27	379.11	+ 8.16 + 8.26
1+00.86		3.52	387.95 387.85	379.66	+ 8.19 + 8.29
+ 51.29		3.32	388.15 388.05	380.22	+ 7.83 + 7.93
2+01.72		3.00	388.47 388.37	380.77	+ 7.60 + 7.70
+ 52.15		3.19	388.28 381.88-S	381.33	+ 6.95
3+02.58	-Δ 90° Rt. 393.61	5.26	388.35	382.20-E	+ 6.15
+ 53 = MH#6 = 0+00		4.60	389.01	382.58	+ 6.43
0+58.33		4.68	388.93	382.97	+ 5.96
+ 76.66		4.58	389.03	383.35	+ 5.68
1+15 = DE.					
Lots 1, 2, 3, 4, 5 Bk. 42					
2 #1/2	393.61	5.03	388.58	381.85	+ 6.73
= 0+00		5.38	388.23	382.24	+ 5.99
+ 38.33		5.38	388.23	382.62	+ 5.61
+ 76.66		5.43	388.18	383.00	+ 5.18
1+15 = DE.					

Elev. cut stub DMH#3 P.45 = 385.10
 637
 391.47
 312
 Chk. on cut stub MH#6 = 388.35
 388.35
 0.00

H.I. from P-46 = 393.61
 #6 cut 5.26
 T.P. on MH#6 stub = 388.35

SEWER Const. Alley Blk. 43
 Tract # 1368 Bet. 50th and Altadena St.

48

45' N.W. Corner

= 0+00 = D.E.	385.94	11.49	374.45	370.23	+ 4.22
+ 50.5					
0+50.5		8.55	377.39	369.87	+ 7.52
1+01		6.41	379.53	369.52	+ 10.01
+ 51.5		5.09	380.85	369.17	+ 11.68
2+02 = DMH#2 = 0+00	4.73	381.21	368.87 = South	368.62 = East	+ 12.37
6-46.83			374.00 = North	374.00 = North	+ 13.59
0+46.83	4.83	381.11	374.60		+ 6.51
+ 93.66	4.48	381.46	375.20		+ 6.26
1+40.5	3.71	382.23	375.80		+ 6.43
+ 87.3	2.85	383.09	376.40		+ 6.69
2+34.1	1.28	384.66	377.00		+ 7.66
+ 81 = MH#7 = 90° St = 0+00	390.49	4.66	385.83	377.60 = South	+ 8.23
0+38.33	3.33	387.16	377.90 = East	377.90 = East	+ 7.93
+ 76.66	2.72	387.77	378.93		+ 8.23
1+15 = D.E.	2.56	387.93	379.96		+ 7.81
			381.00		+ 6.93

Elev. cut slab DMH#2 - P. 45 = 381.21

473+
 385.94 -
 003 -
 385.91 -
 458 +
 390.49 -

See P-45

✓

Lots 1, 2, 3, 4, and 5 Blk. 43

Alley	390.49	4.75	385.74	377.50	+ 8.24
= 0+00					
+ 38.33	6.09	384.40	377.88		+ 6.52
+ 76.66	6.42	384.07	378.27		+ 5.80
1+15 = D.E.	7.24	383.25	378.65		+ 4.60

Walker
Rudolph
Shard
9-17-28

Alley Grades Blk 34 Park Villa

Bet 31st & Herman

From N.W. Myrtle to S.W. Dwight Sts

W.L. Ch.	W.L. Grades	Col. Sta.	E.L. Grades
N.W. Myrtle = 0100	326.60	↑	326.60
+46.66	326.86		326.86
+93.32	327.13		327.13
+140 = Brk (8-47.5)	327.40	Brk.	327.40
+187.5	328.12		328.15
2+35.	328.85	Station Square	328.90
+83.5	329.57		329.65
3+31	330.30		330.40
+78.5	331.02		331.15
4+25	331.75		331.90
+72.5	332.47		332.65
5+20 = P.V.C.	333.20	P.V.C.	333.40
+40 Brk	333.40	Brk.	333.60
+60 "	333.50	"	333.60
+80 "	333.40	"	333.40
6+02 = S.W. Dwight	333.10	↓	333.10

328.99 = N.W. B.P. Upper 431 St

314 ±

332.13 = T

5.41

326.72 = TP

111 ±

333.83

17 ±

332.07 = TP

58 ±

337.61 = T

339 ±

334.02 = TP

486 ±

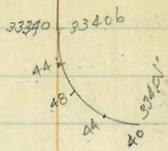
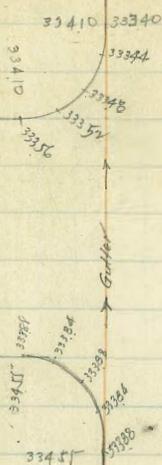
338.88 = T

FL	326.60	326.86	327.13	327.40	328.15	328.90	329.65	330.40	331.15
	553	677	670	643	568	443	418	343	446
	634	552	659	480	529	456	403	222	521
		+1.95	+0.16	+1.63	+0.37	+0.37	+0.15	+1.21	+1.21
FL	326.60	326.86	327.13	327.40	328.12	328.85	329.57	330.30	331.02
	553	677	670	640	571	498	426	353	6.59
	634	552	663	475	421	480	419	386	6.18
		+0.44	+1.07	+0.65	+1.50	+0.18	+0.07	+0.07	+0.41
FL	331.90	332.65	333.40	333.60	333.60	333.40	333.10		
	571	496	421	478	528	548	578		
	313	239	376	469	262	452	577		
		+2.58	+2.57	+0.45	+0.59	+3.26	+0.96		
FL	331.75	332.47	333.20	333.40	333.50	333.40	333.10		
	586	514	441	528	538	548	578		
	543	447	468	550	489	466	579		
		+0.67	-0.21	-0.02	+0.99	+0.82	0.01 Low		

42nd St Paving
Bet. Landis & Thorn sts.

54

DWIGHT



57



N.Y.C.P. DWIGHT
Prod 42nd St
33471 = BM
434
337.05 = T

4200

34131 34141

34115 34100

57

LANDIS

51

THORN

57

Raked from a East end CB.
to 11' East of Prop. Line

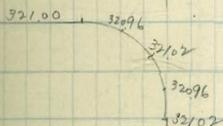
16' N. Next C.B.

1+3333 31525

0+3333 31860

0+00

MIRTL



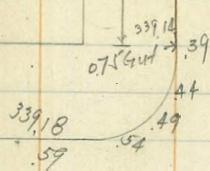
57

N.Y.
321.62 = BM.
M₁+16+422

4200

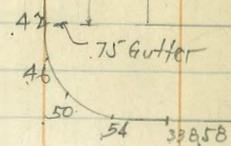
4319 St. Parking
bed lands + 14 ft high

300' to Bk



54

300' to Bk



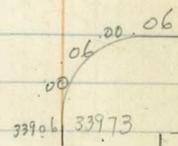
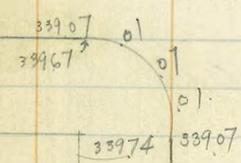
31873

53

31903

DWIGHT

St.



