Grade - 133 - Book.

S.E Portion.

SEWERS.

FIELD BOOK

No. 385

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

CHICAGO, ILL.

MICROFILMED

APR 8 1965

W. Line

E. 84th St

E. Line

10'

E.W.

17'-0½" inside

13'-3" Buried Top

19'-0½" outside Top

5.26
3.43
8.69
4.72
3.97
4.38
8.25

-21.25
10.50
4.38
+4.12

8.25
1.38
9.63

-2.75
11.00
4.69
+6.31

+4.00
4.25
4.69
-0.44

Sewer Cons. East of 32nd St

Outlet 16"

BM	3.20	8.46		5.26		
00 = Pump House			12.09	-3.63	+14.30	
+ 25			4.61	3.85	-14.22	
0+50			4.26	4.20	-14.17	
+ 75			4.46	4.00	-14.11	
1+00			4.51	3.95	-14.05	
+ 25			4.46	4.00	-13.98	
1+50			4.43	4.03	-13.92	
			4.35	4.11	-13.86	
2+00			4.17	4.29	-13.80	
			4.21	4.25	-13.73	
+ 50			4.07	4.39	-13.67	
			4.11	4.35	-13.61	
3+00			4.15	4.31	-13.55	
			4.12	4.34	-13.48	
+ 50			4.01	4.45	-13.42	
			3.63	4.83	13.36	
4+00			3.75	4.71	-13.30	
M.H.		7.92				
4+34 ∠ 50°-36' L			2.83	5.09	-13.24	
4+50			2.78	5.14	-13.17	
			3.84	4.08	-13.11	
5+00			4.35	3.57	-13.05	
			4.54	3.38	-12.98	
+ 50			4.74	3.18	-12.92	
			4.80	3.12	-12.86	
6+00			4.79	3.13	-12.80	
M.H.		5.26 = BM				
6+35.5 ∠ 32°-32' L		4.89 RESET				
1931		10.15 = X - Walker	3.26	4.66	-12.71	
6+50			4.23	3.69	-12.64	
			3.00	2.92	-12.62	
7+00			5.28	2.64	-12.56	
			5.55	2.37	-12.50	
+ 50			6.01	1.91	-12.43	
			6.01	1.91	-12.36	
8+00			7.66	+0.26	-12.30	
			8.56	-0.64	-12.23	
+ 50			7.62	+0.30	-12.17	
			6.98	+0.94	-12.11	
9+00			3.95	+3.97	-12.05	
M.H.						
9+19.5 ∠ 54.44'-40'			3.53	+4.39	-12.00	
9+50			5.03	2.89	-11.94	
			5.84	2.08	-11.87	
10+00 T.P.	5.50	5.74	7.68	+0.24	-11.81	
			5.77	-0.03	-11.75	
+ 50			6.39	-0.65	-11.69	
+ 75			6.81	-1.07	-11.63	

1

7.92
2.66
5.26 B.M. B.P. in base of S.D. & A.-A.R. Elev. Xing Signal at 32nd St

+10.67
+18.08 moved 3.79 +14.33 +18.02
+18.37
+18.11
+18.00
+17.98 Moved +17.96
+17.95
+17.97
+18.09
+17.98
+18.06
+17.96
+17.86
+17.82
+17.87
+18.19
+18.01

5.26
2.96
8.22
3.67
4.54
0.85
5.39

+18.33 → New 3.70 4.76 -13.24 +18.00

+18.31	3.08	5.14	-13.17	+18.31
+17.19	4.09	4.12	-13.11	+17.23
+16.62	4.61	3.60	-13.05	+16.25
+16.36	4.84	3.37	-12.99	+16.35
+16.10	5.03	3.18	-12.92	+16.10
+15.98 — OK	5.09	3.12	-12.86	+15.98
+15.93	5.08	3.13	+12.80	+15.93
+17.37	3.53	4.68	-12.71	+17.37
+16.37	4.50	3.71	-12.68	+16.39
+15.54	5.39	2.82	-12.62	+15.44
+15.20	5.53	2.68	-12.56	+15.24
+14.87	5.83	2.34	-12.50	+14.85
+14.34	6.32	1.89	-12.43	+14.32
+14.27	6.40	1.81	-12.36	+14.17
+12.56	7.93	0.28	-12.30	+12.58
+11.59	7.86	0.35	-12.17	+12.52
+13.05	4.51	8.58	-12.11	+12.99
+16.02	1.36	4.03	-12.05	+16.08
+16.39	1.03	4.36	-12.00	+16.36
+14.83	2.46	2.93	-11.94	+14.87
+13.95	3.26	2.13	-11.87	+14.00
+12.05	5.09	0.30	-11.81	+12.31
+11.72	5.37	+0.02	-11.75	+11.77
+11.04	6.01	-0.62	-11.69	+11.01
+10.56	6.41	-1.02	-11.63	+10.61

10.15 = X - Walker
12.71
27.86
5.44
4.79
22.83
5.33
+1.427

2227 2265 783 +14.87 22.51 838 +14.13 2238 1055 +11.53 2226 939 1.293
2258 538 +X.30 2245 998 +12.53 2232 982 +12.50 2220 614 +1.606
5.39

16" Line

		5.74				5.39				
11+00		6.48	-0.74	-11.57	+10.83					
		6.02	-0.28	-11.51	+11.23		6.09	-0.70	-11.57	+10.87
+50		5.95	-0.21	-11.45	+11.24		5.62	-0.28	-11.51	+11.28
		6.50	-0.76	-11.39	+10.63		5.53	-0.14	-11.45	+11.31
12+00		5.73	+0.01	-11.33	+11.34		6.15	-0.76	-11.39	+10.63
		4.61	1.13	-11.27	+12.40		5.35	+0.04	-11.33	+11.38
+50		4.23	1.51	-11.21	+12.72		4.28	1.18	-11.27	+12.40
		4.24	1.50	-11.15	+12.65		3.84	1.55	-11.21	
13+00		3.53	2.21	-11.09	+13.30					
M.H.										
13+40.48 ∠ 11°09' R		2.94	2.80	-11.00	+13.80					
		2.54	3.20	-10.94	+14.14				4.25	
13+90.4		0.24	5.50	-10.84	+14.38	1.42			-0.91	
		2.43	3.31	-10.81	+14.12	2.05				
14+40.4		4.56	1.18	-10.75	+11.93	3.47				
		8.99	-1.25	-10.68	+9.43	3.27				
14+90.4		8.20	-2.46	-10.62	+8.16	-0.80				
		8.10	-2.36	-10.55	+8.19	3.64				
15+40.4		8.24	-2.50	-10.49	+7.99	3.34				
M.H.		8.12	-2.38	-10.42	+8.04				24.2	
15+90.4		7.80	-2.06	-10.36	+8.30					
51.44		6.74	-1.00	-10.31	+9.31					
16+41.8 T.P.		6.88	-1.14	-10.25	+9.11					
		6.64	-0.90	-10.19	+9.29					
16+93.2		5.66	+0.08	-10.13	+10.21					
		2.45	3.29	-10.07	+13.36					
17+44.2		1.28	4.46	-10.01	+14.47					
		5.64	+0.10	-9.95	+10.05					
17+96.2		7.24	-1.50	-9.89	+8.39					
D.M.H.	4.79	7.49	-1.75	-9.83	+8.98	+3.34				
18+47.6		7.17	-2.38	-9.77	+7.39 Main Line		13.17		-9.83	
(48.23)		6.12	-1.47	-9.70	+8.23 ✓		7.38	-4.04	-9.77	+5.73
18+95.82		6.18	-1.39	-9.63	+8.24 ✓		4.79	-1.45	-9.70	+8.25
		6.86	-2.07	-9.56	+7.49 ✓		5.58	-2.24	-9.64	+7.40
19+44.84		6.62	-1.83	-9.50	+7.67 ✓		4.75	-1.41	-9.57	+8.16
		5.84	-1.05	-9.43	+8.38 ✓		4.78	-1.44	-9.50	+8.06
19+92.24		5.62	-0.83	-9.36	+8.53 ✓		4.41	-1.07	-9.44	+8.37
		6.03	-1.24	-9.30	+8.06 ✓		4.87	-1.53	-9.37	+7.84
20+40.48		4.40	+0.39	-9.23	+9.62 ✓		3.74	-0.40	-9.30	+8.90
MH	4.34	5.28	-0.49	-9.17	+8.68 ✓		3.08	+0.26	-9.24	+9.50
N. Line Filbert 20+88.70		5.40	-1.06	-9.10	+8.04 ✓		12.51	-9.17	-9.17	
21+13.7		5.25	-0.91	-9.01	+8.10 ✓					
21+38.7		5.08	-0.74	-8.91	+8.17					
21+63.7		4.57	-0.23	-8.82	+8.59					
21+88.7		5.22	-0.88	-8.73	+7.85					
22+13.7		5.14	-0.80	-8.64	+7.84					
22+38.7 MH E. Alley & Main				-8.55						

16" Line

MH. & Alley 2.92 S.of Main		4.34		1.42	-6.00	+5.34
22+38 (25.4)			5.00	-0.66	-8.55	+7.89
22+64 1			4.97	-0.63	-8.48	+7.85
22+89 5			4.94	-0.60	-8.42	+7.82
23+14 9			4.76	-0.42	-8.35	+7.93
23+40.3			4.76	-0.42	-8.29	+7.87
23+65 7			4.23	0.11	-8.23	+8.34
23+91 1			4.34	0.00	-8.16	+8.16
24+16 5	N Pav BM. 4.00	5.42	2.30	2.04	-8.10	+10.14
24+41 9			193 3.03	2.39	-8.04	+10.43
24+67 3			6.08	-0.66	-7.97	+7.31
24+92 7			5.80	-0.38	-7.91	+7.53
25+18 1			5.59	-0.17	-7.85	+7.68
25+43 5			5.38	+0.04	-7.79	+7.83
25+68 9			5.30	+0.12	-7.72	+7.84
25+94 3			4.92	+0.50	-7.66	+8.16
MH. & Alley 26+19 (25') N.of Main			5.09	+0.33	-7.60	+7.93
26+44 8			4.55	+0.87	-7.53	+8.40
26+69 8			4.61	+0.81	-7.47	+8.29
26+94 5			4.44	+0.98	-7.41	+8.39
27+19 8			4.05	+1.37	-7.34	+8.71
27+44 8			3.43	1.99	-7.28	+9.27
27+69 8			3.59	1.83	-7.22	+9.05
27+94 8			4.14	1.28	-7.16	+8.44
28+19 8			2.32	+3.10	-7.09	+10.19
28+44 5			4.26	-0.84	-7.03	+6.19
28+69 8	T.P. 5.12	8.03	2.51	+2.91	-6.97	+9.88

2.92 500 434 -0.66

17.5

612 2.08 8.20

4.78 / +0.70 = +0.71 P

1.42 2.37 3.79 — 11.99 − 8.20 — 19.20 1.5 11.61 3.41 −8.02

12.72 3.79 8.93 2.81

#2 − 6.12 0.75 −5.37 − 8.08 +2.71

#3 − 6.12 0.68 −5.44 − 8.07 +2.63

− 6.12 1.17 −4.95

X 6.12 1.17 4.95 − 8.12 +3.17

16" Line

		8.03				
28+94 S			5.09	2.94	-6.91	+9.85
29+19 S			4.71	3.32	-6.85	+10.17
29+44 S			4.66	3.37	-6.78	+10.15
29+69 S			4.90	3.13	-6.72	+9.85
29+94 S			5.34	2.69	-6.66	+9.35
N.H. & Alley N.of TP 30+20 Dolberg in 90°00 Δ 5.74 30		8.90	4.87	3.16	-6.60	+9.76
30+50			5.92	2.98	-6.54	+9.52
30+80			5.72	3.18	-6.47	+9.65
31+10			5.53	3.37	-6.40	+9.77
31+40			6.92	1.98	-6.33	+8.31
31+70			5.00	3.90	-6.26	+10.16
32+00			4.84	4.06	-6.20	+10.26
32+30			4.90	4.00	-6.13	+10.13
32+60			4.95	3.95	-6.06	+10.01
32+90			5.10	3.80	-5.99	+9.79
33+20			9.69	-0.79	-5.92	+5.13
33+50 M.H. 30			5.15	3.75	-5.85	+9.60
33+80			5.48	3.42	-5.76	+9.18
34+10			5.48	3.42	-5.68	+9.10
34+40			5.38	3.52	-5.60	+9.12
34+70			5.95	2.95	-5.52	+8.47
35+00			5.85	3.05	-5.44	+8.49
35+30	T.P. 5.15	8.47	5.58	3.32	-5.35	+8.67
35+60			5.13	3.34	-5.29	+8.61
35+90			5.65	2.82	-5.19	+8.01
36+20			5.60	2.87	-5.11	+7.98
36+50			4.53	3.94	-5.03	+8.97
36+80 M.H. & Thor Δ 90°00			4.56	3.91	-4.95	+8.86

16" Line
14" "

		8.47				
	℄Thor+Alley N.of					
36+80 MH 38	Delbert+19		4.17	4.30	-4.95	+9.25
37+18			4.95	3.52	-4.85	+8.37
37+56			5.36	3.11	-4.76	+7.87
37+94			4.93	3.54	-4.66	+8.20
38+32			4.74	3.73	-4.57	+8.30
38+70			4.37	4.10	-4.47	+8.57
39+08			4.45	4.02	-4.38	+8.40
39+46			4.53	3.94	-4.28	+8.22
39+84			4.46	4.01	-4.19	+8.20
40+22			4.25	4.22	-4.09	+8.31
40+60 MH 38	℄Thor+Alley N.of CN+7 Gilman east	12.42 16.70	4.19	4.28	-4.00	+8.28
40+98			12.10	4.60	-3.91	+8.51
41+36			11.98	4.72	-3.81	+8.53
41+74			12.00	4.70	-3.72	+8.42
42+12			11.70	5.00	-3.62	+8.62
42+50 MH 32.9	℄Thor+ Birch	4.60 9.75	11.55	5.15	-3.53	+8.68 End 16" Line Start 14" Line
42+82.9 MH 30.66	Δ=0+32.9		4.44	5.31	-3.44	+8.75
0+63.56			4.54	5.21	-3.37	+8.58
0+94.22			4.35	5.40	-3.29	+8.69
1+24 88			4.32	5.43	-3.21	+8.64
1+55 54			4.46	5.29	-3.14	+8.43
1+86 20			4.52	5.23	-3.06	+8.29
2+16 86			4.53	5.22	-2.99	+8.21
2+47 52			4.31	5.44	-2.91	+8.35
2+78 2 MH	℄Alley Blk C.		4.33	5.42	-2.83	+8.25

			9.75	14" Lime		
2+78.2 MH ℄ Alley Blk C.			4.33	5.42	-2.83	+8.25
3+11 95			4.55	5.20	-2.75	+7.95
3+45 20			4.49	5.26	-2.67	+7.93
3+79 45			4.90	4.85	-2.58	+7.43
4+13 20			4.78	4.97	-2.50	+7.47
4+46 95			4.64	5.11	-2.41	+7.52
4+80 70			4.64	5.11	-2.33	+7.44
5+14 45			4.75	5.00	-2.24	+7.24
5+48 MH ℄ 37"St			4.40	5.35	-2.16	+7.51
T.P. 6.97		N 11° 37" 54" E 11.84	4.88	4.87		
5+82 26			5.94	5.86	-2.08	+7.94
6+16 32			5.88	5.96	-1.99	+7.95
6+50 75			5.93	5.91	-1.90	+7.81
6+84 44			5.62	6.22	-1.82	+8.04
					-1.25	+7.48
7+18 MH ℄ Beta			5.61	6.23	-1.74	+7.97
7+56 5			5.37	6.47	-1.60	+8.07
7+94 5			4.96	6.88	-1.45	+8.33
8+32 5			4.57	7.27	-1.30	+8.57
8+70 5			4.23	7.61	-1.15	+8.76
9+08 MH ℄ Alley N ℄ Beta		Δ 90°-0'-14" E. in Alley Blk H12-H19.	4.29	7.55	-1.00	+8.55
9+41 5			3.64	8.16	-0.92	+9.08
9+74 5			3.72	8.12	-0.83	+8.95
10+07 5			3.88	7.96	-0.75	+8.71
10+40 5			3.71	8.13	-0.67	+8.80
10+73 5			3.64	8.20	-0.58	+8.78
11+06 5			3.44	8.40	-0.50	+8.90
11+39 5			3.13	8.71	-0.41	+9.12

14" Line
E to Alleys Blks 412-419
11.84

11+72 S			3.02	8.82	-0.33	+9.15	
12+05 S			3.07	8.77	-0.25	+9.02	
12+38 S MH.			2.56	9.28	-0.17	+9.45	
12+71 S			3.03	8.81	-0.09	+8.90	
13+04 S	T.P. 3.93	13.17	2.60	9.24	0.00	+9.24	
13+37 S			3.90	9.27	+0.08	+9.19	
13+70 S			3.38	9.79	+0.16	+9.63	
14+03 S			3.57	9.60	+0.24	+9.36	
14+36 S			3.64	9.53	+0.32	+9.21	
14+69 S			3.54	9.63	+0.40	+9.23	
15+02 S			3.09	10.08	+0.48	+9.60	
15+35 S			3.02	10.15	+0.56	+9.59	
15+68 S MH @ 38th St	7.78	17.77	3.18	9.99	+0.65	+9.34	
16+01			7.47	10.30	0.73	0.87	+9.43
16+34			6.87	10.90	0.81	1.09	+9.81
16+67			6.47	11.30	0.89	1.31	+9.99
17+00			6.50	11.27	0.98	1.53	+9.74
17+33			6.87	11.40	1.06	1.75	+9.65
17+66			5.98	11.79	1.14	1.97	+9.82
17+99			5.65	12.12	1.22	2.19	+9.93
18+32			5.26	12.57	1.30	2.41	+10.16
18+65			5.15	12.62	1.38	2.63	+9.99
18+98 M.H.			4.90	12.87	1.47	2.85	+10.02
19+31			4.52	13.25	1.55	3.07	+10.18
19+64			4.35	13.42	1.63	3.29	+10.13
19+97			4.20	13.57	1.72	3.51	+10.06

Adopted channel

Original

+ 9.57	✓
+ 10.09	✓
+ 10.41	✓
+ 10.29	✓
+ 10.34	✓
+ 10.65	✓
+ 10.90	✓
+ 11.27	✓
+ 11.24	✓
+ 11.40	✓
+ 11.70	✓
+ 11.79	✓
+ 11.85	✓

13.17
2.11
11.06

13 P 11.06 SE Alpha + 34"

14" Line

17.77

11+7	20+30			3.53	14.24	1.80	3.13	+10.51		+ 12.44 ✓
12+0	20+63			3.27	14.50	1.88	3.95	+10.55		+ 12.62 ✓
12+4	20+94			3.12	14.65	1.97	4.17	+10.48		+ 12.68 ✓
12+7	21+29			2.90	14.87	2.05	4.39	+10.48		+ 12.82 ✓
13+1	21+62			2.77	15.00	2.13	4.61	+10.39		+ 12.87 ✓
13+	21+95			2.47	15.30	2.21	4.83	+10.47		+ 13.09 ✓
	90°Δ on 14" Line	T.P. 3.85	19.43	2.19	15.58	7.00	7.00	+ 8.68	SPUR	+ 8.68
13+	22+28 MH ℄ 39th 31.67			3.75	15.68	2.30	5.05	+10.63	14" Line	+ 13.39 ✓
14+	22+59 67			4.40	15.03	2.38	5.13	+ 9.90		+ 12.65 ✓
14+	22+91 33			4.31	15.12	2.46	5.21	+ 9.91		+ 12.66 ✓
14+	23+23			4.21	15.22	2.54	5.29	+ 9.93		+ 12.68 ✓
15+	23+54 67			3.61	15.82	2.62	5.37	+10.45		+ 13.20 ✓
15+	23+86 33			4.40	15.03	2.70	5.45	+ 9.58		+12.33 ✓
						8.00	8.00	+ 6.89	SPUR	+ 6.49
15+	24+18 ΔMH ℄ Alpha 31.67			4.54	14.89	2.77	5.52	+ 9.37	14" Line	+ 12.12 ✓
16+	24+49 67			4.02	15.41	2.85	5.60	+ 9.81		+ 12.56 ✓
16+	24+81 33			3.69	15.74	2.93	5.68	+10.06		+ 12.81 ✓
16+	25+13 00			3.81	15.62	3.01	5.76	9.86		+ 12.61 ✓
17+	25+44 67			3.67	15.76	3.09	5.84	+ 9.92		+ 12.67 ✓
17+	25+76 33 ℄ 39th & Alley W. of Alpha	T.P. 5.55	20.54	4.44	14.99	3.17	5.92	+ 9.07		+ 11.82
						3.25	6.00	+ 8.25	14" Line	+ 11.00
17+	26+08 00 33 DMH Δ 90° on 14" Line			6.29	14.25	7.00		+ 7.25	14" "	+ 7.25
17+	26+41			5.75	14.79	7.20		+ 7.59		
18+	26+74			6.50	14.04	7.40		+ 6.64		
18+	27+07			7.34	13.20	7.60		+ 5.60		
18+	27+40			7.60	12.94	7.80		+ 5.14		
19+	27+73			6.70	13.84	8.00		+ 5.84		
19+	28+06			5.61	14.93	8.20		+ 6.73		
19+	28+39			5.17	15.37	8.40		+ 6.97		

Not changed

Original

14.24
1.67
15.91
9.7
6.2

			14" Line			
		20.54				
28+72			4.90	15.64	8.60	+7.04
29+05			4.73	15.81	8.80	+7.01
29+38 MH			4.43	16.11	9.00	+7.11
29+71			4.80	15.74	9.10	+6.64
30+04			4.48	16.06	9.20	+6.86
30+37			4.45	16.09	9.30	+6.79
30+70			4.28	16.26	9.40	+6.86
31+03			4.16	16.38	9.50	+6.88
31+36			4.24	16.30	9.60	+6.70
31+69			3.54	17.00	9.70	+7.30
32+02			3.39	17.15	9.80	+7.35
32+35			2.83	17.71	9.90	+7.81
90° Δ in 14" Line						
32+18 MH. ℄ 40 T.P. 6.71		25.64	1.61	18.93	10.00	+8.93
31.67						
32+99 47			5.68	19.96	10.14	+9.82
33+31 38			5.60	20.04	10.78	+9.76
33+63			7.50	18.14	10.42	+7.72
33+94 47			7.76	17.88	10.56	+7.32
34+26 33			7.47	18.17	10.70	+7.47
90° Δ in 14" Line						
34+58 MH. ℄ 40 Z			6.95	18.69	10.84	+7.85
33						
34+91			6.83	18.81	10.98	+7.83
35+24			6.71	18.93	11.13	+7.80
35+57			5.80	19.84	11.27	+8.57
35+90			4.64	21.00	11.42	+9.58
36+23			4.17	21.47	11.56	+9.91
36+56			4.06	21.58	11.71	+9.87
36+89			4.13	21.51	11.85	+9.66

		25.64				
37+22			3.73	21.91	12.00	+9.91
37+55			3.44	22.00	12.15	+9.85
37+88 33	M.H. T.P. 5.02	27.15	3.51	22.13	12.30	+9.83
38+21			5.38	21.77	12.44	+9.33
38+54			4.48	22.67	12.59	+10.08
38+87			4.50	22.65	12.73	+9.92
39+20			4.41	22.74	12.88	+9.86
39+53			4.22	22.93	13.02	+9.91
39+86			4.47	22.68	13.17	+9.51
40+19			4.10	23.05	13.31	+9.74
40+52			4.01	23.14	13.46	+9.68
40+85			3.81	23.34	13.60	+9.74
	90° Δ 14" Line					
41+18 31.67	MH ℄ 41st & Z T.P. 3.58	28.25	2.48	24.67	13.74	+10.93
41+49 67			5.06	23.19	13.88	+9.31
41+81 33			4.90	23.35	14.02	+9.33
42+13			4.42	23.83	14.16	+9.67
42+44 67			4.43	23.82	14.30	+9.52
42+76 33			4.52	23.73	14.44	+9.29
43+08 46.9	MH ℄ 41st Alley		4.60	23.65	14.57	+9.08
43+54 9			4.78	23.46	14.78	+8.68
44+01 8			5.55	22.70	15.00	+7.70
44+48 7			14.55	13.70	15.20	−1.50
MH ℄ Boston						
44+95 38			4.79	23.46	15.40	+8.06
45+33			5.25	23.00	15.60	+7.40
45+71			5.15	23.10	15.80	+7.30
46+09			4.98	23.27	16.00	+7.27

187.6 + 19.4 = 207.0

12.72
1.83
14.55

← Change in Line

6.22	29.68	23.46	15.40	+8.06
6.80	22.88		15.60	+7.28
6.85	22.83		15.80	+7.03
6.47	23.21		16.00	+7.21

		28.25				29.68		4.97 / 24.79	3.63 / 20.04	1
46+47 ℄ M.H. ℄ Alley			3.95	24.90	12.20	+8.10		5.64	24.04	16.20 +7.84
46+85 T.P. 5.96		30.67	3.54	24.71	16.40	+8.31		5.36	24.32	16.40 +7.92
47+23			5.92	24.75	16.60	+8.15		5.22	24.46	16.60 +7.86
47+61			5.88	24.79	16.80	+8.00		5.08	24.60	16.80 +7.80
47+79			5.76	24.91	17.00	+7.91		5.02	24.66	17.00 +7.66
48+37			5.55	25.12	17.20	+7.92		4.90	24.78	17.20 +7.58
48+75			5.84	24.83	17.40	+7.43	change in HI	5.01	24.67	17.40 +7.27
49+13			5.56	25.11	17.60	+7.51		4.58	25.10	17.60 +7.50
49+51			4.77	25.90	17.80	+8.10		3.85	25.83	17.80 +8.03
49+89			4.82	25.85	18.00	+7.85		3.87	25.81	18.60 +7.81
50+27 150'S. of ℄ Lin-National			4.61	26.06	18.20	+7.86		3.76	25.92	18.20 +7.72
50+65 MH ℄ Alley 41.7			4.81	25.86	18.40	+7.46 OK		21.00 + 4.86		14.40
			4.46	26.21	18.59	+7.62 OK				
			4.31	26.36	18.78	+7.58 O.K.				
			3.44	27.23	18.97	+8.26 O.K				
T.P. 9.86		37.83	2.70	27.97		gone				
		gone	5.30	32.43 ~~32.53~~	19.16	+13.37 +13.27				
		gone	~~4.81~~	32.41 ~~33.02~~	19.35	gone +13.67 +13.06				
			3.28	34.55	19.54	+15.01 OK				
			7.93	29.90	19.72	+10.22 OK				
T.P. 0° 0' =DM.H @ 39-10' L 12.72		41.25	9.40	28.43	23.50 18.90	+8.53	8 333.8 / 41.7	23.50	+4.93	
					26.00	+4.01				
00.= DM.H ℄ Alley 5-49.18			11.24	30.01	24.00	+6.01				
+49 14			12.18	29.07	24.40	+4.67				
+98 36			11.92	29.33	24.80	+4.53				
1+47 54	T.P. 10.63	40.47	11.46	29.79	25.20	+4.59				
1+96 22			8.96	31.46	25.60	+5.86				
2+45 90 MH ℄ Logan			7.91	32.51	26.00	+6.51				

		40.42				
2+45 99 M. H. Logan 5-46.6 5-47.00			7.91	32.51	26.00	6.51
2+94 7			6.68	33.74	26.90	+6.84
3+43 5			6.97	33.45	27.80	+5.65
3+92 3			3.85	36.57	28.70	+7.87
4+41 1			2.19	38.23	29.60	+8.63
4+89 9 MH Δ 30°-37' R 6-46.07		46.68	4.40 10.67	chk (36.02 36.01	30.5	+5.51
5+35.92			7.93	38.75	31.42	+7.33
5+82 04			8.62	38.06	32.34	+5.72
6+28 10			7.20	39.48	33.25	+6.23
6+74 17			8.11	38.57	34.16	+4.41
7+20 24			6.17	40.51	35.08	+5.43
7+66 3 D.M.H.			5.64	41.04	36.00 38.00	+.5.04 +3.04
+50			2.02 1.28	44.66 45.40	39.24	+5.42
1+00	T.P. 11.96	57.36	11.33	46.03	40.48	+5.55
+50			12.12	45.24	41.72	+3.52
2+00			9.65	47.71	42.96	+4.75
+50			8.70	48.66	44.20	+4.46
3+00 MH			7.14	50.22	45.44	+4.78
+50			4.96	52.40	46.68	+5.72
4+00			4.12	53.24	47.92	+5.32
+50			1.45	55.91	49.16	+6.75
5+00	T.P. 12.45	68.56	1.25	56.11	50.40	+5.71
+50			11.62	56.94	51.64	+5.30
6+00 M.H.			10.78	57.78	52.88	+4.90

Continued in Book 1186 Page 27

Sewer Cons. from ℄ Una
℄ Thru Blks 162 + 161

				Page 14		
00 = MH. 3+80 Page 14	6.08	12.25	6.17	6.17	-0.50	+6.67
+55			5.30	6.95	-0.24	+7.21
1+10			4.97	7.28	-0.02	+7.30
1+65			4.44	7.81	+0.22	+7.59
2+20			4.21	8.04	+0.46	+7.58
2+75			4.68	7.57	+0.70	+6.87
3+30 MH			4.56	7.69	+0.95	+6.74
3+85			4.79	7.46	+1.19	+6.27
4+40			5.28	6.97	+1.43	+5.54
4+95			3.91	8.34	+1.67	+6.67
5+50			4.66	7.59	+1.91	+5.68
6+05	T.P. 485	12.72	4.38	7.87	+2.15	+5.72
M.H. ℄ Vista 6+60 46.5 PVI			5.55	7.17	+2.40	+4.77
7+06			6.54	6.18	+2.62	+3.56
7+52			6.81	5.91	+2.84	+3.07
7+98			5.56	7.16	+3.06	+4.10
8+44			4.49	8.23	+3.28	+4.95
~~9+90~~ DE			3.13	9.59	+3.50	6.09
8+90						

5 | 2 39 / 4 2

Sewer Cons. ℄ Una from ℄ Blks 202-203 to ℄ Blks 162 & 163

12,34

00=MH 13+87.1 Page 15		2.73	9.61	-3.85	+ 13.46
0+47.5		3.43	8.91	-3.44	+ 12.35
0+95		3.83	8.51	-3.02	+ 11.53
1+42.5		4.48	7.86	-2.60	+ 10.46
1+90		5.05	7.29	-2.18	+ 9.47
2+37		5.44	6.90	-1.76	+ 8.66
2+85		5.65	6.69	-1.34	+ 8.03
3+32		5.96	6.38	-0.92	+ 7.30
℄ Una 3+80 MH		6.17	6.17	-0.50	+ 6.67
Sewer Cons W. from ℄ Una Thru Blks 163+164					
00=MH 3+80 above		6.17	6.17	-0.50	+ 6.67
+48.5		7.26	5.08	-0.29	+ 5.37
+97		7.60	4.74	-0.08	+ 4.82
1+45		7.50	4.84	+0.13	+ 4.71
1+94		7.58	4.76	+0.34	+ 4.42
2+42.5	T.P 12.4 17.03	7.52	4.82	+0.55	+ 4.27
2+91		11.69	5.34	+0.77	+ 4.57
3+40 MH 53,33 7 Pts		10.88	6.15	+1.0	+ 5.15
3+93		8.30	8.73	+2.25	+ 6.48
4+46		8.06	8.97	+3.50	+ 5.47
5+00		5.49	11.54	+4.75	+ 6.79
5+53		4.57	12.46	+6.00	+ 6.46
6+06		3.97	13.06	+7.25	+ 5.81
M.H. ℄ Thor 6+60 47.5 4 Pts		2.12	14.91	8.50	+ 6.41
7+07		2.06	14.97	+8.87	+ 6.10
7+55		1.47	15.56	+9.25	+ 6.31
8+02		0.89	16.14	+9.62	+ 6.52
8+50 DE		1.60	16.07	10.0	+ 6.03

Sewer Cons. 8" Sheet #7

Allens 201-202 Silver Gate Park 8"

10.53

18+47.50 DM. H16" Lin. 00' Page 2 8 PTS			12.96	-2.43	-7.30	+4.87				
0+47.5			8.60	+1.93	-7.18	+9.11				
0+95.00			1.96	+8.57 ✓	-7.06	+15.63				
1+42.50			1.79	8.74	-6.94	+15.68				
1+90.0			1.57	8.96 ✓	-6.82	+15.78				
2+37.5			2.24	8.29 ✓	-6.70	+14.99				
2+85			1.88	8.65 ✓	-6.58	+15.23 ✓				
3+32.5			1.93	8.60 ✓	-6.46	+15.06				
3+80.0 M.H 48.3 7 PTS			2.60	7.93 ✓	-6.34	+14.27				
4+28.3			3.74	6.79 ✓	-6.22	+13.01				
4+76.2			3.09	7.44 ✓	-6.10	+13.54 ✓				
5+24.9			2.66	7.87 ✓	-5.98	+13.85 ✓				
5+73			2.71	8.32 ✓	-5.86	+14.18				
6+21.5			2.08	8.43 ✓	-5.74	+14.19 ✓				
6+69.8 MH & THOR			1.67	8.86	-5.62	+14.48 ✓				
7+18.1 .5 5.6 PTS			1.48	9.05	-5.50	+14.55				
7+73.1			1.21	9.32	-5.36	+14.68				
8+28.1 T.P	H.I.2	13.58	1.07	9.46	-5.22	+14.68				
8+83.1			3.95	9.63	-5.09	+14.72				
9+38 ⊥			4.48	9.10	-4.95	+14.05				
9+93 ⊥ M.H			4.47	9.11	-4.81	+13.92				
10+48.1 55.1 6 PTS			4.22	9.36	-4.67	+14.03				