339.77 - Bk
Dwight 143rd

31986

31959

31996 31933

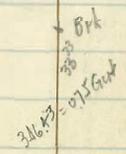
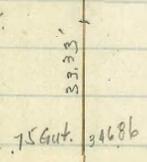
31933 31971

300'

300'

Bk.

4319



347.65 - Bk
4.25 +
331.90 = X

Bk.

331.92 - 331.25
15'
332.41 - 331.74
15'
332.09 - 332.22

331.94
331.25 = EVC
331.74 332.42
332.22 332.09
PVC

Bk.

300'

300'

LANDIS

St.

Walker
Replinger
Shaw
9-25-28

CURB LEVELS ON 4229 ST
from S.W. Myrtle to N.W. THOMAS ST.

324.37

50

2+66.66

			W.R.P. Myrtle + 4200			
	2.75	324.37	321.57	E	12.94	311.43
	S.W. Myrtle = 0+00			W	12.97	311.40
W	3.78	320.59		T.P. 132	312.66 1303	311.34
E	3.77	320.60		3+00		
	0+33.33			W	2.89	310.27
W	5.20	319.17		E	2.40	310.26
E	5.11	319.26		3+33.33		
	0+66.66			E	3.53	309.13
E	6.26	318.11		W	3.60	309.06
W	6.29	318.08		3+66.66		
	1+00			W	4.71	307.97
W	7.37	317.05		E	4.67	307.99
E	7.24	317.13		4+00		
	1+33.33			E	5.81	306.85
E	8.45	315.92		W	5.81	306.85
W	8.49	315.88		4+33.33		
	1+66.66			W	6.98	305.68
W	9.53	314.84		E	6.96	305.70
E	9.54	314.83		4+66.66		
	2+00			E	8.10	304.56
E	10.66	313.71		W	8.10	304.56
W	10.70	313.67		5+00		
	2+33.33			W	9.38	303.48
W	11.84	312.53		E	9.13	303.43
E	11.84	312.53				

5433.33

E 10.38 302.28
 W 10.82 301.84

5466.66

W 11.84 300.82
 E 11.52 301.14

5495

E 12.45 300.71
 W (5489) 12.98 299.68
 T.P. 2.85 302.88 12.63 300.03

Grades on 42nd of Thorn St.

N.E. cb. E.O.	302.88	2.33	300.55	300.00	0.55
S.E. End cb.		12.49	290.39	299.40	-9.0
SW "		6.66	296.22	299.00	-2.78
N.W. E.Curb Return on Thorn		3.04	299.84	300.00	-0.16
" " " " 42nd		2.85	300.03	300.00	+0.03

300.58 = Elev. cut slab at 00 cb. Inlet #1 page 50
 518+
 300.76 = X
 12.93 =
 297.83 = T.P. See continuation Levels on P. 50

	NE on 42nd			
End cb	Return	6 PC.	EC	End cb on Thorn
300.00	300.00	300.00	300.00	300.00
576	576	576	576	479
	488	537	523	433
	+0.88	+0.39	+0.53	+0.46
End	PC	EC	End cb.	
300.00	300.00	300.00	300.00	
576	576	576	576	
574	569	544	592	
100V	+0.07			-0.18
				Out.

30479 = X
 300.00 End Return
 300.00
 479
 433
 +0.46 +0.34

-EC on Thorn
 N.W. 300.00 300.00
 479 479
 513 508
 -0.34 -0.29

John H. ...
 10-8-28

(EAST) Alley Paving Blk. 129 Univ. H + S
 Bet. E. L. Cajon & Harvard Ave.
 From E.L. Florida to N.L. Alabama St.

N.L. Sta	N.L. Grades	St. Sta.	St. Grades
= 0+00	294.70	↑	Bk. 294.40
+30 = Bk.	293.00	↑ Stat. same as N	" 292.70
+50 = "	292.10		" 291.80
+70 = "	291.70		" 291.50
2-40	291.50		" 291.30
1+10	291.50	↓ Stat. same as N	" 291.10
+50 = Bk.	291.30		" 290.90
+70 = "	291.50		" 291.30
2-40	292.85		" 292.65
2+10	292.85	↑ Stat. same as N	Bk. 294.00
+50 = Bk.	294.20		" 296.00
2-30	296.25		" 296.00
2+80	296.25		" 298.00
3+10 = N.L. Alabama	298.30		

300.65 = N.L. BP E. L. Cajon & Florida
 0.28 +
 300.93 = N
 7.57 -

Blk.	Blk.	Blk.	Blk.	Blk.	Blk.	Blk.	Blk.	Blk.	Blk.
29136 = T.N.L.	29470	29300	29210	29170	29150	29130	29150	29285	
5837	623	773	880	549	567	589	567	434	
29719-T	550	618	815	997	561	510	475	376	
679 -	+0.73	+1.65	+0.67	+0.52	+0.04	+0.79	+0.75	+0.58	
29690-T	Bk.	Bk.	Bk.	Bk.	Bk.	Bk.	Bk.	Bk.	
29440	29270	29180	29150	29130	29110	29090	29130	29265	
622 +	653	823	913	567	589	607	629	589	454
30273-T	683	805	915	587	570	475	551	511	192
115 -	-0.90	+0.18	-0.02	-0.13	+0.19	+0.14	+0.78	+0.78	+1.62
30098-T	Bk.	29420	29625	29830					
911 -	2.99	648	443		29900 = top of				
31059-T	2.28	528	4.5		373				
379 -	+0.71	+1.50	4.5		395				
30660	Bk.	Bk.	Bk.		0.77 Low.				
30657 = Sh.	29400	29600	29800						
009-T	319	673	4.75						
	284	554	4.65						
	+0.35	+1.19	0.8 High						

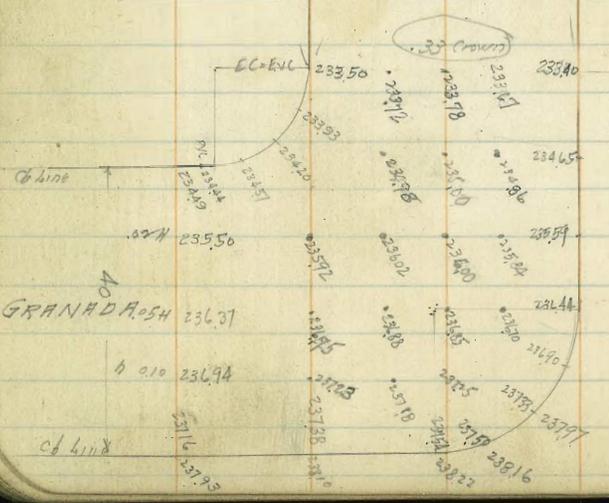
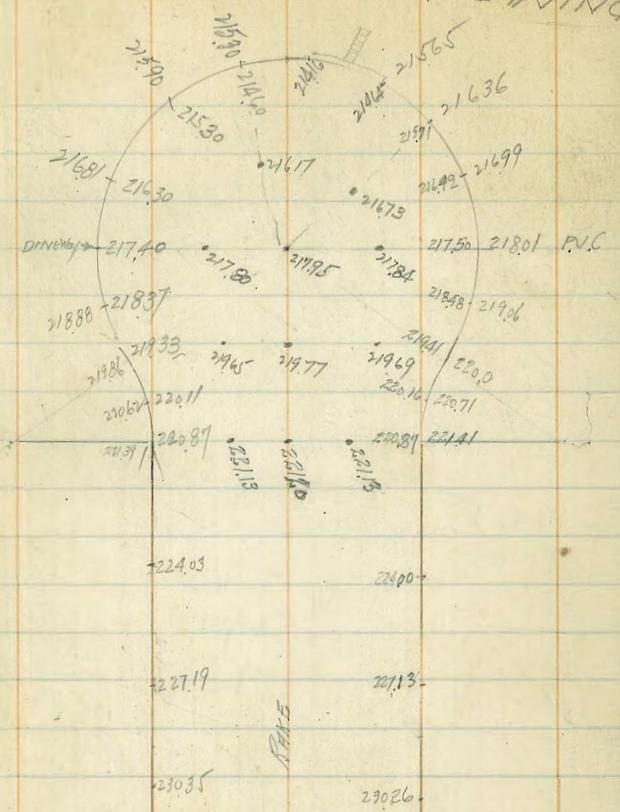
On NE. BP E. L. Cajon & Alabama
 299.69 -
 291.10
 8.53
 7.82
 + 0.77