17.03 Page 14

8.71
8.32
2.13
10.53

11.3
2.7
13.5
10.85
-3.0

10.81
21

3.34 10.75 -7.41

0.12 Diff. (13.48) between B.M.5 old B.M.12 Low Level N.G.

4.30	9.18	-5.37	+14.55	
4.01	9.47	-5.25	+14.72	
3.87	9.61	-5.12	+14.73	
3.70	9.78	-4.99	+14.77	
4.22	9.26	-4.87	+14.13	
4.21	9.27	-4.74	+14.01	
3.96	9.52	-4.61	+14.13	

MH Page 15		13.58					13.48			
10+48 ⊥ 55' 6 PTS			4.22	9.36	−4.67	+14.03	3.96	9.52	−4.61	+14.13
11+03 ⊥			4.44	9.14	−4.54	+13.68	4.18	9.30	−4.49	+13.79
11+58 ⊥			3.95	9.63	−4.40	+14.03	3.69	9.79	−4.36	+14.15
12+13 ⊥			3.84	9.74	−4.27	+14.01	3.57	9.91	−4.23	+14.14
12+68 ⊥			3.37	10.21	−4.13	+14.34	3.11	10.37	−4.11	+14.48
13+23 ⊥			2.95	10.63	−3.99	+14.62	2.69	10.79	−3.98	+14.77
M.H. & Una, 13+78 ⊥ 55' 6 PTS	7.17	16.87	4.00	9.70 Page 14 9.58	−3.85	+13.555	3.78	9.70	−3.86	+13.55
14+33 ⊥			6.19	10.68	−3.71	+14.39				
14+88 ⊥			5.75	11.12	−3.57	+14.69				
15+43 ⊥			4.93	11.94	−3.44	+15.38				
15+98 ⊥			4.38	12.49	−3.30	+15.79				
16+53 ⊥			4.27	12.60	−3.16	+15.76				
M.H. 17+08 ⊥ 55' 6 PTS			5.20	11.67	−3.02	+14.69				
17+63 ⊥			5.16	11.71	−2.89	+14.60				
18+18 ⊥			4.14	12.73	−2.75	+15.48				
18+73 ⊥			5.75	11.12	−2.61	+13.73				
19+28 ⊥			7.61	9.26	−2.48	+11.74				
19+83 ⊥	4.53 / 4.76 / 4.27		8.60	8.27	−2.34	+10.61				
M.H. & Vesta 20+38 ⊥ 55' 6 PTS	T.P. 6.19	14.79	8.27	8.10	−2.20	+10.80				
20+93 ⊥			6.05	8.74	−2.06	+10.80				
21+48 ⊥			5.91	8.88	−1.92	+10.80				
22+03 ⊥			5.59	9.20	−1.78	+10.98				
22+58 ⊥			5.33	9.46	−1.65	+11.11				
23+13 ⊥			5.11	9.68	−1.51	+11.19				
M.H. 23+68 ⊥			4.77	10.02	−1.375	+11.39				

8.60
9.33
17.93
1.91
16.02
4.27
20.29
3.46
16.83
20.29
3.62
16.67

New spk S.W. Vesta & Main
old spk S.W. Vesta & Main
This spk flush with Pole

M.H. Page 16		14.79				
23+68 ⊥ 55' 6 pls			4.77	10.02	-1.37	+11.39
24+23 ⊥			3.62	11.17	-1.23	+12.40
24+78 ⊥			3.54	11.25	-1.10	+12.35
25+33 ⊥			3.13	11.66	-0.96	+12.62
25+88 ⊥	T.P 4.66	17.13	2.32	12.47	-0.83	+13.30
26+43 ⊥			4.27	12.86	-0.69	+13.55
M.H. & Woden 24+98 ⊥	M.H.		3.81	13.32	-0.55	+13.87

8" Sewer & Woden from M.H above To & Alleys Blks 255-256

17.13

0.0 = M.H 26+98 above			3.81	13.32	-0.55	+13.87
0+47.6			2.82	14.31	-0.44	+14.75
95.2			3.42	13.71	-0.32	+14.03
1+42.8			4.10	13.03	-0.20	+13.23
1+90.4			8.42	8.71	-0.08	+8.78
2+38.0			4.37	12.76	+0.04	+12.72
2+85.6			6.20	10.93	+0.16	+10.77
3+33.3 & Alley Bet Main & Filbert			8.31	8.82	+0.28	+8.54
3+81.0 47.4	M.H. T.P. 7.04	14.76	9.41	7.72	+0.40	+7.32
4+28.4			6.68	8.08	+0.52	+7.56
4+76.2			5.83	8.93	+0.64	+8.29
5+23.8			4.74	10.02	+0.76	+9.26
5+71.4 & Main			4.60	10.16	+0.88	+9.28
6+19.0			4.40	10.36	+1.00	+9.36
6+64.6			4.05	10.71	+1.12	+9.59
7+14.2 & Alley Bet. Main + Dalbergia			3.67	11.09	+1.24	+9.85
7+62.0 MH			3.33	11.43	+1.35	+10.08

12.72
1.20
11.52

8 (38 ⊥) 47.6 .75 895/12

17.13
4.14
12.99 B.P.N.W. Woden + Main

17.13
2.58
14.55 3 P.K.N.W. Woden + Main

Sewer Construction & Alley Blk 210.

from W. Woden W. to D.E.

& Alley Bet Filbert & Main					
00=M.H.	T.P. Page 17 9.84	17.56		7.72	+0.40
+50			7.10	10.46	+4.70
1+00 Blk			3.41	14.15	+9.00
+50			0.37	17.19	+9.25
2+00			1.17	16.39	9.50
+50			3.87	13.69	9.75
3+00 MH			3.67	13.89	10.00
+50	T.P. 6.89	20.59	3.84	13.70	10.25
4+00			6.59	14.00	10.50
+50			5.19	15.40	10.75
5+00			4.86	15.73	11.00
+50			4.71	15.88	11.25
6+00 D.E. E. of Vesta			5.30	15.29	11.50

+7.32
+5.76
+5.15
+7.94
+6.89
+3.94
+3.89
+3.45
+3.50
+4.65
+4.73
+4.63
+3.79

18.6
4.3

20.59
14.63
3.96

14.63
5.325
21.955
6.265
15.690 B.P.N.W. Main & Vesta.

Sewer Construction

Thru Blks 214-213-212-211

BM	3.45	4.87		1.42	SW Main & Spk Sieva.		
O.E. 14" N of Siva = 1+40			6.53	−1.66	−5.00	+3.34	
1+05			6.04	−1.17	−5.25	+4.08	
0+70			5.72	−0.85	−5.50	+4.65	
0+35			5.54	−0.67	−5.75	+5.08	
0+00 D M.H. & Siva			5.53	−0.66	−8.55 / −6.0	+5.34	
+28.33			5.19	−0.32	−5.84	+5.52	
+56.67 T.P.	5.14	4.82	5.19	−0.32	−5.67	+5.35	
+85.00			5.22	−0.40	−5.50	+5.10	
1+13 33			5.47	−0.65	−5.34	+4.69	
1+41 67			5.26	−0.44	−5.17	+4.73	
1+70 00			4.97	−0.15	−5.00	+4.85	
1+98 33			5.04	−0.22	−4.84	+4.62	
2+26 67			4.87	−0.05	−4.67	+4.62	
2+55 00			5.12	−0.30	−4.50	+4.20	
2+83 33			5.03	−0.21	−4.34	+4.13	
3+11 67			4.73	+0.09	−4.17	+4.26	
3+40 MH (26.66)			5.14	−0.32	−4.0	+3.68	
3+66 67			4.62	+0.20	−3.50	+3.70	
3+93 33			3.89	+0.93	−3.00	+3.93	
4+20			2.49	2.33	−2.50	+4.83	
4+46 67	TP — 12.62	16.14	1.30 / 12.51	3.52 / 3.63	−2.00	+5.63	
4+73 33			11.22	4.92	−1.50	+6.42	
5+00			10.44	5.70	−1.00	+6.70	
5+26 66			10.56	5.58	−0.50	+6.08	
5+53 33			10.51	5.63	0.00	+5.63	
5+80			10.41	5.73	+0.50	+5.23	

5.99 − 0.77 = 5.22 → 5.67 − 0.45 = 5.22; 5.22 − 0.45 = 4.77

5.87 − 1.00 = 4.87

5.66 − 4.66 = 1.00 → 6.00 − 1.00 = 5.00

BMs 114113-112 — 111

16.14

6+06 (6)		8.71	7.43	+1.00
6+33 (33)		8.20	7.94	+1.50
6+60 MH & Thor (30)		7.76	8.38	+2.0
6+90		6.80	9.34	2.15
7+20		5.15	10.99	2.30
7+50		4.50	11.64	2.46
7+80		4.24	11.90	2.61
8+10		4.27	11.87	2.76
8+40		3.58	12.56	2.92
8+70		3.18	12.96	3.07
9+00		3.51	12.63	3.22
9+30		2.90	13.24	3.38
9+60		2.00	14.14	3.55
9+90 M.H. T.P. 3.64 (58)	18.23	1.55	14.59	3.57
10+45		2.35	15.88	4.90
11+00		2.11	16.12	4.29
11+55		3.15	15.08	4.57
12+10		3.75	14.48	4.81
12+65		4.20	14.03	5.17
13+20 MH & 4na (50)		5.76	12.47	5.43
13+70		5.76	12.47	5.70
14+20		7.16	11.07	5.96
14+70		7.05	11.18	6.22
15+20		6.74	11.49	6.50
15+70		6.97	11.26	6.75
16+20 M.H		7.32	10.91	7.00

+6.73
+6.74 Marked Road 6.74
+6.38
+7.19
+8.69
+9.18
+9.29
+9.11
+9.64
+9.89
+9.41
+9.86
+10.59
+10.87
+11.88
+11.85
+10.51
+9.62
+8.89
+7.04
+6.77
+5.11
+4.96
+4.99
+4.51
+3.91

Blks 114-113-112-111

18.23

16+20 MH T.P.	6.14	17.05	7.32	10.91	7.00
16+68			5.70	11.35	7.25
17+16			4.04	11.01	7.50
17+65			5.33	11.72	7.75
18+13			4.65	12.40	8.00
18+61			4.71	12.34	8.25
19+10 P.E.			3.98	13.07	8.50

+3.91
+4.10
+3.51
+3.97
+4.40
+4.09
+4.57

17.05
1.40
15.65

Grd. Book 197-17
Spike in S.E. Pole 39th & Gamma. = 51.76
3.70+
61.46=x

Walker
Osborne
5-19-43

Extension of Sewer Block 418

Arlington Subdivision.

61.46

Station		Elev. Stakes Flow	Elev. Flow line 50.00 P. 55
5+90 Page 55 = 0+00	Chk. Flow	11.45	50.01
+25		5.34	56.12	50.38
+50		5.08	56.38	50.76
+75		4.65	56.81	51.14
1+05=DE 5'E EL. 39th St.		4.21	57.25	51.58
2+05 Profile Elev.		3.8	57.7	

1.50%

Cuts. offsets.

+5.74
+5.62
+5.67
+5.67

38½ St.

4' Lt.

4' Rt.

End of Existing Sewer

For Construction Notes. This line Page 55

Constructed by City Sewer Dept May 1, 1943 GR.H.

M.H. 370' M.H. 220' Extension 57' 48'

180°00

30°36'

Block 418

198.52'

39th St.

17' 43'

53'

Gamma

27'

Fd Nail

17' 43'

BM Mon 22.59 / 13.07 / 7.52 Main + Division

Sewer Construction

Alley Blk 257.

10.34 Page 27

2.3 / 26.5

00 MH. & Yama			4.14	6.20	3.00	+3.20
+42.5			4.51	5.83	3.10	+2.73
+95			5.00	5.34	3.20	+2.14
1+42.5			5.04	5.30	3.30	+2.00
1+90			5.14	5.20	3.40	+1.80
2+37.5			5.94	4.40	3.50	+0.90
2+85			6.04	4.26	3.60	+0.66
3+32.5			4.38	5.96	3.70	+2.26
	T.P.	12.36	22.63	0.07	10.27	
3+80 M.H. 52.5				12.09	10.54	3.80 +6.74
4+32.5				6.88	15.75	8.35 +7.40
4+85	T.P.	9.93	28.78	3.78	18.85	12.90 +5.95
5+37.5				5.43	23.35	17.45 +5.90
5+90 P.E.				1.90	26.88	22.00 +4.88

Sewer Construction Thru

Alleys Blks 251-252-253-254

BM.	4.15	5.57		1.42	Spk. S.W. Main & Siva	
H10W of ℄ Siva = DE			4.47	1.10	-5.00	+6.10
B+69			4.14	1.43	-5.26	+6.69
3+28			4.14	1.43	-5.52	+6.95
2+87			4.24	1.33	-5.78	+7.11
2+46			4.22	1.35	-6.04	+7.39
2+05			4.41	0.96	-6.30	+7.26
1+64			4.77	0.80	-6.56	+7.36
1+23			5.07	0.50	-6.82	+7.32
0+82			4.77	0.80	-7.08	+7.88
0+41 N			4.61	0.96	-7.34 ↑	+8.30
00 = D.M.H. ℄ Siva			4.86	0.71	-7.6 -6.0 ↓	+8.31 +6.71
+38			4.83	0.74	-5.80	+6.54
+76			4.57	1.00	-5.60	+6.60
1+14			4.87	0.70	-5.40	+6.10
1+52			4.13	1.44	-5.20	+6.64
1+90			3.69	1.88	-5.00	+6.88
2+28 T.P.	8.52	10.25	3.84	1.73	-4.80	+6.53
2+66			8.52	1.73	-4.60	+6.33
3+04			8.71	1.54	-4.40	+5.94
3+42			8.77	1.48	-4.20	+5.68
3+80 MH.			8.71	1.54	-4.00	+5.54

B.M.'s 251 - 252 - 253 - 254

		10.25				
3+50 M.H. 89			8.71	1.54	-4.00	+5.54
4+15			8.88	1.37	-2.94	+4.31
4+50			7.42	2.83	-1.88	+4.71
4+85			5.25	5.00	-0.82	+5.82
5+20			4.25	6.00	+0.25	+5.75
5+55			3.02	7.23	+1.31	+5.92
5+90			0.80	9.45	+2.37	+7.08
6+25			0.67	9.58	+3.43	+6.15
6+60 M.H. ℄ T hor T.P. 10.17 41.25		19.10	1.32	8.93	+4.50	+4.43
7+01 25			9.18	9.92	5.00	+4.92
7+42 50			7.98	11.12	5.50	+5.62
+83 75			7.98	11.12	6.00	+5.12
8+25			7.38	11.72	6.50	+5.22
+66 25			6.83	12.27	7.00	+5.27
9+07 50			5.57	13.53	7.50	+6.03
+48 75			4.01	15.09	8.00	+7.09
9+90 M.H. 41.25			3.48	15.62	8.50	+7.12
10+31 25			2.59	16.51	8.70	+7.81
10+72 50			1.93	17.17	8.90	+8.27
11+13 75			1.19	17.91	9.10	+8.81
11+55			1.52	17.58	9.30	+8.28
11+96 25			1.73	17.37	9.50	+7.87
12+37 50 T.P. 3.11		20.19	2.02	17.08	9.70	+7.38
12+78 75			3.85	16.34	9.90	+6.44
13+20 M.H. ℄ Una			4.09	16.10	10.11	+5.99
		M.I.	gr Rear	gr Ct	F.L.	