1466' N &
 = 0+00

Culvert For Above Alley	Flow
30093 9.05 291.88 289.40	+ 7.48
+ 29.32 = End 11.24 289.69 289.00	+ 0.69

HAYTHORNE ST PAVING

Walker
Ruphner
Rocky
Hood
10-26-28



Walker
Prop. 11/11/1911
Moulton
12-23-28

JOHNSON Ave Paving etc.

SEWER Const. EAST of 10th St.

Sta.	Dist. East of MH	Flow Line
+0+00	592.32	281.50
+33.5	4.46	287.86
+67 = MH #1 (1-20')	4.93	287.39
+1+07 = Plug end	5.93	286.39
	4.52	287.80

SW. B.P. Handricks ^{and} Richmond = 288.48
 1.25+
 200.43-
 0.85-
 Richmond
 SW. Cap. back on ST line fixed on 1.5' SW WCB = 279.58-TP
 2.65+
 302.23-
 10.88-
 2012 Back on N = 291.35-TP
 7.60+
 298.95-
 8.73-
 290.02-TP
 2.30+
 292.32-
 9.88-

on ELY line
 CURB Const. 12 Johnson Ave North of Lincoln Ave

Sta.	Dist. East of MH	Flow Line
+0+00 = Equip. on curb		292.00
+36 = P.C. 4.28°35' = turned 3 Parts		291.83
⊙ def = 1°45'30"		291.87
⊙ 9°31'40"		291.85
⊙ = E.C. 14°17'30" (8-2837)		291.85
+0+23.37		291.77
+46.74		291.69
+70.11		291.61
+93.48		291.53
+1+16.85		291.45
+40.22		291.37
+1+63.6		291.29
+1+76		291.25
+1+87 = P.C. 20°15' = A (2 parts)		291.22
⊙ 5°03'45"		291.20
⊙ = E.C. 10°07'30"		291.20
+0+28.25		291.10
+56.5 = East end curb Inlet. #1		291.08
+66.5 = " " " " #2		291.05

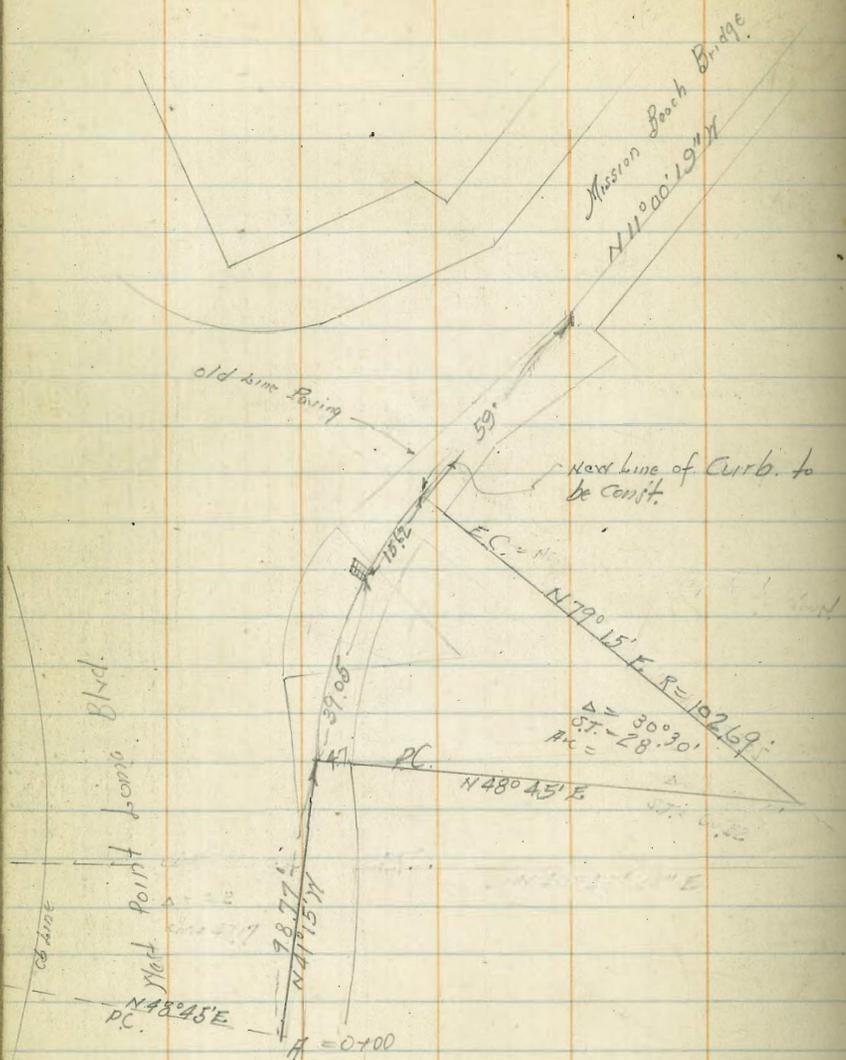
291.35 = above TP on Rock
 3.6 ELY line at Lincoln + Hayes
 29.61-
 4.56 4.8 4.7 4.74 4.76 4.84 4.92 5.00

N.W. B.P. Johnson + 10th = 282.44
 E.C.
 291.53 291.45 291.37 291.29 291.22 291.20 291.10 290.99 290.99
 5.08 5.16 5.24 5.32 5.36 5.39 5.41 5.51 5.62 5.74
 5.60 5.60
 1.002 0.02

(1.165)
 +0+83 = P.C. 291.00
 +87.01 = E 290.99

Walker
12-29

Curb Location South end Mission Beach
Bridge and Point Loma Blvd.