		20,19				
13+20 M.H. ℄ Una			4.09	16.10	10.11	+5.99
13+70			3.49	16.70	10.35	+6.35
14+20			4.84	15.35	10.59	+4.76
14+70			4.17	16.02	10.84	+5.18
15+20			4.47	15.72	11.08	+4.64
15+70			4.10	16.09	11.32	+4.77
16+20 M.H. 48.33			4.44	15.75	11.57	+4.18
+68 33			4.62	15.57	11.81	+3.76
17+16 67			4.64	15,55	12.05	+3.50
17+65			3.41	16.78	12.29	+4.49
18+13 33	TP 4.51	21,85	2.85	17.34	12.53	+4.81
+61 67			4.77	17.08	12.77	+4.31
19+10 DE Wolfvista			3.30	18.55	13.00	+5.55

21.85 − 6.20 = 15.65 // 15.69

BIK 255

Bet Maine Dalbergia Woodruff West

BM.	5.01	20.70		15.69	N.W. Vee To a Main		
5+90 W. & Woodruff: DE			2.63	18.07	13.00		+5.07
5+46 67 W			4.35	16.35	12.00		+4.35
5+03 33 W			6.67	14.03	11.00		+3.03
4+60 - B+K			7.31	13.39	10.00		+3.39
4+13 33			7.01	13.69	9.67		+4.02
3+66 47			6.91	13.79	9.33		+4.46
3+20 M.H.			6.32	14.38	9.00		+5.38
2+80			5.22	15.48	8.75		+6.73
2+40			4.43	16.27	8.50		+7.77
2+00 T.P.	0.27	16.30	4.67	16.03	8.25		+7.78
1+60			0.66	15.64	8.00		+7.64
1+20			0.79	15.51	7.75		+7.76
0+80			1.05	15.25	7.50		+7.75
0+40			2.90	13.40	7.25		+6.15
0+00 = D ANH & Woodruff S			4.86	11.44 = 1143 Page 17	7.0 1.35	+444	+10.08
+41 25			2.14	14.16	1.45		+12.71
+82 50			1.86	14.44	1.55		+12.89
1+23 75			4.65	11.65	1.65		+10.00
1+65			7.78	8.52	1.76		+6.76
2+06 25			12.15	4.15	1.86		+2.29
2+47 50			12.83	3.47	1.96		+1.51
2+88 75			12.76	3.54	2.06		+1.38
3+30 M.H			12.43	3.87	2.17		+1.70

BIK 252

BLK 256 8" Line

	16.30				
3+30 MH.		12.43	3.87	2.17	+1.70
3+71.25		12.00	4.30	2.27	+2.03
4+12.50		11.84	4.46	2.38	+2.08
4+53.75 T.P. 5.63	10.34	11.59	4.71	2.48	+2.23
4+95		5.48	4.86	2.58	+2.28
5+36.25		5.06	5.28	2.69	+2.59
5+77.50		4.75	5.59	2.80	+2.79
6+18.75		4.62	5.72	2.90	+2.82
△ 8" 6+60 MH ℄ Yama T.P. 6.40 250.0	12.60	4.14	6.20	3.0	+3.20
7+10		6.43	6.17	3.12	+3.05
7+60		6.70	5.90	3.25	+2.65
8+10		6.58	6.02	3.37	+2.65
8+60		2.81	9.79	3.50	+6.29
9+10		6.28	6.32	3.62	+2.70
9+60		6.15	6.45	3.75	+2.70
10+10		5.98	6.62	3.87	+2.75
10+60.2 M.H. △ ℄ Yama T.P. 6.04 (40.0) ℄ Hwy	12.95	5.69	6.91	4.00	+2.91
11+04.7		5.53	7.42	4.11	+3.31
11+49.1		5.33	7.42	4.22	+3.40
11+93.5		5.15	7.80	4.33	+3.47
12+37.8 MH ℄ Collen wood △ T.P.		4.47	8.98	4.44	+4.04

BLK 256

N. of Yama

For BLK 5.7 ℄ Yama E to D.E. see page 28

Alley Blk 260 & 259

17.09

580' W of Yama: D.E.		4.51	12.58	7.50	+5.08
5+41 27 W		3.68	13.41	7.17	+6.24
4+93 33 W		4.25	12.84	6.83	+6.01
4+45 W		7.63	9.46	6.50	+2.96
	13.32				
3+96 67		2.21	11.11	6.17	+4.94
3+48 33 |		1.42	11.90	5.83	+6.07
3+00 MH V		2.61	10.71	5.50	+5.21
2+50		4.27	9.05	5.25	+3.80
2+00		6.01	7.31	5.00	+2.31
1+50		6.95	6.37	4.75	+1.62
1+00		7.00	6.32	4.50	+1.82
0+50		6.53	6.79	4.25	+2.54
=10+60.3 P27					
00 MH & Yama		6.41	6.91	4.00	+2.91
0+42.5		5.33	7.97	4.25	3.72
0+85		5.76	7.54	4.50	+3.04
1+27.5		4.86	8.44	4.75	+3.69
✓	12.95 P27				
1+70 MH & Alley		4.12	8.83	5.00	+3.83
0+35' S		4.15	8.80	5.20	+3.60
0+70 S - D.E.		5.75	7.20	5.40	+1.80
0+46.67 N		4.60	8.35	5.27	+3.08
0+93.33 N		4.42	8.53	5.54	+2.99
1+40' N: DE		4.05	8.90	5.80	+3.10

11 11
5.98
17.09

8.83
4.47
13.30
6.47
1.84

6.41
6.41
12.82

Hill-45 261-262-

		27.26			
00=B.F. Sta 4+0			6.94	20.32	13.50	+6.82
+51.5 +48			7.96	19.30	12.59	+6.71
1+03 +96			8.73	18.53	11.68	+6.85
1+54.5 1744	30' short		9.75	17.51	10.76	+6.75
2+06 1792		20.73	4.52	16.21	9.84	+6.37
2+57.6 MH. 2+40			5.95	14.78	8.92	+5.86
2+87.6 MH. 9+0 2.37	Below 9.68	22.26	6.11	14.62	8.0	+6.62
00=B.F. Wolfwoden			2.97	19.29	13.50	+5.79
+50			2.98	19.28	13.25	+6.03
1+00			3.60	18.66	13.00	+5.66
1+50			4.43	17.83	12.75	+5.08
2+00			4.55	17.71	12.56	+5.21
+50			3.67	18.59	12.25	+6.34
3+00 MH			3.80	18.46	12.00	+6.46
+50			3.98	18.28	11.77	+6.51
4+00			3.96	18.30	11.52	+6.78
+50	T.P. 2.70	20.73	4.23	18.03	11.30	+6.73
5+00			2.63	18.10	11.07	+7.03
+50			2.73	18.06	10.83	+7.17
6+00=MH & Vista			3.13	17.60	10.60	+7.00
6+50.4			3.63	17.10	10.17	+6.93
7+00.20			3.72	17.01	9.73	+7.28
7+51 20			4.86	15.87	9.30	+6.57
8+01 60			5.70	15.03	8.87	+6.16
8+52			6.36	14.37	8.43	+5.94
9+02 29 MH. ∆			6.11	14.62	8.00	+6.62

=2+57.6 above
=2+87.6

16.21
11.05
27.26

13.41
8.85
22.26

12.58
9.68
22.26

18.04
2.70
20.82
15.69
5.13
OK

18.07
2.75

20.77
2.70
1.03

Alley Blk 263

27.26 (P.29)

20=PE W of Alley			4.60	22.66	18.00	+4.66
+ 48.33			3.97	23.29	17.67	+5.62
+96.67			2.70	24.56	17.33	+7.23
1+45			1.43	25.83	17.00	+8.83
1+93.33			0.84	26.40	16.67	+9.73
2+41.67			1.18	26.08	16.33	+9.75
2+90 MH.			3.23	24.03	16.00	+8.03
	0.12	20.82	6.56	20.70		
3+40			0.76	20.06	13.17	+6.89
3+90			4.76	16.02	10.33	+5.73
4+40			8.15	12.67	7.50	+5.17
4+90			11.09	9.73	+4.67	+5.06
	T.P. 5.65	13.49	12 98	7.84		
5+40			16.26	7.23	+1.83	+5.40
Connection with 16" Line						
5+90 DMH & Thor.			9.66	3.83	−1.00	+4.83

Blks 265 - 266

00 DMH & Sewer connection	T.P. 3.73	6.89		3.16	−5.50	+8.66
+36			3.89	3.00	−5.25	+8.25
+72			4.22	2.67	−5.00	+7.67
1+08			4.63	2.26	−4.75	+7.01
1+44			4.57	2.32	−4.50	+6.82
1+80			5.07	1.82	−4.25	+6.07
2+16			4.84	2.09	−4.00	+6.09
2+52			5.34	1.53	−3.75	+5.28
2+88			4.77	2.12	−3.50	+5.62
3+24			4.60	2.29	−3.25	+5.54
3+60 MH.			5.43	1.46	−3.00	+4.46

Con Page 31

9.97 − 3.41 = 13.38 − 9.56 = 3.82

13.49 − 8.93 = 4.56

8.93 + 4.46 = 13.39

689

36.0 M.H			5.43	1.46	-3.00	+4.46
3+99			6.13	0.76	-2.75	+3.51
4+34			5.74	1.15	-2.50	+3.65
4+77			3.82	3.07	-2.75	+5.32
	TP. 6.38	11.90	1.37	5.52		
5+16			4.49	7.41	-2.00	+9.41
5+55			1.36	10.54	-1.75	+12.29
5+94			2.03	9.87	-1.50	+11.37
6+33			4.16	7.74	-1.25	+8.99
6+72			5.93	5.97	-1.00	+6.97
7+11			6.67	5.23	-0.75	+5.98
7+50 DE	40' W of Rigel		6.37	5.53	-0.5	+6.03

Alley N. of Cottonwood

BMs B--
16.70 Page 5

BM. & Thor					-4.00	+8.28
+40			12.58	4.12	-3.33	+7.45
+80			13.08	3.62	-2.47	+6.29
1+20 BrK			11.05	5.65	-2.00	+7.65
1+60			2.16	14.55	+8.00	+6.55
	TP 10.98	27.27	0.41	16.29		
12+00 DE			1.55	25.72	+18.00	+7.72

Blks 191-190-189
Hiway N. of Cottonwood

page 5

DM.H & Thor	5.15	9.43		4.28	-4.00	+ 8.28
+35			5.25	4.18	-3.84	+8.02
+70			5.19	4.24	-3.67	+7.91
1+05			4.91	4.52	-3.50	+8.02
1+40			5.20	4.23	-3.34	+7.57
1+75			5.16	4.27	-3.17	+7.44
2+10			5.01	4.42	-3.00	+7.42
2+45			5.00	4.43	-2.83	+7.26
2+80			4.58	4.85	-2.66	+7.51
3+15			4.53	4.90	-2.49	+7.39
3+50 M.H. (37)			4.46	4.97	-2.32	+7.29
3+87			7.00	2.43	-2.14	+4.57
4+24			4.76	4.67	-1.96	+6.63
4+61			4.79	4.64	-1.77	+6.41
4+98			5.25	4.18	-1.58	+5.76
5+35			5.58	3.85	-1.40	+5.25
5+72			5.27	4.16	-1.22	+5.38
6+09 T.P.	12.88	16.11	6.20	3.23	-1.04	+4.27
6+46			12.95	3.16	-0.86	+4.02
6+83			13.32	2.79	-0.68	+3.47
M.H. 30' W of 5+x a 7+20 (36)			12.54	3.53	-0.50	+4.03
7+56			12.80	3.31	-0.21	+3.52
7+92			10.03	6.08	+0.08	+6.00
8+28			5.93	10.18	+0.37	+9.81
8+64			2.39	13.72	+0.66	+13.06
9+00			1.14	14.97	+0.95	+14.02

12.88
-5.43
-6.11

Alleys Blks 191 - 190 - 198

16.11

9+36			0.98	15.13	1.24	+13.89
9+72			2.45	13.66	1.53	+12.13
10+08			3.91	12.20	1.81	+10.39
10+44			4.90	9.21	2.09	+8.12 +7.12
10+80 MH			11.07	5.04	2.37	+2.67
11+20			11.10	5.01	2.68	+2.33
11+60 Brk			6.48	9.63	3.00	+6.63
12+10	T.P. 8.89	24.93	0.07	16.04	8.50	+7.54
12+60 Brk			5.80	19.13	14.00	+5.13
13+10			4.60	20.33	14.25	+6.08
13+60			3.65	21.28	14.50	+6.78
14+10 110' W of Rigel			4.44	20.49	14.75	+5.74
14+60 DE			7.46	17.48	15.00	+2.48

Sewer Cons from M.H. ℄ Thor + Birch

S.E. on ℄ Birch to M.H. Δ + across Blks B-2934-262
To MH. ℄ Alley in Blk 262 Page 29

0 = M.H ℄ Thor + Birch	3.58	8.73	5.15	-3.53	+8.68	Page 5
+34.5			3.85	4.88	-3.37	+8.25
+69.0			3.80	4.93	-3.21	+8.14
1+03.5			4.11	4.62	-3.05	+7.67
1+38			4.30	4.43	-2.89	+7.32
1+72.5			4.30	4.43	-2.73	+7.16
2+07			4.57	4.16	-2.58	+6.74
2+41.5			4.66	4.07	-2.42	+6.49
2+76			4.75	3.98	-2.24	+6.24
3+10 E MH ℄ Birch Δ 34°33' R (33.6)			4.58	4.15	-2.10	+6.25
3+44 1			4.64	4.09	-1.94	+6.03
3+77 2			4.36	4.37	-1.78	+6.15
4+11 3			5.42	3.31	-1.62	+4.93
4+44 4			5.60	3.13	-1.46	+4.59
4+78 5			6.01	2.72	-1.30	+4.03
5+12 1			5.93	2.80	-1.14	+3.94
5+45 7			6.29	2.44	-0.98	+3.42
5+79 3 T.P.	10.81	13.39	6.15	2.58	-0.82	+3.40
6+12 9			7.52	5.87	-0.66	+6.53
6+46 E M.H. ℄ Alley Blk B (47.85)			7.84	5.55	-0.50	+6.05
6+94.3			5.37	8.02	-0.08	+8.10
7+42 1 T.P.	8.21	16.45	5.15	8.24	+0.34	+7.90 = +7.93 gone
7+89 3			10.42	6.03	+0.76	+5.27
8+37 7			9.64	6.81	+1.17	+5.64
8+85 5			10.28	6.17	1.59	+4.58
9+33 E MH ℄ Cottonwood			8.30	8.15	2.00	+6.15

Elev. Sub 0+30 Page 37 = 5.31 / 4.10 + / 9.41 = π

Re Checked on Account of Water

1941	4.95	4.46	-2.89	+7.35
	4.95	4.46	-2.73	+7.19
	5.20	4.21	-2.58	+6.79
	5.38	4.03	-2.42	+6.45
	5.51	3.90	-2.26	+6.16
	5.51	3.90	-2.10	+6.00

		16.45					
9+33.5 (47.85) MH			8.30	8.15	2.00	+6.15	
9+81.3			7.84	8.61	3.00	+5.61	
10+29.1			7.66	8.79	4.00	+4.79	
10+76.2			6.94	9.51	5.00	+4.51	
11+24.2			5.70	10.75	6.00	+4.75	8.10
11+72.5			4.03	12.42	7.00	+5.42	
12+20.5 = M.H. 9+02.39 Page 29				14.62	8.00	+6.62	
		Alley Blk B 13.39 Page 34					
00 = M.H. & Alley & Birch			7.84	5.55	-10.50	+6.05	31.38 / 5.65 / 25.73 = 25.72
+45			9.22	+4.17	0.00	+4.17	
+90 BrK (42.5)			4.15	9.24	+0.50 (4.87)	+8.74	
1+32.5 T.P.	11.35	24.04	0.70	12.69	5.37	+7.32	
1+75			5.72	18.32	10.25	+8.07	
2+17.5 T.P.	9.57	31.38	2.23	21.81	15.12	+6.69	
2+60 BrK (33.4)			4.18	27.20	20.00	+7.20	
2+93.6			2.94	28.44	23.00	+5.44	
3+27.24			2.68	28.70	26.00	+2.70	

Sewer Construction

Alleys 293 - 294 & 295

13.39 Page 34

00 = M.H. & Alley BK B			7.84	5.55	− 0.50	+6.05
+50			5.13	8.26	+1.25	(+7.01) +6.88 } gone
1+00			5.70	7.69	+3.00	(+4.69) +4.64 }
+50 T.P.	11.90	22.52	2.77	10.62	+4.75	+5.87
2+00 = BrK			7.82	14.70	+6.50	+8.20
2+45			7.31	15.21	7.26	+7.95
2+90			5.28	17.24	8.02	+9.22
3+35			5.22	17.30	8.78	+8.52
3+80 M.H.			8.36	14.16	9.54	+4.62
53.8 4+33.8	450.4	1700.8	9.96	12.56	10.32	+2.24
4+33.8		1700.8	6.37	16.15	11.10	+5.05
4+87.6		1751.2	3.86	18.66	11.88	+6.78
5+41		2+01.2	3.85	18.64	12.66	+5.98
5+95		2+52.8	3.16	19.36	13.44	+5.92
6+49		3+02.4	1.96	20.56	14.22	+6.34
7+02.8	M.H. & Vesta TP.	7.76	28.63	1.65	20.87	15.00
55						
7+57.8				4.76	21.87	15.50
8+12.8				5.81	22.82	16.00
8+67.8				5.98	22.65	16.50
9+22.8				4.64	23.99	17.00
9+77.8				4.23	24.40	17.50
10+32.8	M.H.			4.15	24.48	18.00
10+87.8				4.33	24.30	18.32
11+42.8				4.00	24.63	18.64
11+97.8				4.03	24.60	18.96
12+52.8				3.72	24.91	19.28
13+07.8				2.37	26.26	19.60
13+62.8	M.H. & Woden			1.41	27.22	19.91
						+7.31

Alley 295

28.63

13+62 50.7 MH dw. to TP. 4.71	31.43	1.41	27.22	19.91		+7.31
14+13 5		4.64	26.77	20.20		+6.57
14+64 5		5.45	25.98	20.50		+5.48
15+14 9		4.90	26.53	20.80		+5.73
15+65 6		3.06	28.37	21.10		+7.27
16+16 3		1.97	29.46	21.40		+8.06
16+67 0		0.43	31.00	21.70		+9.30
17+17 8 D.E. E. of wooden		1.50	29.93	22.00		+7.93

Alleys Blks C-302-301-300 & Etta St

17.70

Raised 0.83

2+78.2 00 = MH. 16" Linx & Blk C. Page 6		12.31	5.39	-2.00		+7.39	9.67	Rods
+30 2		12.40	5.30	-1.80		+7.10		436
+60 4		12.62	5.08	-1.60		+6.68		457
+90 9		12.72	4.98	-1.40		+6.38		467
1+21 2		12.80	4.90	-1.20		+6.10		476
1+51 5		12.40	4.90	-1.00		+5.90		473
1+82 0		13.03	4.67	-0.80		+5.47		498
2+12 3		13.03	4.67	-0.60		+5.27		498
2+42 7 MH. 35		12.74	4.96	-0.40		+5.36		469
2+77.7		12.96	5.44	-0.05		+5.49		430
3+12 7		12.12	5.58	+0.30		+5.28		1322
3+47 7		11.08	6.62	+0.65		+5.97		1215
3+82.7 Blk		2.16	15.54	+1.00		14.54		325

Same

T.P. 12.74 18.83 3.58 6.09

31.