N.F.P.P. Supper Club + Mt. Point Blk. 1.84
561-
7.45-

R = 173.05'
GRADES For new line paving from P.C. to E.C.
= P.C. @ @ @ = Low Point

184 - N.F. Mt. Point Supper Club

CURB GRADES												
506												
6.90 = T												
3.73												
3.17 T	350	317	284	252	224	196	168	140	112	84	56	28
5.26	4.93	3.73	2.06	1.38	4.26	2.54	1.67	1.10	4.77	4.68	4.59	3.79
8.43 = T					4.30	3.79	3.76	4.20				
					7.008	10.75	10.86	10.50				

Stations	Curb GRADES
PC. R 93816-6 = 0+00	3.50
+32.92	3.17
+65.84	2.84
+98.77 P.C. R. 10269	2.52
①	2.44
②	2.36
③	2.28
④	2.20
⑤ = Low Point = Proposed catch Basin	2.13
⑥	2.22
⑦ = E.C.	2.31
59'	
↓ S end of bridge	3.01

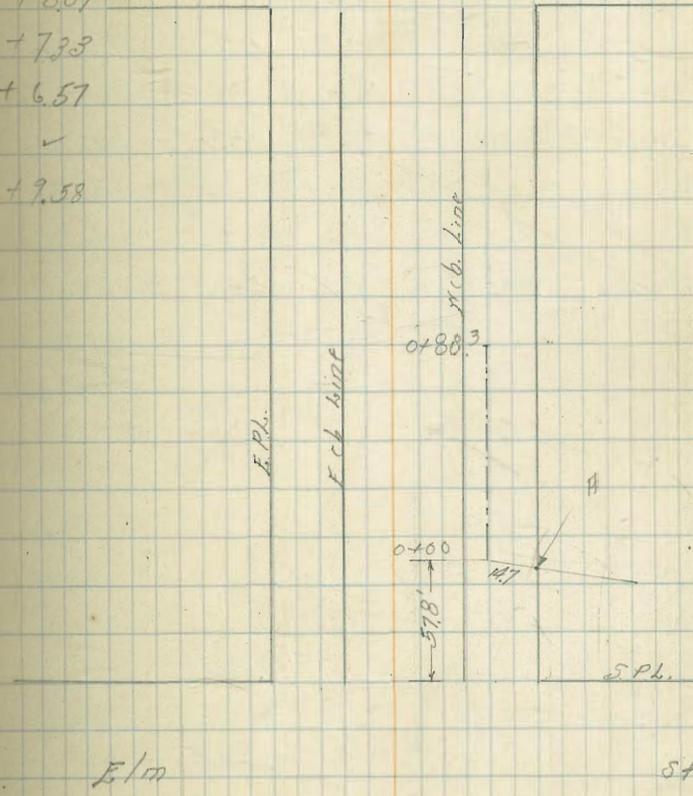
Y. W. K.
 R. W. K.
 J. W. K.
 1-5-29

LEVELS For Sewer Line

Bot Elm and DATE
 on W Side 4th St. Bot. c. b. 4th St.

TP	4.40	134.98	9.38	130.58	Flow Line	DATE	ST.
57.8' S.S. Elm = 0+00			2.70	132.28	123.20	+ 9.08	
+23.5			3.94	131.04	122.97	+ 8.07	
+47.1			4.91	130.07	122.74	+ 7.33	
+72.8			5.93	129.05	122.48	+ 6.57	
+88.3 = End of Pipe			12.65	122.33	122.33	✓	
# on West				132.92	123.34	+ 9.58	

N. W. B. P. Elm
 and DATE



Elm

st.

Walker
Mr. Duff
Montgomery
books 1/17/28

Alley PAVING Blk 125 Univ. Hts.
Bk. Georgia and Florida
From N.W. UNN. to St. Lincoln Ave's

N.W. Sta.	N.W. Grade	Elev. Sta.	E.L. Grades
= 0+00 (6-40')	314.00		313.80
+40	312.99		312.83
+80	311.97		311.88
1+20	310.96		310.91
+60	309.94		309.94
2+00	308.92		308.97
+40 = P.V.C.	307.90		P.V.C. 308.00
+60 = Bk.	307.20		Bk. 307.20
+80 = Bk.	306.00		" 306.00
3+00 = Bk. - E.V.C.	304.60		E.V.C. 304.60
(6-399)			
3+29.9	301.65		301.62
+79.8	298.70		298.65
4+19.7	295.75		295.67
+59.6	292.80		292.70
+99.5	289.85		289.72
5+29.3 = Bk.	286.90	5+39.3	286.75
+59.3 = Bk.	285.60	+49.3 = Bk.	286.00
+79.3 = "	284.80	5+69.3 = Bk. - sup. ch.	284.80
+99.3 = St. Lincoln	285.00	5+79.3 = Bk.	284.30
		+99.3 = St. Lincoln	283.60

elevation same as West

336.41 = Bk. Univ. + Georgia

4

Sta.	Grade	Grade	Grade	Grade	Grade	Grade	Grade
312.99 - TP	312.99	311.97	310.96	309.94	308.92	307.90	- P.V.C.
311.97 - TP	311.97	310.96	309.94	308.92	307.90	306.90	
310.96 - TP	310.96	309.94	308.92	307.90	306.90	305.90	
309.94 - TP	309.94	308.92	307.90	306.90	305.90	304.60	
308.92 - TP	308.92	307.90	306.90	305.90	304.60	303.60	
307.90 - TP	307.90	306.90	305.90	304.60	303.60	302.60	
306.90 - TP	306.90	305.90	304.60	303.60	302.60	301.65	
305.90 - TP	305.90	304.60	303.60	302.60	301.65	300.60	
304.60 - TP	304.60	303.60	302.60	301.65	300.60	299.60	
303.60 - TP	303.60	302.60	301.65	300.60	299.60	298.70	
302.60 - TP	302.60	301.65	300.60	299.60	298.70	297.70	
301.65 - TP	301.65	300.60	299.60	298.70	297.70	296.70	
300.60 - TP	300.60	299.60	298.70	297.70	296.70	295.70	
299.60 - TP	299.60	298.70	297.70	296.70	295.70	294.70	
298.70 - TP	298.70	297.70	296.70	295.70	294.70	293.70	
297.70 - TP	297.70	296.70	295.70	294.70	293.70	292.70	
296.70 - TP	296.70	295.70	294.70	293.70	292.70	291.70	
295.70 - TP	295.70	294.70	293.70	292.70	291.70	290.70	
294.70 - TP	294.70	293.70	292.70	291.70	290.70	289.72	
293.70 - TP	293.70	292.70	291.70	290.70	289.72	288.70	
292.70 - TP	292.70	291.70	290.70	289.72	288.70	287.60	
291.70 - TP	291.70	290.70	289.72	288.70	287.60	286.70	
290.70 - TP	290.70	289.72	288.70	287.60	286.70	285.60	
289.72 - TP	289.72	288.70	287.60	286.70	285.60	284.80	
288.70 - TP	288.70	287.60	286.70	285.60	284.80	283.60	
287.60 - TP	287.60	286.70	285.60	284.80	283.60	282.60	
286.70 - TP	286.70	285.60	284.80	283.60	282.60	281.60	
285.60 - TP	285.60	284.80	283.60	282.60	281.60	280.60	
284.80 - TP	284.80	283.60	282.60	281.60	280.60	279.60	
283.60 - TP	283.60	282.60	281.60	280.60	279.60	278.60	
282.60 - TP	282.60	281.60	280.60	279.60	278.60	277.60	
281.60 - TP	281.60	280.60	279.60	278.60	277.60	276.60	
280.60 - TP	280.60	279.60	278.60	277.60	276.60	275.60	
279.60 - TP	279.60	278.60	277.60	276.60	275.60	274.60	
278.60 - TP	278.60	277.60	276.60	275.60	274.60	273.60	
277.60 - TP	277.60	276.60	275.60	274.60	273.60	272.60	
276.60 - TP	276.60	275.60	274.60	273.60	272.60	271.60	
275.60 - TP	275.60	274.60	273.60	272.60	271.60	270.60	
274.60 - TP	274.60	273.60	272.60	271.60	270.60	269.60	
273.60 - TP	273.60	272.60	271.60	270.60	269.60	268.60	
272.60 - TP	272.60	271.60	270.60	269.60	268.60	267.60	
271.60 - TP	271.60	270.60	269.60	268.60	267.60	266.60	
270.60 - TP	270.60	269.60	268.60	267.60	266.60	265.60	
269.60 - TP	269.60	268.60	267.60	266.60	265.60	264.60	
268.60 - TP	268.60	267.60	266.60	265.60	264.60	263.60	
267.60 - TP	267.60	266.60	265.60	264.60	263.60	262.60	
266.60 - TP	266.60	265.60	264.60	263.60	262.60	261.60	
265.60 - TP	265.60	264.60	263.60	262.60	261.60	260.60	
264.60 - TP	264.60	263.60	262.60	261.60	260.60	259.60	
263.60 - TP	263.60	262.60	261.60	260.60	259.60	258.60	
262.60 - TP	262.60	261.60	260.60	259.60	258.60	257.60	
261.60 - TP	261.60	260.60	259.60	258.60	257.60	256.60	
260.60 - TP	260.60	259.60	258.60	257.60	256.60	255.60	
259.60 - TP	259.60	258.60	257.60	256.60	255.60	254.60	
258.60 - TP	258.60	257.60	256.60	255.60	254.60	253.60	
257.60 - TP	257.60	256.60	255.60	254.60	253.60	252.60	
256.60 - TP	256.60	255.60	254.60	253.60	252.60	251.60	
255.60 - TP	255.60	254.60	253.60	252.60	251.60	250.60	
254.60 - TP	254.60	253.60	252.60	251.60	250.60	249.60	
253.60 - TP	253.60	252.60	251.60	250.60	249.60	248.60	
252.60 - TP	252.60	251.60	250.60	249.60	248.60	247.60	
251.60 - TP	251.60	250.60	249.60	248.60	247.60	246.60	
250.60 - TP	250.60	249.60	248.60	247.60	246.60	245.60	
249.60 - TP	249.60	248.60	247.60	246.60	245.60	244.60	
248.60 - TP	248.60	247.60	246.60	245.60	244.60	243.60	
247.60 - TP	247.60	246.60	245.60	244.60	243.60	242.60	
246.60 - TP	246.60	245.60	244.60	243.60	242.60	241.60	
245.60 - TP	245.60	244.60	243.60	242.60	241.60	240.60	
244.60 - TP	244.60	243.60	242.60	241.60	240.60	239.60	
243.60 - TP	243.60	242.60	241.60	240.60	239.60	238.60	
242.60 - TP	242.60	241.60	240.60	239.60	238.60	237.60	
241.60 - TP	241.60	240.60	239.60	238.60	237.60	236.60	
240.60 - TP	240.60	239.60	238.60	237.60	236.60	235.60	
239.60 - TP	239.60	238.60	237.60	236.60	235.60	234.60	
238.60 - TP	238.60	237.60	236.60	235.60	234.60	233.60	
237.60 - TP	237.60	236.60	235.60	234.60	233.60	232.60	
236.60 - TP	236.60	235.60	234.60	233.60	232.60	231.60	
235.60 - TP	235.60	234.60	233.60	232.60	231.60	230.60	
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232.60 - TP	232.60	231.60	230.60	229.60	228.60	227.60	
231.60 - TP	231.60	230.60	229.60	228.60	227.60	226.60	
230.60 - TP	230.60	229.60	228.60	227.60	226.60	225.60	
229.60 - TP	229.60	228.60	227.60	226.60	225.60	224.60	
228.60 - TP	228.60	227.60	226.60	225.60	224.60	223.60	
227.60 - TP	227.60	226.60	225.60	224.60	223.60	222.60	
226.60 - TP	226.60	225.60	224.60	223.60	222.60	221.60	
225.60 - TP	225.60	224.60	223.60	222.60	221.60	220.60	
224.60 - TP	224.60	223.60	222.60	221.60	220.60	219.60	
223.60 - TP	223.60	222.60	221.60	220.60	219.60	218.60	
222.60 - TP	222.60	221.60	220.60	219.60	218.60	217.60	
221.60 - TP	221.60	220.60	219.60	218.60	217.60	216.60	
220.60 - TP	220.60	219.60	218.60	217.60	216.60	215.60	
219.60 - TP	219.60	218.60	217.60	216.60	215.60	214.60	
218.60 - TP	218.60	217.60	216.60	215.60	214.60	213.60	
217.60 - TP	217.60	216.60	215.60	214.60	213.60	212.60	
216.60 - TP	216.60	215.60	214.60	213.60	212.60	211.60	
215.60 - TP	215.60	214.60	213.60	212.60	211.60	210.60	
214.60 - TP	214.60	213.60	212.60	211.60	210.60	209.60	
213.60 - TP	213.60	212.60	211.60	210.60	209.60	208.60	
212.60 - TP	212.60	211.60	210.60	209.60	208.60	207.60	
211.60 - TP	211.60	210.60	209.60	208.60	207.60	206.60	
210.60 - TP	210.60	209.60	208.60	207.60	206.60	205.60	
209.60 - TP	209.60	208.60	207.60	206.60	205.60	204.60	
208.60 - TP	208.60	207.60	206.60	205.60	204.60	203.60	
207.60 - TP	207.60	206.60	205.60	204.60	203.60	202.60	
206.60 - TP	206.60	205.60	204.60	203.60	202.60	201.60	
205.60 - TP	205.60	204.60	203.60	202.60	201.60	200.60	
204.60 - TP	204.60	203.60	202.60	201.60	200.60	199.60	
203.60 - TP	203.60	202.60	201.60	200.60	199.60	198.60	
202.60 - TP	202.60	201.60	200.60	199.60	198.60	197.60</	

Culvert #7 = 95' 8" Sewer Pipe for Drain
Flow Line Elev

End of line = 0+00	352.22	7.07	345.15	337.00	+8.15
+22.5 = R+6326'	351.35	5.65	346.57	337.47	+9.10
(3-36.3)					
0+58.8		5.37	346.85	338.24	+8.61
		6.22	345.13		+6.13 Reset
0+95.1 = End of line		7.82	344.40	339.00	+5.40

H.I. from P-66 = 352.22
12.97
339.25 = T.P.
1.314
340.60 = H
1.08
339.52
339.55 = JUEGERS
0.17 = diff.