Bm. 35.40 Alpha

Re-checked on Account of Water in Alley - Walker

Grades	Rods			
-2.00				
-1.80	436	5.31	-1.80	+7.11
-1.60	457	5.10	-1.60	+6.70
-1.40	467	5.00	-1.40	+6.40
-1.20	476	4.91	-1.20	+6.11
-1.00	473	4.94	-1.00	+5.94
-0.80	498	4.69	-0.80	+5.49
-0.60	498	4.69	-0.60	+5.29
-0.40	469	4.98	-0.40	+5.38
-0.05	430	5.37	-0.05	+5.42
+0.30	1322	5.61	+0.30	+5.31
+0.65	1215	6.68	+0.65	+6.03
+1.00	325	15.58	+1.00	+14.58

1106
452 -
1358
874 -
484 - TP
283 +
9.67 = X

		17.70						↑		
3+82 BK 45.2			2.16	15.54	+1.00		+14.54	1883		
4+29			0.05	17.65	+6.75		+10.90		1.16	17.67	6.75	+10.92
4+73.9 MH & Unpaved St 47.1 TP on C6 6.71		24.47	0.62 +0.06	17.08 17.76	+12.50		+4.58			
5+20			5.15	19.32	13.07		+6.25			
5+64			4.95	19.52	13.64		+5.88			
6+14			4.63	19.84	14.21		+5.23			
6+61			4.12	20.35	14.78		+5.57			
7+08			2.78	21.69	15.35		+6.34			
7+55			2.55	21.92	15.92		+6.00			
8+03 MH. 47	8.15	31.06	1.56	22.91	16.50		+6.41			
8+50			8.66	~2.40	17.04		+5.38			
8+97			7.86	~3.20	17.64		+5.56			
9+44			7.16	~3.90	18.21		+5.69			
9+91			6.89	~4.17	18.78		+5.39			
10+38			6.31	~4.75	19.35		+5.40			
10+85			5.79	~5.77	19.92		+5.85			
11+33 MH & Vesta 47			4.84	~6.72	20.50		~~+5.97~~ +5.72 6 Sour th			
11+80			3.37	~7.69	~1.42		+6.77			
12+27			~1.16	~8.90	22.25		+6.55			
12+74			0.85	30.21	~3.28		+6.93			
13+21.5 TP. 10.48		41.37	0.17	30.89	~4.21		+6.68			
13+68			9.68	31.69	25.14		+6.55			
14+15			8.89	~32.48	26.07		+6.41			
14+63 M.H.			8.53	~32.84	27.00		+5.84			

4/17

14+63 MH. 47 1					27.00	+5.84
15+10 1			5.04	33.33	27.50	+5.83
15+57 2			7.13	34.14	28.00	+6.14
16+04 4			7.13	34.14	28.50	+5.64
16+51 5			7.12	34.25	29.00	+5.25
16+98 6			6.35	35.07	29.50	+5.57
17+45 8			6.36	35.01	30.00	+5.01
17+93 MH. ℄ Woodin 46.33			4.81	36.56	30.50	+6.06
18+39 23			4.46	36.91	30.75	+6.16
18+85 67			4.16	37.21	31.00	+6.21
19+32			4.08	37.29	31.25	+6.04
19+78 33			4.39	36.98	31.50	+5.48
20+24 67			4.37	37.00	31.75	+5.25
20+71 MH. TP ℄ 39th St 4/3 52		4.18	3.53	37.84	32.00	+5.84
21+23			2.99	39.19		+6.19
21+75			1.67	40.51		+6.51
22+27			1.38	40.80	35.0	+5.80
22+79			0.96	41.22	36.0	+5.22
23+31 D.E. ℄ E 1a St			0.70	41.48	37.00	+4.48
℄ 39th St						
00=20+71 MH above			4.34	37.84	32.00	+5.84
+54			3.14	39.04	33.20	+5.84
1+08			1.84	40.34	34.20	+5.94
1+62	1.61	5.18	0.61	41.57	35.60	+5.97
2+16			11.52	42.66	36.80	+5.86
2+70 D.E.			11.08	43.10	38.00	+5.10

Ch. B.M.

54.18 Ch B.M. est 42/10/26

39.94
50.92
31
55.01
50.30

5039 BP School Math & E 42/10/26

E. on Vesta & Delta from MH 11+33 P. 38

11+33 = 00 = M.H. & Vesta Page 38	1 N 5 W	38.74		26 N	20.50	+5.7
1+55			11.47	N 7.77	21.313	+5.94
1+10			10.33	N 8.41	N 1.7	+6.24
1+65 M.H. & Vesta Delta			9.4	N 9.60	23.00	+6.60
2+16			7.50	3 1.24	N 5.50	+5.74
2+68			4.97	33.77	N 8.00	+5.79
3+19			2.43	36.31	30.50	+5.81
TP	11.90	49.96	0.68	38.06		
3+71			10.56	39.40	33.00	+6.40
4+23 M.H. & All-4 Spur			9.34	40.62	35.50	+5.12
4+74			5.38	41.58	36 N 8	+5.30
5+25			7.09	42.87	37.07	+5.80
5+76			5.80	44.16	37.85	+6.31
6+27			4.63	45.33	38.6	+6.69
6+78			4.0 N	45.94	39.44	+6.5 N
7+29			3.93	46.03	40.2 N	+5.81
7+80 M.H. & 39th St			3 N 6	46.70	41.00	+5.70
8+35			2 N 5	47.68	N 2.37	+5.31
8+90			0.9 N	49.04	43.75	+5.29
	1 S 9	6 N 0.3	0.2 N	49.74		
9+45			11.75	50.78	45.1 N	+5.16
10+00			10.43	51.60	46.50	+5.10
10+55			8.93	53.10	47.87	+5.23
11+10 MH			6.80	55.23	49.25	+5.98
11+65			4.3 L	57.67	50.64	+7.03
12+20			2.98	59.05	52.00	+7.05
12+75			1.40	60.63	53.37	+7.26
TP	13 N	74.60	0.65	61.38		
13+30			12.41	62.19	54.75	+7.44

Delta St
74.60

13+85	11.88	6v.7v	56,1v	+6.60
14+40 M.H. & H.H. 50 14	11.10	63.50	57.50	+6.00
14+90	10.18	64v	58.39	+6.03
15+40	9.34	65.v6	59.v8	+5.98
15+90	8.57	66.03	60.17	+5.84
16+40	8.37	66.v3	61.06	+5.17
16+90	7.71	66.89	61.95	+4.84
17+40 M.H. 48 33	6.18	68.4v	6v.84	+5.58
17+88 33	4.51	70.09	63.70	+6.39
18+36 67	3.47	71.13	64.56	+6.57
18+85	3.04	71.56	65.4v	+6.14
19+33 33	2.70	7v.40	66.v8	+6.12
19+81 67	1.49	73.11	67.14	+5.97
20+30 D.E.	0.19	74.49	68.00	+6.49

BlK B Edendale + BlKs 304+305

00=MH. ℄ 37th	3.44	10.99		7.55	-1.00	+8.55						
+36			2.88	8.11	-0.90	+9.01						
+72			3.47	7.52	-0.80	+8.32						
1+08			3.49	7.30	-0.70	+8.00						
1+44			3.64	7.35	-0.60	+7.95						
1+80			3.87	7.12	-0.50	+7.62						
2+16			3.97	7.02	-0.40	+7.42						
2+52			3.92	7.07	-0.30	+7.37						
2+88			4.34	6.65	-0.20	+6.85						
3+24			4.38	6.61	-0.10	+6.71						
3+60 MH			4.46	6.53	0.00	+6.53	427	10.80		6.53	0.00	+6.53
3+95			4.66	6.33	0.11	+6.22 ✓			4.48	6.33	0.11	+6.22
4+30			5.05	5.94	0.23	5.71 ✓			4.86	5.94	0.23	+5.71
4+65			4.94	6.05	0.34	5.71 ✓	This slak run over		4.86	5.94	0.34	+5.60
5+00			4.80	6.19	0.46	5.73 ✓			4.61	6.19	0.46	+5.73
5+35			4.82	6.17	0.57	+5.60 ✓			4.63	6.17	0.57	+5.60
5+70			4.62	6.37	0.69	+5.68 ✓			4.43	6.37	0.69	+5.68
6+05			4.95	6.04	0.80	+5.24 ✓	This slak was skipped on original Marking		4.74	4.04	0.80	+5.24
6+40			7.11	3.88	0.92	+2.96 ✓			6.92	3.88	0.92	+2.96
6+75			10.30	0.69	1.03	-0.34 ✓			10.11	0.69	1.03	-0.34
Now = 7+01 location intersection E Alleys					1.14							
7+10 MH. △ ℄ Alley Blk 304			7.73	3.26	+1.14	+2.12 ✓ -0.33			7.54	3.26	1.14	+2.12

Alley bet. Acacia + Birch Sts.
P. ⑤ Sheet 6
From Blk 304 West

Above MH. 7+10 ℄ Alley Blk 304

= 0+00 (6=46.67)		11.57	10.79	0.78	1.11	-0.33						
+46.7			5.73	5.84	3.09	+3.75						
T.S. 1159		22.95	0.21	11.36								
+93.3			10.67	12.33	5.07	+7.26						

Page 42
Elev Stub Sta. 7+10 = 3.26

3.26 + 8.31 = 11.57 = A
11.57 - 0.21 = 11.36 = TP
11.59 + 10.76 = 22.35 = A1

Walker

Alley Cont
Bet. Acacia + Birch
Blk. 304

1+40.01		22.95	8.02	14.93	7.05	+7.88				
+86.8			3.49	17.46	9.03	+8.43				
2+33.35			7.70	15.25	11.04	+4.24				
2+80=MH & Sta 8-42.5			4.79	18.16	13.00	+5.16				
3+22.5			2.49	20.46	13.27	+7.19				
+65.2			1.22	21.73	13.54	+8.19				
4+07.5			0.55	22.40	13.81	+8.59				
TP	4.09	26.49	0.55	22.40						
+50			3.55	22.94	14.08	+8.86				
+92.5			3.12	23.37	14.35	+9.02				
5+35			3.12	23.37	14.62	+8.75	MH			18.18
+77.5			3.44	23.05	14.89	+8.16	H3N			18.36	+0.36
6+20=MH, Blk. 305 6-58.33			4.98	21.51	15.16	+6.35	1 St P to 2	4.62	18.14	18.41	-0.27
6+73.33			6.29	20.20	15.50	+4.70	2 P to 3	6.10	16.66	18.46	-1.80
7+26.66			5.97	21.02	15.84	+5.18	3	8.17	14.57	18.51	-3.94
+79.99			6.52	19.99	16.18	+3.81	4	6.58	16.17	18.56	-2.39
8+33.32			6.70	19.79	16.52	+3.27	E.C.E.	5.37	19.37	18.61	+1.24
+96.65			4.06	22.43	16.86	+5.57	4 B	1.44	21.33	18.81	+2.52
9+40=MH & Rigol + Alley 6-40 TP 6.82		30.13	3.18	23.31	17.20	+6.11						
9+80			6.52	23.61	17.36	+6.25						
10+20			6.47	23.66	17.53	+6.13						
10+60			6.48	23.65	17.69	+5.96						
11+00			5.85	24.28	17.86	+6.42						
11+40			5.39	24.74	18.02	+6.72						
11+80=End MH, Blk. 306 1-43			7.89	22.24	18.18	+4.06						
12+23			11.21	18.92	18.36	+0.56						
12+35=1st Pier con.			11.99	18.14	18.41	-0.27						

22.95=K
0.55-
22.40=TP
4.09+
26.49=K
3.18-
23.31=K
6.82+
30.13=K
6.52-
23.61=TP

Elev Stub & Rigol = 23.31=TP
6.82+
30.13=K
11.99-
18.14=TP

18.18
4.54
22.72

18.92
3.45
22.37

4.54
18.18

3.89
.55
4.44
18.72

3.46
.55
4.01 18.75 0.62 low

Alley Cont.

bet. Acacia + Birch

Blk. 304

12+17 = 2nd Cor. Per	24.94	8.28	16.66	18.36	− 18.0
+59 = 3rd Cor. Per		10.37	14.57	18.51	− 3.94
+71 = 4th Cor. Per		8.77	16.17	18.56	− 7.39
12+83		7.57	17.37	18.61	− 1.24
13+31.5		3.61	21.33	18.81	+ 7.52
13+80 = D.E. SL. Boston bet. Birch + Acacia		3.71	21.73	19.00	+ 2.23
14+09 = D.E.		4.15 Rigel St. 6"	20.79	19.12	+ 1.67

From ℄ Alley bet. BIRCH + Acacia sts. to ℄ Acacia + Alley produced thence East thru. Blk. 9. to D.E.

9+40 ℄ N.4 Rigel St. Page 43					
= 0+00	34.13			17.20	
0+48.42		8.77	25.36	18.90	+ 6.46
0+96.84		7.52	26.61	20.60	+ 6.01
1+45.77		6.65	27.48	22.30	+ 5.48
1+93.7 = ℄ MH. ind. Acacia + Alley		5.09	29.04	24.00	+ 5.04
2+43.7		4.93	29.20	24.75	+ 4.45
+93.7		5.33	28.80	25.99	+ 3.31
3+43.7		3.62	30.51	26.24	+ 4.27
+93.7		2.52	31.61	26.98	+ 4.63
4+43.7		1.41	32.72	27.73	+ 4.99
4+93.7 = ℄ MH. B&G	39.58	6.09	33.49	28.47	+ 5.07
5+47.7		4.25	35.33	29.28	+ 6.05
6+01.7		4.37	35.21	30.28	+ 5.13
+55.7		3.66	35.92	30.89	+ 5.03
7+09.7		3.06	36.52	31.69	+ 4.83
7+63.7 = DE		2.35	37.23	32.50	+ 4.73
+73.7 = DE = 40' W. of L 31st		1.94	37.64	32.65	+ 4.99

18.14 = TP
6.80 +
24.94 = A
.890 −
24.04 = TP
4.33
28.37
5.07
23.30
2.301 = Elev
0.01 Stub

Sta. 9+40 page 43. Elev Stub = 23.31
10.87 +
34.13 = A
1.46 −
32.67 = TP
.691 +
33.55 = A
1.05 −
Sta 2+60 page 36 = Elev Stub NE = 28.53 = V

Delta Spur M.H. Sta. 4+23 = 0+00 to 39th
Stood on 0+00 Thru DIKE "Arlington" Thence East on Epsilon 38.06.