Culvert #6 = 40' 18" 60" Pipe
Bottom Box

Above 0+00 #7 = 0+00 #6	351.35	5.92	345.43	337.50	+7.93 = Flow Line Box
		5.27	346.08	337.00	+9.08
+35 = Ecb. line = 1 End of End Pipe				338.00	

Culvert #5 = 127.5' of 24" Con. Pipe

Above 0+00 #6 = 0+00	352.22	7.07	345.15	337.00	+8.15
+40		8.68	343.54	334.80	+8.74
+80 = L+1825'	340.60	7.44	333.16	332.60	+0.56
1+27.43 = 1/2 Cleanout #2	330.00			330.00	+1.64

Storm Drain #2

1/2 Above cleanout #2 = 0+00	340.60	8.96	331.64	330.00	+1.64
+27.5		11.30	329.30	328.50	+0.80
+55 = End Pipe		13.17	327.43	327.00	+0.43

Storm Drain #1 = 372.38 of 30" Con Pipe

1/2 Cleanout #2 = 0+00	340.60	8.96	331.64	330.00	+1.64
(8-46.55) at 10		0.82	337.78	330.72	+7.06
0+46.55	352.06	7.14	346.92	331.44	+15.48
+93.10		5.34	348.72	332.88	+15.84
1+39.65		5.44	348.62	334.32	+14.30
+86.2		5.24	348.82	325.75	+13.07
2+27.75		5.41	348.65	337.19	+11.46
+79.30		5.58	348.48	338.63	+9.85
3+25.85		5.71	348.35	340.06	+18.79
3+72.38 = 1/2 Cleanout #1		5.62	348.44	341.50	+16.94

Stations Culvert #1

Flow Line Grades					
Ncb. = 0	355.03 = 17 From P77	5.09	349.94	344.1	+5.84
+00		5.26	349.77	342.50	+7.27
+43.7 = End = Ecb.					

Culvert #2

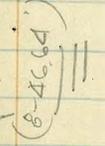
N End Intake #2 = 0+00				342.5
+41 = 1/2 Cleanout #1				341.5

Culvert #3

1/2 Cleanout #1 = 0+00	355.03	5.98	349.05	341.50	+7.55
+18. end		5.52	349.51	342.50	+7.01

Culvert #4 10' 18" Pipe

RM. for Levels from this sta. to 1/2 cleanout #1					
= 350.48					
3.58 =					
354.06 =					
0+00	355.03	7.97	347.06	342.20	+14.76
0+10 = 1/2 Storm Drain #1		7.99	347.04	341.90	+15.14



Exp. Sta.	El. Grade	M.L. Sta.	M.L. Grade
51 N. Meade = cb. PC. S.L. Meade = 0+00	348.30	5 N.S.L. Meade = cb. PC. S.L. Meade = 0+00	348.30
+10	347.10	+10 = Bk.	346.90
+60 = N. End Inlet	346.60	+60 = " = N. End Inlet	346.40
+80 = S " "	346.50	+80 = " = S " "	346.30
+99 = End New cb.	346.53	+99 = End of New cb.	346.35

352.22 = X

El.	348.30	347.10	346.60	346.50	346.53
3.92	5.12	5.62	5.72	5.69	
3.62		5.30		5.1	
3.50					
M.L.	348.30	346.70	346.40	346.30	346.35
3.92	5.32	5.82	5.92	5.87	
	7.28	7.54	5.82	5.67	
	-1.76	-1.72	6.28		
			-0.46		

Change of Above Grades

El. Sta.	El. Grades	M.L. Sta.	M.L. Grades
51. Meade = 0+00	348.20	S.L. Meade = 0+00	348.10
+10 Bk	347.95	+10 = Bk.	347.90
+20 "	347.70	+20	347.60
+40 "	347.10	+40	346.90
+60 = N. end Inlet	346.60	+60 = N. end cb Inlet	346.40
+80 = S " "	346.50	+80 = S " " "	346.40
+99 = Exist. cb	346.53	+99 = Exist. cb.	346.55
1+29	346.33	1+29	346.50
+78	346.36	+78	346.60
2+27 = Bk	346.70	2+27 Bk	346.70

See continuation on p. 27

881 in Bank 12.53-44 f SW. Sph. 10.10 Meade = 350.47

352.22
350.45 = diff Bk on SP level
80' S.E. S.E. Cor Meade 1431

350.47
56.4
356.02
9.55
346.47
5.71
352.22

El. Sta	El. Grade	M.L. Sta.	M.L. Grade
1+07	346.95	2+67	347.25
3+07 = Bk (8-50')	347.20	3+07 Bk	347.80
3+57	348.68	4+57	349.42
4+07	350.16	4+07	351.04
+57	351.64	7+57	352.65
5+07	353.13	5+07	354.27
+57	354.61	+57	355.89
6+57 = N. E. El Cajon	356.10	6+07 = N. E. El Cajon	357.50

353.88 = X from P. 76

El.	348.20	347.95	347.70	347.10	346.60	346.40	346.60	346.64	346.67	346.70
5.68	5.93	6.18	6.78	7.28	7.28	7.24	8.87	8.84		
3556.4 = X				7.28	7.28					
357.87 = X				6.84	6.84					

M.L.	348.10	347.90	347.10	346.90	346.40	346.40	346.50	346.60	346.70
6.12	6.62	6.92	7.62	8.12	7.88	7.38	7.28	7.18	
357.87 = X				6.84	6.84				

El.	346.95	347.20	348.68	350.16	351.64	353.13	354.61	356.10
8.59	8.34	6.86	5.35	3.90	7.41	0.93	3.79	
354.52 = X	8.52	8.22	6.77					
357.87 = X	10.07	1.412	10.07					

M.L.	347.25	347.80	349.42	351.04	352.65	354.27	355.89	357.50
6.63	6.08	6.12	4.50	2.89	1.27	3.07	2.39	
357.87 = X			10.07					
357.87 = X			10.07					

8196-7856

40'

7893 7832

AVE

7813 7859

33rd

St.

7891

7828

7798

7803

7853

MEADE

7840-7775

71

7775 71

MECHANIC

St.

7888-7756

52

48

7740

AVE

8147 8074

8074

8079 8139

8062 - Exit. Av.

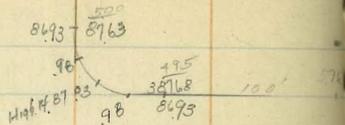
ST.

FALTON

8040 8108

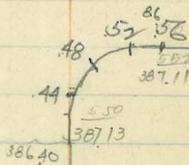
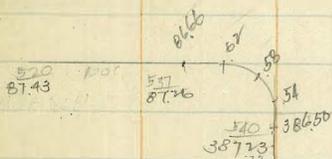
8112 8040

MEADE

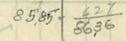
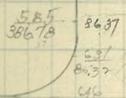


JYIET

H.V.E.