4+23 = 0+00	907	4713	6.50	40.63	35.50	+5.13
0+46			5.77	41.36	35.79	+5.64
0+90			4.90	42.43	35.93	+6.50
1+38			4.89	42.98	36.15	+6.09
1+84			6.40	40.93	36.36	+4.57
2+30 = MH 41.14			6.39	40.74	36.58	+4.16
2+77.14			6.71	40.42	36.76	+3.66
3+24.28	T.P. 6.85	49.13	4.85 / 7.18	42.28 / 41.95	36.94	+5.01
3+71.44			6.47	42.86	37.13	+5.73
4+18.56			5.49	43.64	37.31	+6.33
4+65.7 = MH E 39th			5.43	43.90	37.50	+6.40
5+06.95			5.61	43.57	37.75	+5.77
5+48.40 MH & Epsilon			5.66	43.47	38.00	+5.47
5+98.40			4.41	44.72	38.72	+6.00
6+48.40			3.53	45.60	39.44	+6.16
6+98.40			2.49	46.64	40.16	+6.48
7+48.40			1.83	47.30	40.88	+6.42
7+98.40			1.54	47.59	41.60	+5.99
8+48.40 MH			1.35	47.78	41.73	+5.46
8+58.0 9+06.40	T.P. 6.39	5488	1.03 / 0.64	48.10 / 48.49	43.16	+4.94
9+64.40			5.57	49.31	44.00	+5.31
10+14.40			5.06	49.81	44.83	+4.99
10+80.40			3.44	51.46	45.67	+5.79
11+38.40 = DE			2.01	52.87	46.50	+6.37
	CH BM 5039		4.59	50.74		
	School House					

39th ST
Epsilon to Delta
49.13 π

46.57.00	5.73	+3.9°	37.50	+6.40	
5.75	4.95	44.18	38.12	+6.06	
"	4.94	44.19	38.75	+5.44	
"	4.39	44.74	39.37	+5.37	
5+10 = DE	3.97	45.16	40.00	+5.16	

Walker

Sewer Construction From point 40' West 40+54 on ℄ Gamma (= O.E.) West to ℄ 39th thence South to ℄ Alley Blk 417 thence West thru. Blk 417 bet. Gamma + Delta thence North to ℄ 38th + Beta thence West to ℄ 37th + Beta = Station 26+29.3 = Sta. 718.5 Page 6
(Plan Sheet 3 + 6) Profile Sheet 4

40' West WL 40th St = 0+00 = OE (3-50)	86.38	5.05	81.33	70.50		+10.83
+50		3.50	81.88	69.33		+13.55
1+00		6.57	79.81	68.16		+11.65
1+50 = Dr ℄ (3-46.67 T.P. 1.22)	74.55	13.05 (13.05)	73.33 (79.33)	67.00		+ 6.33
+96.67		6.39	68.16	63.50		+4.66
2+43.34		9.95	64.60	60.00		+4.60
2+90 = ℄ MH (4-50 T.P. 1.43)	63.41	11.95 (12.57)	62.60 (61.98)	56.50		+ 6.10
3+40		4.08	59.33	54.75		+4.58
+90		5.97	57.44	53.00		+4.44
4+40		7.61	55.80	51.75		+4.55
+90		9.36	54.05	49.50		+4.55
5+40		10.90	52.51	47.75		+4.76
5+90 = MH ℄ Gamma (4-42.45 T.P. 2.60)	+39th 54.13	11.88 (11.88)	51.53 (51.53)	46.00		+5.53
6+37.45		3.70	50.43	45.75		+5.18
+84.90		4.28	49.85	44.50		+5.35
7+32.35		4.55	49.58	43.75		+5.83
7+79.80 = MH ℄ 39th + Alley (6-47.5)		5.05	49.08	43.00		+6.08
8+27.3		5.47	48.66	42.50		+6.16
8+74.8		6.20	47.93	42.00		+5.93
9+22.3		6.53	47.60	41.50		+6.10
9+69.8		6.84	47.29	41.00		+6.29
10+17.3		7.50	46.63	40.50		+6.13
10+64.5 = MH 3.85 W ℄ 38th (6-47.23)		8.62	45.51	40.00		+5.51
11+12.03		8.98	45.15	38.66		+6.49
+59.26		9.97	44.16	37.33		+6.83

Cont. on Page 53

1+40 Page 41 = BM = MH ℄ 40th + Delta

63.50
12.54 +
76.04
0.25 -
75.79 = T.P.
10.59 +
86.38 = π
1.80 -
73.33 = T.P.
1.22 +
74.55 = π
1.57 -
61.98 = T.P.
1.43 +
63.41 = π
1.88 -
51.53 = T.P.
2.60 +
54.13 = π

Walker

Alley Bet. Boston & Newton Aves.

From a Point on Main Line West 590'
(See profile = 9)

B.M. on stub at sta. 26+85.6 on Main Line	9.61	33.93		24.32		
= 0+00			9.61	24.32	16.40	+7.92
+45.71			10.89	23.04	16.98	+6.06
+91.42			9.45	24.48	17.57	+6.91
1+37.13			9.40	24.53	18.15	+6.38
+82.84			9.45	24.48	18.74	+5.74
2+28.55			9.67	24.26	19.32	+4.94
+73.26			9.88	24.05	19.91	+4.14
3+20 = P.C.			9.97	23.96	20.50	+3.46
+65			5.67	28.26	21.42	+6.84
4+10			2.86	31.07	22.33	+8.74
+55			2.41	31.52	23.25	+8.27
5+00			1.58	32.35	24.16	+8.19
+45 T.P.	2.37	45.87	0.43 / 0.43	33.50 / 33.50	25.08	+8.42
5+90 = P.E.			10.97	34.85	26.00	+8.85
T.P.	12.30	55.21	0.11	45.71		
T.P.	11.43	68.21	1.40 / 2.84	56.81 / 65.40	4 of 4th & Nail,	
			2.91	653.3 = B.M. SW top Hydt. / 0.07		

See Plan & Profile - 5

Alley Bet. Alpha & Z Sts.

From ℄ 39th St. 12.50' West

38th & Alpha SW B.M. 11.06 + 5.50 = 16.96 − 1.0 = 15.92 + 3.09 = 19.01

26+08 Page 8 = 0+00		19.81	4.80	15.01	3.25	+10.96
+50			5.47	13.59	3.47	+10.12
1+00 T.P.	6.69	16.70	6.88 / 9.50	17.13 / 9.51	3.69	+8.44
+50			5.99	10.78	3.91	+6.87
2+00			10.37	5.83	4.13	+1.70

Walker Alley Bet. ALPHA + Z Sts
Cont.

		↑ 16.70				
2+50			9.97	6.23	4.35	+1.88
3+00			5.84	7.36	4.57	+2.79
+50			1.72	14.18	4.79	+9.69
T.P.	5.54	21.56	0.18	16.02		
4+00=MH.			5.68	15.88	5.0	+10.88
4+50			6.95	14.61	5.38	+9.23
5+00			7.05	14.51	5.75	+8.76
5+50			6.49	15.07	6.13	+8.94
6+00			6.74	14.82	6.50	+8.32
+50			5.83	15.73	6.88	+8.85
7+00			6.92	14.64	7.26	+7.38
+50			8.21	13.35	7.63	+5.72
8+00=MH.			8.25	13.31	8.00	+5.31
+50			5.35	16.21	8.37	+7.84
T.P.	2.11	30.32	3.21	18.15		
9+00			3.57	14.40	8.75	+5.65
T.P.	5.10	32.58	2.84	17.48		
+50			5.62	16.96	9.12	+7.84
10+00			6.63	15.95	9.51	+6.44
+50			11.27	11.31	9.88	+1.43
11+00=MH			15.67	16.96	10.25	+6.71
T.P.	3.25	13.37	12.51	20.07		
+50			5.0	18.37	11.63	+6.74
12+00			2.77	20.55	13.42	+7.13
12+50=DE.			2.67	20.65	15.00	+5.65
T.P.	1.75	14.97	1.31	20.22		
T.P.			3.88	11.09	Unknown	
				11.06		
				0.03		

Sewer Const Alpha. Street from ℄ 39th st. East 590'
(Profile sh. 5)
Walker

B.M. 38th ALPHA 8.60 19.66			11.06			
DMH ℄ 39th						
= 0+00		4.79	14.87	8.00		+6.87
0-51.43						
+51.43		4.66	15.00	8.23		+6.77
1+02.86		4.94	14.72	8.46		+6.26
+54.3		5.37	14.34	8.69		+5.65
1+05.7		4.91	14.75	8.92		+5.83
+57.16		4.60	15.06	9.15		+5.91
1+08.6		4.16	15.50	9.38		+6.12
1+60 = MH.		4.25	15.41	9.60		+5.81
1+10		3.63	16.03	10.80		+5.23
1+60 = BL 1.27	19.36	2.97	16.69	12.00		+4.69
		2.77	16.69			
2+03.33		7.73	11.63	16.00		+5.63
2+46.7		7.47	11.89	20.00		+6.89
2+90 = DE		0.77	18.59	24.00		+4.59 = Ck. Ground (Profile)

Z st. from a Point 40' East EL 38+4
to 6" line ℄ 39+4 st.

40' E EL 38+4						
= 0+00 = DE	38.83	1.39	37.44	31.50		+5.94
0-48.33						
0+48.33		2.77	36.56	30.06		+6.50
+96.66		3.48	35.35	28.62		+6.73
1+45		4.27	34.56	27.18		+7.38
1+93.33		5.58	33.25	25.74		+7.51
2+41.66		8.49	30.34	24.30		+6.04
2+90 = MH.		10.10	28.73	22.86		+5.85
2-50.						
3+40		11.25	27.58	21.40		+6.18
3+90		11.41	27.42	19.92		+7.50

cont. Page 50

38+4
11.06 = 87. St. Alpha
12.44 +
23.50
0.04 −
23.46
12.50 +
35.96 =
1.26 −
34.70
0.19
38.83 = T

4+40 T.P.	1.26	38.83 / 27.39	12.70 / 12.70	26.13 / 2.13	18.40	+ 7.69	
4+90			2.30	25.09	16.96	+ 8.13	
5+40			4.97	27.47	15.45	+ 6.94	
5+90 = ONH & 39th			8.94	15.45	14.00 / 10.00	+ 4.45	+ 8.45
		39th St + NWly Across Blk.					
		422 + 423					
		From Alley bet. Alpha & Z sts to Alley bet. National & Newton Aves. (See Page 5)					
℄ 39th st + Alley Bet Alpha + Z st. = 0+00		19.37	5.21	14.16	3.25	+ 10.91	
+40			5.35	14.02	3.67	+ 10.35	
+80			10.68	8.69	4.09	+ 4.60	
1+20 = B.k			10.28	9.09	4.50	+ 4.59	
1+55 T.P.	11.99	30.48	1.63 / 0.85	17.74 / 15.49	7.75	+ 10.49	
1+90 = ONH & Z st. (4-27.45)			12.05 above	18.43	14.00 / 10.00	+ 4.45	+ 0.04
2+37.45			9.91	20.57	10.50	+ 10.07	
2+84.90			5.39	25.09	11.00	+ 14.09	
3+37.35			6.27	24.71	11.50	+ 12.71	
3+79.80 (8-50.9)	∠ 20°37' = ONH Alley bet Z st. + Preston		9.47	21.01	12.00 / 18.00	+ 9.01	
4+30.7 T.P.			3.56	26.97	20.65	+ 6.77	
4+81.6 T.P.	13.17	43.60	0.00 / 0.00	30.48 / 30.48	23.30	+ 7.18	
5+32.5			5.56	38.04	25.95	+ 12.09	
5+83.4			8.47	35.18	28.60	+ 6.58	
6+34.3			5.56	38.04	31.25	+ 6.79	
6+85.2 T.P.	10.67	54.08	3.85 / 1.19	39.75 / 42.41	33.90	+ 5.85	
7+36.1			8.83	45.25	36.55	+ 8.70	

Cont'd Page 51

4.82
11.03
15.85

3883
12.70
26.13
1.26
27.39 = ↗
9.65 −
17.74
1.63
19.37 = ↗

10.00
10.41
20.41

1.30
19.11

3.25
15.85
19.10

1.30
17.80

10.40
8.70

19.37
0.88 −
18.49
11.99 +
30.48 = ↗
0.80 −
30.48
13.12 +
43.60 = ↗
1.19 −
42.41
11.67 +
54.08 − ↗

5.06
9.06 10.04
19.10
4.99
5.95
10.85
8.25
3.88
12.13
4.50
7.63
.55
7.08

14.04
2.67
+10.37

8.25
4.58
+3.67

7.99
4.84
3.15

12.13
2.09
10.04
4.07
2.97

Walker — 39th St N&Sly Cont. From Page 50

7+87.2 (9-28.69) = DMH & alley Bet Newton & Boston	Δ 9°02' L	54.08 (57.02)	10.92	46.10 Stake Shifted	57.02 / 10.92 / 46.10 / 39.20	40.60	+ 6.90	+ 5.50
8+35.69		57.02	11.49	45.53	43.09		+ 2.44	+ 4.50
8+84.39			8.54	45.48	45.58		+ 2.90	Δ 9°02' = 45.10 = Elev Stub
9+33.09	12.79	69.43	3.88 / 0.38	53.14 / 56.64	48.07		+ 5.07	11.97+ / 57.02 / 0.38- / 56.64 = TP
9+81.78			7.70	61.73	50.56		+ 11.17	12.79+ / 69.43 = X
10+30.99			6.33	63.10	53.05		+ 10.05	0.11- / 69.32 = TP
10+79.19			10.72	58.71	55.54		+ 3.17	12.07+ / 81.39 = X
11+27.99			4.35	65.08	58.03		+ 7.05	see page 52 for
11+76.58			2.69 / 2.09	66.74	60.51		+ 6.23	Redmon, Haldrod and E instead offset
12+25.27 = MH & alley Bet 38th & Newton Ave.				67.34	63.00		+ 4.34	See Sta 225-27 page 52 for correction

{From 39th St 430' East See Page 55} Alley Bet. Boston Ave. + Z St. (Profile & Plan)

From ℄ 39th St West 590' Block 421 Duncans Addition

3+79.8 Page 50 = 0+00 = ℄ 39th DMH		33.38			12.00 / 18.00		+ 9.01	Sta. 3+79.8 Page 50 BM on Stub of ℄ +3.01
0+50			7.15	26.23	19.50		+ 6.73	
1+00 = Brk			6.13 / 0.27	32.75 / 33.11	21.00		+ 6.25	
1+46.66		25.65	1152	34.13	27.67		+ 6.46	
1+92.33 TP	12.09	57.67	6.15 / 0.07	39.54 / 45.58	34.33		+ 5.91	
2+40 = Brk			12.20	45.47	41.00		+ 4.47	
2+90 TP	12.69	70.24	2.71 / 0.12	54.96 / 57.53	49.30		+ 5.46	
3+40 = MH			7.61	62.63	58.00		+ 4.63	
3+90 TP	2.24	72.46	2.19 / 0.02	68.05 / 70.22	58.60		+ 5.45	
4+40			1.89	70.57	59.20		+ 11.37	
4+90			1.35	71.11	59.80		+ 11.31	
5+40			5.76	66.70	60.40		+ 6.30	
5+90 = DE = 40'EE ℄ 38th St		8.67	63.75		61.00		+ 2.79	Chk on 0+00 on Z St. Page 49 = Elev. DE = 37.44

5408 − 0.80 = 53.28 + 12.89 = 66.17 − 0.69 = TP 6548 + 12.51 = 77.99 − 0.18 = TP 77.81 + 6.00 = 83.81 − 7.30 = Chk on 0+00 = 76.51 = BM + 0.07

21.01 + 12.37 = 33.38 − 0.27 = 33.11 = TP + 12.54 = 45.65 = X − 0.07 = 45.58 = TP + 12.09 = 57.67 = X − 0.12 = 57.55 = TP + 12.69 = 70.24 = X − 0.02 = 70.22 = TP + 2.24 = 72.46 = X − 1.31 = 59.32 = TP + 0.60 = 59.92 + 12.69 = 47.23 = TP + 3.01 = 50.24 − 12.82 = 37.42 − 0.02

Alley Bet Boston & Newton Aves. From 38th to 39th St.

(Prof. No. 9 Sheet 2)

B.M. S.E.B.P. 38th + Nott.						
40' East EL 38th St.	2.70	79.28		76.58		
= 0+00 = DE			5.38	73.90	69.50	+ 4.40
4-48.63	T.P. 0.54	74.44	5.38	73.90		
0+48.63			2.45	71.99	67.62	+ 4.37
+97.24			2.95	71.49	65.75	+ 5.74
1+45.87			1.84	69.60	63.87	+ 5.73
1+94.5 = DMH			7.63	66.81	62.00 / 58.50	+ 4.81
9-22.5						+ 8.31
2+37			8.84	65.60	57.12	+ 8.48
+79.5			8.91	65.53	55.75	+ 9.78
3+20.0	T.P. 0.06	61.31	11.59	67.85	54.37	+ 8.48
+64.5 = Brk.			13.19	61.75		
			2.48	58.83	53.00	+ 5.83
4+04.5			9.18	57.13	46.10	+ 6.03
4+44.5 = DMH = Sta. 2+37.79 page 51			15.14	46.17	39.20	- 0.07 + 2.90 + 5.50
2-37.79						
4+82.24			17.04	41.27	39.85	+ 1.42
5+20 = DE = 40'W 39th St.			9.07	52.42	40.50	+ 11.76

Alley Bet Newton + Nott. Aves. From 38th to 39th St.

(Prof. No. 9 Sheet 2)

40'E EL 38th St.		81.34 (From Page 51)				
= 0+00 = DE.			3.45	77.89	74.00	+ 3.89
3-41.75						
+41.75			1.89	79.45	72.67	+ 6.78
+ 83.5			3.64	77.70	71.33	+ 6.37
1+25.26 = Brk.			5.38	75.96	70.00	+ 5.96
2-50						
1+75.26			9.59	71.25	66.50	+ 5.25
2+25.26 = MH = Sta. 1+25.26 page 51			13.18	68.16	63.00	+ 5.16
6-49.12						
2+74.38			10.12	71.22	64.83	+ 6.39
3+23.51			5.55	75.79	66.66	+ 9.13
3+72.63			3.21	78.13	68.50	+ 9.63
4+21.76			2.51	78.83	70.33	+ 8.50

Contan opposite page

Continuation of Alley bet. Newton + Nott.

81.34						
4+70.88		2.12	79.22	72.16	+ 7.06	
5+20 = DE = 40'W 39th St.		1.64	79.70	74.00	5.70	

H.I. from page 51 = 81.34

1.31 -

80.03 = T.P.

3.94 +

83.97

7.44 -

76.53

76.58 = B.M. 38th + Nott.

+ 0.05

38th + Nott.

76.58 = B.M.

2.70 +

79.28

5.38

73.90 = T.P.

0.54 +

74.44 = π

1.19 -

73.25 = T.P.

0.06

61.31

15.14

46.17 = ℄ on Station 2+37 p. 51

4+70.88 = 44.17 = ℄ on Station 2+37 p. 51

Cont. from page 46

12+06.5		5413	10.56	43.57	36.00	+7.57	5413=A
+53.73			11.60	42.53	34.66	+7.87	1326
13+00.96			13.26	40.87	33.33	+7.54	4087=TP
TP 1.29		4216	13.26	40.87			129+
13+48.7 = M.H. & Blk. 17			4.15	38.0	32.00	+6.01	4216=A
3-47.66							1253
13+95.86			7.07	35.09	24.66	+10.43	2963=TP
							1637
14+43.52			9.65	37.51	17.33	+15.18	3176=A
TP		1932					1381
14+91.7 = M.H. El 38th st + Alley △			1.69	17.63	10.00	+7.63	1045=TP
2-35.5							087
15+26.7			4.55	14.77	8.50	+6.27	1932=A
							779
15+62.7 = D.M.H 38th st + alley produced			6.34	12.98	7.00 4.00	+5.98	+598
5-43.42							
16+05.62			8.18	11.14	3.50	+7.34	953=TP
							3304
+49.04			8.43	10.89	3.60	+7.29	1283=A
+92.46			8.58	10.74	3.40	+7.34	For CK see page 54
17+35.88			8.71	10.61	3.20	+7.41	
17+79.3 = M.H. Bet Gamma + Beta on 38th			9.07	10.25	3.00	+7.25	
4-47.5							
18+26.8			9.25	10.07	2.75	+7.32	
+74.3			9.36	9.96	2.50	+7.46	
19+21.8			9.42	9.90	2.25	+7.65	
19+69.3 = M.H. & Beta + 38th			9.79	9.53	2.00	+7.53	
7-47.14 TP 3.30		1283	9.79	9.53			
20+16.44			3.30	9.53	1.72	+7.81	
+63.58			3.80	9.03	1.44	+7.59	
21+10.73			4.39	8.44	1.15	+7.29	
+57.87			4.46	8.37	0.87	+7.50	
22+05.01			4.73	8.10	0.58	+7.52	
+52.16			4.83	8.00	0.29	+7.71	
22+99.3 M.H. = bet 38th + 37th on Beta			4.95	7.88	0.00	+7.88	

Cont. on page 54

7-47.14

Cont. from page 53

				El.		
23+46.44	12.63	4.93	7.90	-0.18	+8.08	12.83=T
+93.56		5.17	7.66	-0.36	+8.02	9.53
24+40.73		5.66	7.17	-0.54	+7.71	4.97+
24+87.87		5.71	7.12	-0.72	+7.84	1.450
25+35.01		6.05	6.78	-0.90	+7.68	3.45-
25+82.16		6.68	6.15	-1.08	+7.23	11.03
26+29.3	=DM.H. & 37½ Beta = Sta. 7+16.2 page 6			-1.25		11.06=BM
						+0.01 38th & Alton

Alley N.E. of Acacia

from 38th St. & Alley produced to

1+57.2 Page 53 Point 3 28' N&S (=DE)

7=0+00=DM.H.	19.32	6.34	12.98	4.00	+8.98	+5.98
+4.87		6.49	12.83	4.21	+8.62	
+93.73		6.94	12.38	4.42	+7.96	
1+40.59		10.38	8.94	4.64	+4.30	
1+87.45		11.07	8.30	4.85	+3.45	
2+34.3		11.37	7.95	5.07	+2.88	
2+81.15		11.66	7.66	5.29	+2.37	
3+28=DE		11.87	7.45	5.50	+1.95	

6.15
5.13
1.02
1.03

Alley Bet Gamma + Beta Sts.
From ℄ 38th St. East 590' (Profile 4 Sheet 6)

17+79.8 Page 53	23.48					
8.46.5						
= 0+00				3.00	= Ins Cut see Page 23	
+46.25		12.88	10.60	3.50	+7.10	
+92.5		12.79	10.69	4.00	+6.69	
1+38.75		12.65	10.83	4.50	+6.33	
+85.0		12.68	10.80	5.00	+5.80	
2+31.25		12.09	11.39	5.50	+5.99	
2+77.5		11.84	11.64	6.00	+5.64	
3+23.75		11.45	12.03	6.50	+5.53	
3+70 = MH		8.84	14.64	7.00	+7.64	
4.44.5						
4+12.5 TP 12.93	36.29	1.77	21.71	16.75	+4.96	
		0.14	23.34			
4+55 TP 12.71	48.75	2.72	33.57	26.50	+7.09	
		0.25	36.04			
4+97.5 TP 10.78	58.88	7.23	41.52	36.25	+5.27	
		0.65	48.10			
5+40 = Brk		7.67	51.21	46.00	+5.21	
5+90 = DE = 40' NWLy 39th St		3.70	55.18	50.00	+5.18 → Note: Line Extended 5-19-43 See Page 21	

Alley Bet. Boston Ave & Z Sts. (Profile 8 Sheet 7)
(From 39th St 595' West See Page 51) From ℄ 39th St to a Point 490' East = DE

Elev. M.H. Stub Sta. 3+79.8 Page 50						21.01
Stub 3+32.8 Page 50						4.93+
= 0+00	25.94	4.93	21.01	12.00	+9.01	25.94-T
0+47.79		7.24	18.70	12.19	+5.98 +6.51	1.73-
+95.56		9.02	16.92	12.38	+3.48 +4.54	24.21
1+43.34		8.95	16.99	12.57	+4.83 +4.42	Chk. on Stub 3+32.8 Page 50 Elev. = 24.21
+91.12		8.56	17.38	12.76	+2.50 +4.62	0.00
2+38.9		8.08	17.86	12.95	+4.26 +4.91	
+86.68		7.75	18.19	13.14	+1.87 +5.05	
3+34.46		7.73	18.21	13.32	+1.17 +4.89	
3+84.43 = DE		7.24	18.70	13.50	+0.93 5.20	
4+30 = DE this Leftout.						

17+79.8 Page 53 = Elev M.H. Stub
10.25
1.33
2.345 = T
0.14
2.334 = TP
12.93
36.29 = T
0.25
36.04 = TP
12.71
48.75 = T
0.65
48.10 = TP
10.78
58.88 = T
7.35
51.53 = Elev. Stub Sta 5+90 Page 46

Siva St.

From ℄ Alley Bet. Acacia + Birch Sts to ℄ Acacia (Profile Sheet 5)

2+80 Page 43 = 0+00		30.35	12.22	18.13	13.00	+ 5.13
+ 47.5			8.98	V 13.7	14.50	+ 6.87
+ 95.0			7.66	V 11.69	16.00	+ 6.69
1+42.5			7.26	V 3.09	17.50	+ 5.59
1+90 =	MH ℄ Acacia St.		4.77	V 5.58	19.00	+ 6.58

Elev. from below

Acacia St.

From DE. 70'S East of Siva St (Profile Sheet 6)
to " " 190' N.W. of Siva St.

70'S East ℄ Siva St = 0+00		28.46	3.36	25.10	20.00	+ 5.10
0+35			3.20	2.526	19.50	+ 5.76
+ 70 = 1+90 = above MH.			2.88	2.558	19.00	+ 6.58
1+17.5			3.15	2.531	20.00	+ 5.31
+ 65.0			1.67	2.679	21.00	+ 5.79
2+12.5 TP	2.09	30.35	0.72 / 0.20	V 7.74 / 2.26	22.00	+ 5.74
+ 60.0 = DE 190' N.W. of ℄ Siva St			1.85	V 8.50	23.90	+ 5.50

30.35
12.22
18.13 = TP
1.26 +
19.39
9.59 -
9.80 = TP
1.57 +
11.37
8.31
3.26 = Elev. Stub
Sta. 7+10 Page 42

Page 42 Elev. Stub of Sta. 7+10 = 3.26
12.97 +
16.23 = A
0.27 -
15.96 = T.P.
12.50 +
28.46 = A
0.20 -
28.26 = TP
2.69 +
30.95 = A
12.22 -
18.13 = TP

Line A 1065 Bks. 528 Bet Alley North of Boston & Alley South of National Ave
From existing MH in Blk 5 to P.H. 12.65 EAST EL 34th West W/L 36th St. in Blk 8, thence East to D.E. approximately 40 Sept. 12 17 Sheet 5

existing MH at Alley Wd. North + Newton = 0+00					1.09	
5-43.86 TP	4+14	10.96	824	2.72	2.00	+ 0.72 Flow line must be lowered
	8.47	18.60	00.83	10.13		
+ 43.86			5.33	1327	2.30	+ 1.97
+ 87.72			7.17	1143	2.60	+ 8.83
1+31.58			1398	468	2.90	+ 1.72 -
+ 75.44			973	887	3.20	+ 5.67 - F.C.
2+19.30 = MH & Newton Δ			406	1454	3.50	+ 11.04
4-49.5						
+ 66.8			6.57	1203	3.87	+ 8.16
3+14.3			640	1220	4.25	+ 7.95
+ 61.8						
TP	9.34	20.37	780	1580	4.62	+ 11.18
			1.37	1 1.03		
4+09.3 = MH & Alley 12.65 EL 34th			1234	803	5.00	+ 3.03
7-37.6						
+ 46.9			12.02	8.35	5.25	+ 3.10
4+84.5 = Blk			1260	777	5.50	+ 7.27
3-53.33 TP	12.97	32.47	0.37	20.00		
5+37.83			11.20	21.27	10.67	+ 10.60
+ 91.16			636	2611	15.84	+ 10.77
6+42.5 = MH west of 35th			452	2795	21.00	+ 6.95
5-53.3						
+ 97.8			2.90	2957	22.40	+ 7.17
7+51.10			2.65	2987	23.80	+ 6.07
8+04.4			074	3173	25.20	+ 6.53
8+57.7 TP	11.21	42.94	0.74	31.73		
			858	3436	26.60	+ 7.76
9+11 = MH & 35th			919	3375	28.00	+ 5.75
6-48.92						
9+59.97			757	3537	29.00	+ 6.37
10+08.84			766	3528	30.00	+ 5.28
+ 57.76			633	3661	31.00	+ 5.61
11+06.68			438	3856	32.00	+ 6.56
11+55.6			342	3952	33.00	+ 6.52

Cont Page 58

1036 − 647 = 389 ÷ 9.81 = 0.55 + 3.40

3.54 − 6.82 = BM; 1036 − X

E.P. S.E. Cor 34th & Nat'l. = 6.82

414 + 1096 = X; 0.83 − 1012 = TP
847 + 1860 = X; 757 − 1103 = TP
934 + 2037 = X; 837 − 2000 = TP
1247 + 3247 = X; 074 − 3173 = TP
1121 + 4294 = X

Cont. from page 57

42.94

12+04.3 = MH 293.5' E 35th		2.71	40.23	34.00	+6.23	
+53.7		1.55	41.39	35.17	+6.22	
13+03.34 T.P. 6.79	48.85	0.88 / 0.88	42.06 / 42.06	36.34	+5.72	
+52.76		5.93	47.97	37.51	+5.41	
14+02.16		4.72	44.13	38.68	+5.25	
14+51.6		2.98	45.87	39.84	+6.03	
15+01 = DE West of 36th		1.02	47.83	41.00	+6.83	

Alley Bet. Alpha + Zeta Sts.

From a point on Canyon line bet. 36th + 37½ Sts. 2' West of Edendale to a D.End. 290' East {Profile & Plan - 6}

4+20.9 Page 59 = 0+00 (2-50)	to 12.86	19.99		7.13	1.75	+4.02
+50			12.84	7.15	2.62	+4.53
1+00 = Brk. (4-47.5)			7.33	12.68	3.50	+9.15
+47.5			2.38	17.61	6.62	+10.99
+95.0 T.P. 7.06	26.12		0.93	19.06	9.75	+9.31
2+42.5			5.56	20.56	12.87	+7.69
2+90 = DE West of 37½ St.			4.85	21.27	16.00	+5.27

H.I. from page 57 = 42.94 − 0.88 = 42.06 = T.P. + 6.79 = 48.85 = π − 11.84 = 37.61 + 37.69 = 40.03

8" line. CANYON LINE From a point on Alley 2' W of Edendale to Drop MH. in Blk. 4 Emerson Heights 135' East EL 36th St. {Profile 6/5}

3+60 Page 42		12.56				
= 0+00 (9-46.77)			12.65	-0.09	0.00	
+46.77			5.36	7.20	0.19	+7.01
+93.54			5.26	7.30	0.38	+6.92
1+40.31			5.50	7.06	0.57	+6.49
+87.08			9.92	2.64	0.77	+1.87
2+33.84			6.58	5.98	0.96	+5.02
2+80.60			5.80	6.76	1.15	+5.61
3+27.37			6.78	5.78	1.35	+4.43
+74.18			6.84	5.72	1.55	+4.17
4+20.9 (4-44.78)	= MH. Alley bet. Alpha & Z St. ∠ 5°07'		6.79	5.77	1.75	+4.02
4+65.67			6.04	6.52	1.94	+4.58
5+10.45			5.69	6.87	2.13	+4.74
+55.27	T.P. 8.95	16.08	5.43	7.13	2.37	+4.81
6+00 (3-52.67)	= Blk.		8.47	7.61	2.50	+5.11
6+52.67			7.63	8.45	3.00	+5.45
7+05.33			7.18	8.90	3.50	+5.40
7+58 (6-50.79)	= MH. Alley bet. Z St. + Boston ∠ 6°27'		6.46	9.62	4.00	+5.62
8+08.79			6.01	10.07	5.00	+5.07
+59.58			4.75	11.33	6.00	+5.33
9+10.38			4.26	11.82	7.00	+4.82
+61.17			3.57	12.51	8.00	+4.51
10+11.96			1.96	14.12	9.00	+5.12
10+62.76 (8-35.76)	= MH. Blk 4 115.97' W & Emerson St.	T.P. 29.71	0.47	15.61	10.00	+5.61
10+98.57			13.35	16.36	11.50	+4.86
11+34.28	= DMH 135' E EL 36th St.		4.74	24.97	13.00	+11.77 Main Line