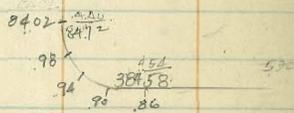
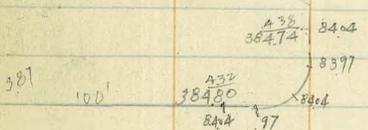


Alley



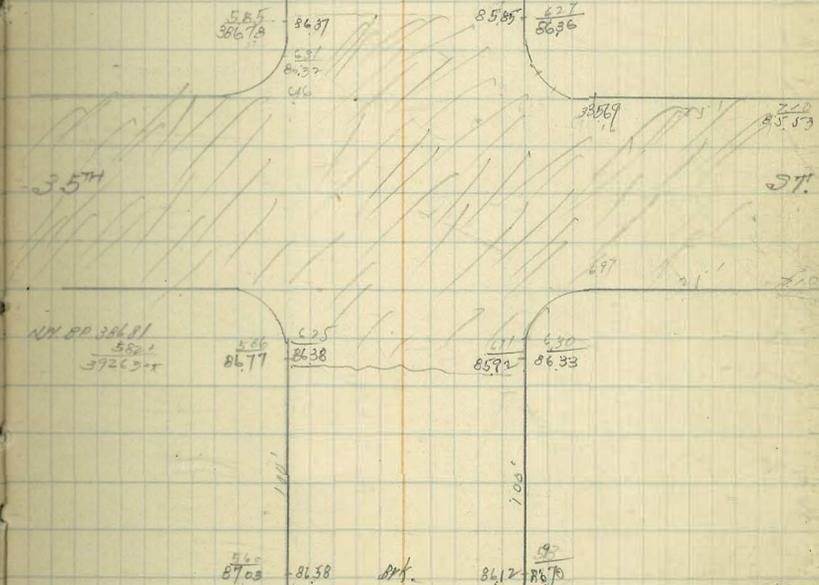
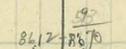
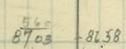
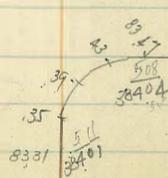
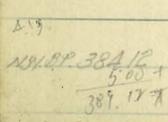
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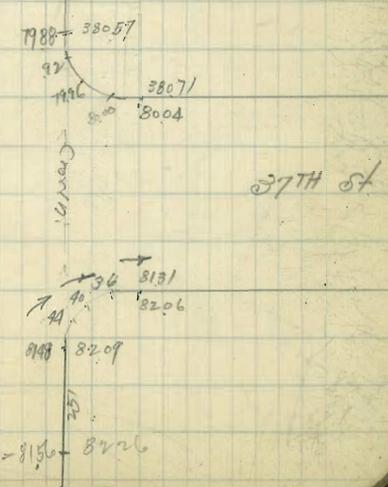
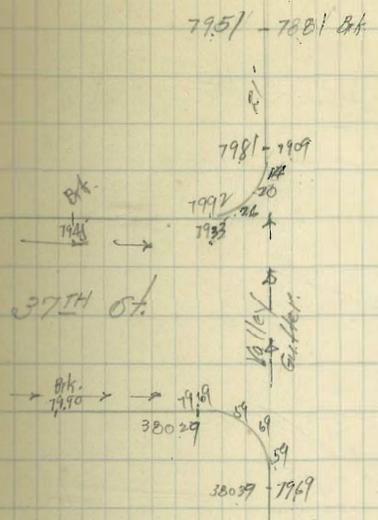
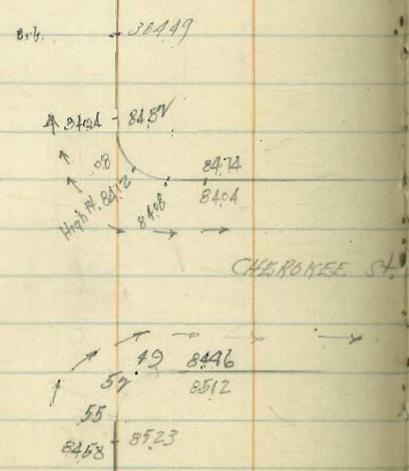
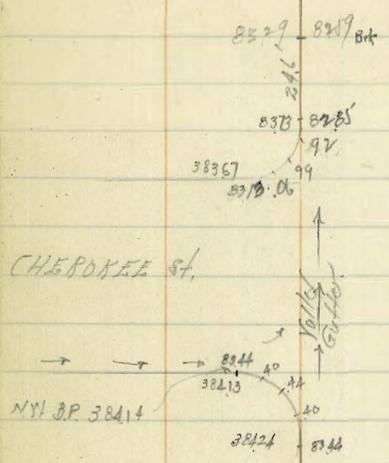
ST.



34TH

ST.





38TH

7379 7308

7224

7266

37438

4864

37734-X

333-

37591-TP

6301

38721-X

37441

7374

Road Survey

7288

7337

Alt. 7302

7353

3165

7574

Crown

37553

37621

37628

37648

37590

78

58

68

68

37573

M. E. LINTOCK

7673

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Crown

31616

20

27

750

40TH

72

St.

6969

6910

6749

6743

6956

6858

6832

6931

39TH

St.

6962

6906

6868

6917

6852

Alt. 6893

6951

MEADE Cont. from P-96

SL. Sta.	SL. Grade	N.L. Sta	N.L. Grades
②	348.35	②	
③ = E.C. on Meade = 0+00 (6-4417)	348.45	③	
0+4417	350.58	4 = End cb. on hinc Meade	
+80.34 1+15 = 88.	349.65 352.17	PC. = End cb. N.W. Cor Van Dyke	
1+32.51	350.00		
1+76.68	353.75		
2+20.85	355.34		
SE. Cor Van Dyke	356.92	3	25' N.W. Van Dyke
+65 = cb. PC. on Meade	358.39	④ = C6 EC. = 0+00 (5-4809)	359.80
Return	358.63	0+4809	360.65
SE. Cor		+96.18	361.41
3 = E.C. on Van Dyke	358.76	+44.27	362.17
SW. Cor		+92.36	362.93
cb. PC. on Van Dyke	359.15		363.70
Return	359.25	2+40	
E.C. = 0+00	359.45		
0+10	359.90		
1+20	360.20		
+30 = 0+00 = E.C. on Meade (6-4417)	360.45	① = E.C.	363.96
0+4417	360.70	② = E.C. curb Return = N.W. Cor Copeland	364.04 = Exit C6
+38.34	361.40	PC. on Copeland	
1+32.51	362.10	①	
+76.68	362.80		
2+20.85	363.50	= 0+00 ③ = E.C. on Meade	364.30
SE. Cor Copeland		(2-40.66')	
+15 = cb. PC. on Meade	364.20	0+40.66	364.33
		+81.32	364.40
		1+22 = SE. Alley	364.44
		+22 = SE. Alley at Top	364.60

Cont. on P-78

359.13 = T from P-76

361.76 = X from P-72

360.92 = TP

367.91 = T

SL	EC	CLPS
349.00	350.53	352.17
10.13	6.55	6.96
16.00	10.7	10.1
5.87	2.15	3.14
		3.42
		-1.88
		+0.38
		0.63
		0.08
		0.55
N 359.88	360.65	361.41
1.96	7.26	6.50
0.39	6.40	5.28
+1.67	1.66	1.02
		1.14
		1.39
		1.12
S 360.00	360.70	361.46
1.76	7.21	6.57
1.63	6.08	5.98
1.01	+1.13	+0.53
		+0.7
		+0.65
		+0.77
		0.04 High.
N 364.30	364.35	364.40
		364.44

FINISH STAKES

N 361.41 362.17 362.93 363.70

358.80 = N.W. end of SE. Van Dyke

365.64 = T

358.80 = E.C. = End P

SL	EC	CLPS
348.25	348.45	349.45
7.25	7.01	6.88
		6.84
J 359.06	359.15	359.25
6.58	6.49	6.39
		6.19
		5.74
		5.44
		5.19

MEADE AVE Cont. from P-77

S.L. Sta. S.L. Grade N.L. Sta. N.L. Grade

S.L. Sta. 36420 36428 36436 36443 36449 36455 36460

①
S.V. Cor Capular rd 36420

② = 0+00 = Cb E.L. on Meade

(2-42.56)
0+42.56 36428

+85.12 = exist cb. 36436 = Miles
(1-17.88')

1+43 = 3' x 1/2" Alley 36443

1+43 = 3' x 1/2" Alley at Prop 36458

(3-35.66')
1+78.66 36449

2+14.32 36455

E.L. 42nd
+50 = Cb pc. 36460

①

②

③ = End of Return.

10-4-28

300.0

X. Section Pile Tin Cans
Intersection 42nd + Thorn

Section A B = 0+100

A = West	11.4	288.6
B = East	4.0	296.0
0+05		
E	4.0	296.0
+5	4.3	295.7
+13	5.9	294.1
X	11.2	288.8
0+10		
X+1	11.2	288.8
+4	5.6	294.4
+9	4.5	295.5
+14	4.4	295.6
E	4.0	296.0
0+15		
E	4.8	295.2
+5	4.6	295.4
+11	5.6	294.4
+15	7.0	293.0
X	11.6	288.4
0+20		
X	11.6	288.4
+5	8.2	291.8
+9	6.5	293.5
+13	5.5	294.5
E	5.2	294.8

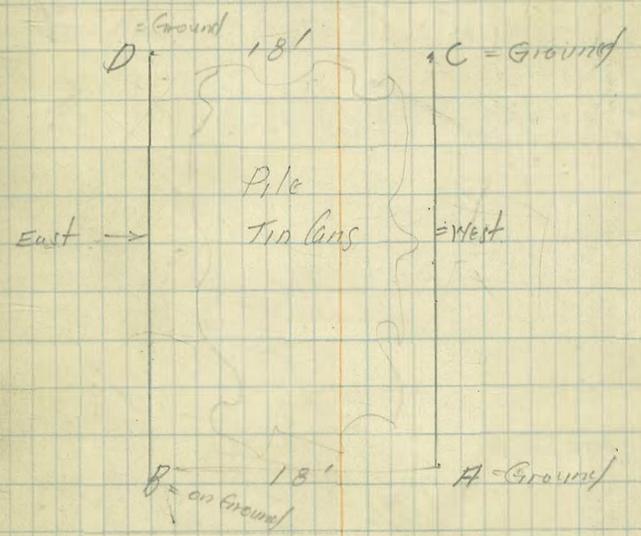
Yardage Figured
 10-4-28
 T.G.H.
 98-16-247

300.0

79

0+25 = D.C

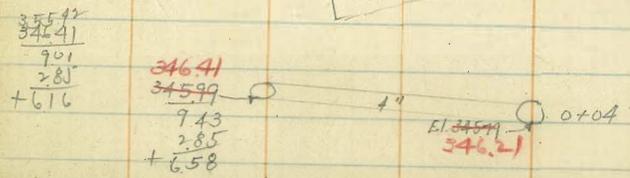
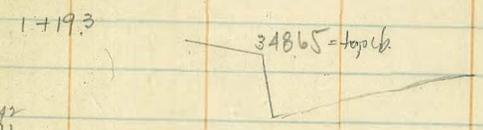
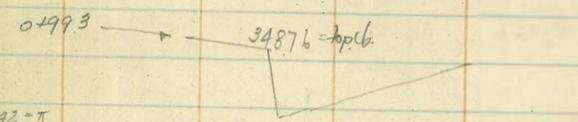
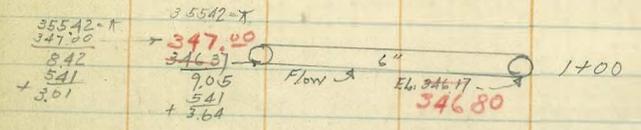
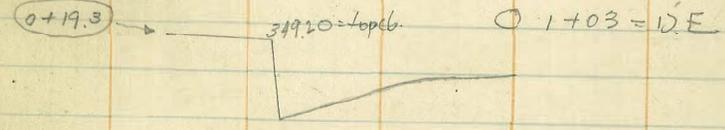
E	5.3	294.7
+5	7.2	292.8
+9	8.4	291.6
+12	10.5	289.5
X	12.0	288.0



SEWER COST MADE AVE
Bet. 43rd and Fairmount.

	π			Flow Line
$\frac{1}{2}$ M.H. 12" 6" 1178	355.42			345.52 = M.H.
= 0+00	355.64 = π	8.44	347.20	346.20 345.77 = 6" line
131.33	355.42	6.50	349.12	346.41 345.91
768.66		6.49	348.93	346.62 346.05
1+03 = D.E.		6.90	348.52	346.82 346.17

Grading Stations



Note: For Sewer Cost in Made bet. Mechanic and 33rd

350 Y P = 81%
194 +
355.42 = π

17.0
13.21 + 2.71
12.88 + 2.31
12.35 + 1.70

TABLE No. 1

375
85
90

stake for any width roadway, slope 1:1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body from side stake to slope stake. If ground is not

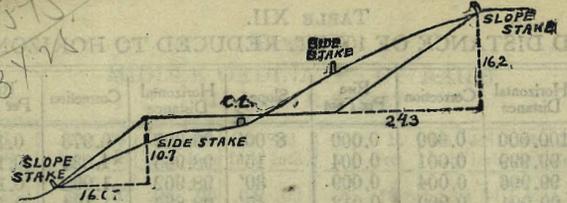
0+23.8
+49.1
35.7
72.8
1.5
88.3

IMPROVED TABLES AND INFORMATION

To find tangent and external for curve of any other degree, divide by degree of curve and add connection found in column of connections. Degree of curve with a given I may be found by dividing tangent (or external) by I. The distance from a point on the tangent to length divided by twice the radius.

Lat # 14
347.00
El. 346.00

285
3426



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

36628 = 8.4010196
 36647 = 5717.8
 36657 = 5731.8
 36639 = 5711.8

36928
 293
 36906628
 293
 366466950
 293
 36637
 36657
 38570
 37170
 17.00

18
 30
 529
 27720807

36591 = 4+678
 36545 = 4+138
 36499 = 3+798
 36453 = 3+358
 36401 = 2+918

36930
 293
 36639
 2.30
 46
 31

13.5
 514

7966
 518
 8780
 197
 7983
 36374 = 2+437
 36731 = 1+945

17896
 116
 1270
 116
 1788
 615.0
 83
 9

36956 = 1+459
 36674 = 0+924

362.00
 293
 359.07

35990 = 0+486
 35907 = 0+100

32660
 293
 32367