BM 11.06 + 3.16 = 14.22 − 6.47 = 7.81 + 4.75 = 12.56

1.06 + 12.29 = 13.35

38th & Alpha 59

Line 135'E 36th + North of Boston Ave

29.71

24.56 NNL Boston = DE = 135'E & L 36th St.					
= 0+00	2.21	27.50	17.50	+10.00	
0+50 = ℄ DMH = 11734 28 page 59 5-33	4.74	24.97	17.00 / 13.00	+7.97	+11.97 Mainline
1+63	0.81	28.90	13.65	+15.35	
1+56	7.40	22.31	14.30	+8.01	
2+09	9.53	20.18	14.95	+5.23 v	
+62	8.22	21.49	15.60	+5.89 v	
3+15 = ℄ MH 41.45 25	4.45	25.26	16.25	+9.01 v	
3+61.25	3.48	26.03	16.81	+9.22 v	
4+07.5	3.95	25.76	17.37	+8.39 v	
+53.25	4.46	25.25	17.93	+7.32	
T.P. 12.26 41.72	0.75				
5+00 = DMH 135'E & L 36th St. 14.1 Emerson Hgts.	2.96	28.96	18.50 / 23.00	+10.46 Mainline	+5.96
+45	11.41	29.81	24.00	+5.81	
+90 = DE South Nat. 135'E & L 36th St. 37.39	7.95	33.27	25.00	+8.25	
53.91 E of 5+00 Above = DMH	14.11	23.28	Main 19.00 / Sprinkle 20.50	+4.28 Mainline	+2.78
+35	12.50	24.89	19.50	+5.39	
+70	11.20	26.19	20.00	+6.19	
1+00 41.20	6.74	34.43	30.50	+3.93	
1+53.2 = Existing Sewer	3.15	38.07	31.00	+7.07	
chk on old stub	3.20	34.02	31.00	+7.02 = +6.98	

28.96 + 8.43 = 37.39

12.74 + 1.37 = 14.11

℄ Gamma St. From a point 40' E.E.L. 40+11 to a O.E. 190'E of 42nd St. {See profile Plan - 3}

40'E EL. 40+11 ch.		95.52				
= 0+00			7.16	8836	7650	+11.86
0-48.33						
+48.33			8.22	8730	7625	+11.05
+96.66			8.47	8705	76.00	+11.05
1+45			7.40	8812	75.75	+10.37
1+93.37			6.61	8891	75.50	+13.41
2+41.65			7.68	8784	75.25	+12.59
2+90 = MH			10.27	8525	75.00	+10.25
0-50						
3+30			11.77	8375	7425	+9.50
+70			12.81	8271	7350	+9.21
TP	6.88	83.39	12.81	8271		
4+10			2.26	8133	72.75	+8.58
4+50 = B.K.			4.66	7893	72.00	+6.93
3-46.67						
4+96.67			8.06	7553	7167	+3.86
5+43.33			9.27	7432	71.34	+2.98
5+90 = MH ℄ 41st			9.22	7437	71.00	+3.37
7-48.57						
6+38.57			9.10	7449	70.82	+3.67
6+87.15			8.50	7509	70.64	+4.45
7+35.72			8.34	7525	70.46	+4.79
7+84.30			8.48	7511	70.28	+4.83
8+32.87			9.13	7446	70.09	+~~3.37~~ 4.37
8+81.45			8.64	7495	69.90	+5.05
9+30 = MH			8.58	7501	69.71	+5.30
7-45.71						
9+75.71			7.80	7579	69.54	+6.25
TP	6.74	82.53	7.80	75.79		
10+21.42			5.31	7722	69.37	+7.85
10+67.13			5.00	7753	69.20	+8.33
11+12.84			5.52	7701	69.03	+7.98

Cont. on Page 42

Page 41
MH 14+40 = Elev. stub = 63.50

12.88+
76.38
0.02
76.36 = T.P.
12.77+
89.13
0.61
88.52 = T.P.
2.80
95.32 = T.P.
12.81 -
82.71 = T.P.
0.68
83.39 = T.P.
7.83 -
75.79 = T.P.
6.74 +
82.53

Cont from Page 61

82.53

11+58.55		585	7668	68.85	+ 7.83
12+04.28		427	7826	68.67	+ 9.59
12+50 = DMH & 42nd St.		178	8081	68.50 } 7400	+ 12.31
12+97.5		195	8055	74.25	+ 6.30
13+45		237	8026	74.50	+ 5.76
+ 92.5		277	7976	74.75	+ 5.81
14+40 = DE 190' E & 42nd		280	7973	75.00	+ 4.73

Blks 498-499-500-Doughertys Sub.

(Profile 14 Sheet 3-4) Bet 42nd St. From a point on Alley bet Eta + Epsilon Sts to & Gamma + 42nd

Alley bet Eta + Epsilon = DMH 4.59 = 0+00 4-50

	49.20	12.50	3670	32.00	+ 4.70
0+50		1137	3783	32.50	+ 5.33
1+00		1075	3845	33.00	+ 5.45
+ 50.		1061	3859	33.50	+ 5.09
2+00 = MH & Epsilon St. 4-50.07		953	3965	34.00	+ 5.65
2+50.07		994	3976	34.50	+ 4.76
3+00.14		933	3987	35.00	+ 4.87
+ 50.21		860	4060	35.50	+ 5.10
4+00.30 = MH at Alley @ 34° ctr L 4-49.47		582	4338	36.00	+ 7.38
4+49.77		644	4276	37.00	+ 5.76
+ 99.15		432	4488	38.00	+ 6.89
5+48.57		438	4482	39.00	+ 5.87
5+98 = MH & DeHart St. 4-49.3 T.P. 1241	37.99	362 (362)	4558 (4558)	40.00	+ 5.58
6+47.3		942	4857	43.62	+ 4.95

Continued on Page 63

HI From Page 61 = 82.53 = π
For Chk. See lower right Page 63

+ 6.81

Elev. stub at 0+00 Page 63 = 45.58
3.67 +
47.20 = π
3.62 −
45.58 = T.P.
1.241
57.99 = π
For Chk. See Page 63

Cont. from Page 62

6+96.6 TP	1169	57.99	414 (0.34)	1385 (57.65)	47.25	+ 6.60		57.99 − 0.34 = 57.65
7+45.9		69.34	1071	5863	50.87	+ 7.76		1169 + 69.34 = π
7+95.8 = MH Δ 74°14' L. (6 − 47.65)			292	6642	54.50	+ 11.97		107 − 48.27 = TP
8+42.85			829	6105	54.92	+ 6.13		1301 − 81.28 = π
+90.50			1077	5857	55.34	+ 3.73		0.46
9+38.15			1127	5807	55.76	+ 2.31		80.87
9+85.8			1071	5863	56.17	+ 2.46	Page 62	
10+33.45			915	6019	56.59	+ 3.60	Elev. Sta 6 of 12+50 =	80.81
10+81.10 = MH ℄ 42nd + Alley Δ 90° R (11 − 47.42)			749	6185	57.00	+ 4.85		0.01 ✓
11+28.52 TP	1301	81.28	390 (1.07)	6544 (6827)	59.87	+ 5.37		
+75.54			1099	7079	62.75	+ 7.54		
12+39.36			464 (0.46)	7664	65.62	+ 11.02		
12+70.8 = MH ℄ 42nd + Gamma St = 12+50 Page 66				8082	68.50 | 74.00	+ 17.32 ✓0.01	+ 6.82 ✓0.01	

℄ DELTA St. {Profile 14 Plan 3}

From a point 3' West Cofelimits W for 930'

3+98 - Page 63 = 0+00 = MH (3 − 46.67)		57.55	1197	4558	40.00	+ 5.58	HI From Page 62 =	82.33 − 1.96 = 80.37 = TP
0+46.67			820	4935	45.67	+ 3.68		0.43 + 79.19
+93.34 TP	12.17	69.49	023 (0.23)	5732 (5732)	51.34	+ 5.95		1323 − 56.96 = TP
1+40 = Brk. (4 − 50)			647	6302	57.00	+ 6.02		0.59 ✓ 57.55 = π
1+90			185	6764	57.69	+ 9.95		0.23 − 57.32 = TP
2+40 TP	84'	77.21	069 (0.69)	6880 (6880)	58.39	+ 10.41		12.17 + 69.49 = π
+90			751	6970	59.08	+ 10.62		0.69 − 68.80 = TP
3+40 = MH ℄ 42nd (6 − 50)			670	7051	59.78	+ 10.73		84' + 77.21 = π
3+90			611	7110	60.47	+ 10.63		
4+40			665	7056	61.17	+ 9.39		

Cont. on Page 64

See Page 64 for ch.

Cont. from Page 63

℄ DELTA St.

4+90		77.21	6.10	71.11	61.87	+9.24
5+40			5.73	71.48	62.56	+8.92
5+90			7.60	69.61	63.25	+6.36
6+40 = MH 6-48 83			7.31	69.90	63.96	+5.94
6+88.33			5.84	71.37	64.63	+6.74
7+36.66			6.37	70.84	65.30	+5.54
+84.29			7.16	70.05	65.98	+4.07
8+33.33			7.03	70.18	66.65	+3.53
+81.66			5.01	72.20	67.32	+4.88
9+30 = DE East 41' on Delta			4.39	74.12	68.00	+6.12

E.F. From Page 63 = 77.21 = X
2.07 −
75.14 = TF
0.60 +
75.74
12.20
63.54
Elev stub at Sta 1+20 Page 41 = 63.50
0.04 ✓

EPSILON St.

Profile 14 Sheet 3 of 4

From a Point near City Limits - West

Elev stub at 0+00 Page 63 = 45.58
6.58 +
52.16

75' East Sta 2+00 Page 62

= 0+00 = DE		52.16	2.65	49.51	43.00	+6.51
+25 = Brk.			6.40	45.76	37.00	+8.76
+75 = MH ℄ Epsilon = 2+00 Page 62			12.51	39.65	34.00	+5.65
1+25 = Brk.			11.18	40.98	36.50	+4.48
1+85 = DE			1.74	50.42	43.50	+6.92

42nd St
From ℄ Nordica to ℄ EPSILON {Profile 14 Sheet 4}

℄ Nordica + 42nd	32.76				
= 0+00		12.46	20.30	15.74	+4.56
3=51.63					
+51.63		10.37	22.39	16.16	+6.23
403.86		10.53	22.23	16.58	+5.65
1+54.80 = MH ℄ Alley		10.30	22.46	17.00	+5.46
3-56					
2+09.2		9.41	23.35	18.67	+4.68
+64.9		7.80	24.96	20.34	+4.62
3+19.9 = MH ℄ Eta St.		4.73	28.03	22.00	+6.03
4-47.35					
3+67.45		4.41	28.35	24.12	+4.23
4+15.0 T.P.	44.78	12.85	31.86	26.25	+5.61
+62.55		9.24	35.47	28.37	+7.10
5+10.10 = MH ℄ Alley		5.43	39.28	30.50	+8.78
4-47.53					
5+57.63		1.36	43.35	32.62	+10.72
6+05.15		0.10	44.61	34.75	+9.86
6+52.68		1.42	43.29	36.87	+6.42
7+00.20 = MH ℄ EPSILON + 42nd St.		0.56	44.15	39.00	+5.15

41.15
0.56
44.71
1.85
37.86
0.90
32.76

Alley bet Eta + EPSILON St. {Profile 14 Sheet 4}
From ℄ 42nd East 430'

℄ 42nd bet Eta + EPSILON					
= 0+00 = MH.	48.73	9.45	39.28	30.50	+8.78
6-44.56					
0+44.56		11.53	37.40	30.75	+6.65
+89.12		2.44	46.29	31.00	+15.29
T.P. 5.55	53.44	0.84	47.89		
1+33.68		2.86	50.58	31.25	+19.33
1+78.24		7.90	45.54	31.50	+14.04
2.65	49.47	11.67	41.87		
2+22.80		9.75	39.72	31.75	+7.97
2+67.40 = MH.		12.79	36.68	32.00	+4.68
1-52.6					
3+20 = Brk.		8.23	41.24	33.00	+4.24

Cont. on Page 66

Elev Stub at Sta 0+00 Page 62 = 32.76
12.09 +
48.73 = π
0.84
47.89 = TP
5.55 +
53.44 = π
11.67
41.87 = TP
7.65 +
49.47

Cont'd From PAGE 63

Alley bet Eta + Epsilon
From ℄ 42nd East 490'

3+50 T.P. 11.09	49.47 / 59.18	1.38 / 1.38	48.09 / 48.09	43.00	+5.09	49.47 = T 1.38 48.09 = T.P. 11.09+ 59.18 = T
3+80 = Brk.		4.63	54.35	49.00	+5.35	
4+10		2.67	56.51	49.25	+7.26	
4+40 = DE		2.49	56.69	49.50	+7.19	+.09 Sta. 1+85 Page 64 = 8.79 / 50.39 / 50.42 / +0.03

EPSILON St.

From ℄ 42nd St. 140' East. + West 1250' (Profile 15 sheet 4)

℄ 42nd + EPSILON 5.61	56.03		50.42 D.E. P.64	43.50	+ 6.92	
= 0+00 = MH. Sta. 7+00 Page 65		11.88	44.15	39.00	+5.15	
+30		12.80	43.23	39.50	+3.73	
+60 = Brk.		10.31	45.72	40.00	+5.72	
1+00		7.00	49.00	43.00	+6.00	
1+40 = DE. East of 42nd		3.89	52.14	46.00	+6.14	

EPSILON St West of 42nd

0+00 = MH. Sta. 7+00 Page 65 (5.42 / 2-40 / 56.03)		11.88	44.15	39.00	+5.15	
+40		7.67	48.36	42.50	+5.86	
+80 = Brk. (5-90 T.P. 8.51)	63.91	2.66 / 0.13	53.37 / 55.90	46.00	+7.37	
1+30		5.17	58.74	46.23	+12.51	
1+80		3.25	60.66	46.47	+14.19	
2+30		2.59	61.32	46.70	+14.62	
2+50		2.76	61.15	46.94	+14.21	
3+30 = MH. (.7 = 47.14)		4.29	59.62	47.17	+12.45	
3+77.14		4.78	57.13	47.39	+9.74	
4+24.38		8.15	55.76	47.61	+8.15	
+71.42		10.13	53.78	47.84	+5.94	
5+18.57		12.53	51.38	48.06	+3.32	

Cont'd on PAGE 67

Cont. From Page 66

EPSILON St.

TP	8.30	63.91 59.13	13.08	50.83		
5+65			11.07	48.86	48.28	-0.22
6+12.85			8.84	50.29	48.51	+1.78
6+60 = MH & 41st St. 6-50			3.55	55.58	48.73	+6.85
7+10			3.66	55.47	48.96	+6.51
+60			2.98	56.15	49.20	+6.75
8+10			4.00	55.13	49.43	+5.70
+60			4.13	55.06	49.67	+5.33
9+10			4.48	54.65	49.91	+4.74
9+60 = MH. 6-48.33			2.75	56.38	50.14	+6.24
10+08.33			2.26	56.87	50.37	+6.50
+36.66			2.51	56.62	50.60	+6.02
11+04.99	T.P.	0.70	57.57	2.26	56.87	50.82	+6.05
11+53.32				0.37	57.20	51.05	+6.15
12+01.65				1.52	56.05	51.27	+4.78
12+50 = DE 40' E El 40th				2.46	55.11	51.50	+3.61
				7.30	50.27	Top of RR Bridge Bolt head	

Maxine View Ave E & W From M.H. & 40th St

00 = MH & 40th St						36.50
+43.5 W						
+97.0						
1+39.5						
1+74.0 & N+S Alley Bisects (44.4)						39.00
2+18.4						
2+62.8						
3+07.2						
3+51.5 D.E						40.00

Marine View E. of 40th

00 M.H. & 40th	36.50
+ 47.5	
+ 95.6	
1+43.5 M.H. & Alley Blk 16	45.00
38.83	
1+82 33	
2+21. 17	
2+60 Brk	55.00
43.4	
3+03. 4	
3+46 8	
3+90 7	
4+33 5 MH & Alley Blk	
40 17 N.H.	62.75
4+73 5 Brk	65.00
50	
5+23 5	
5+73 5	
6+23 5	
6+73 5 DE	66.00

Alley Blk 16 N.H

M.H. & Marine	
00 View Ave.	45.00
+40	45.20
+80	45.40
1+20	45.60
1+40	45.80
2+00	46.00
2+40	46.20

℄ ETTA from ℄ 42nd W. 190'

		10.87	38.90		28.03 (Page 65)	
00=MH ℄ 42nd St					28.03	22.00	+ 6.03
+47.5				11.85	27.05	23.88	+ 3.17
+95.				6.78	32.12	25.75	+ 6.37
1+42.5				1.84	37.02	27.63	+ 9.39
1+90 D.E.				4.00	34.90	29.50	+ 5.40

Alley Blk 7 N. H

					Page 65		
00=MH ℄ 42nd St		12.44	34.90		22.46	17.00	+ 5.46
+40				12.26	22.64	17.67	+ 4.97 ✓
+80				11.43	23.47	18.33	+ 5.14 ✓
1+20 Brk				9.87	25.03	19.00	+ 6.03 ✓
1+60				7.63	27.27	21.75	+ 5.52 ✓
2+00				4.87	30.03	24.50	+ 5.53 ✓
2+40	T.P.	11.56	44.65	1.81	33.09	27.75	+ 5.84 ✓
2+80 MH				9.50	35.15	30.00	+ 5.15 ✓
3+24.2				6.31	38.34	31.42	+ 6.92 ✓
3+68				4.86	39.79	32.84	+ 7.95 ✓
4+12.6				3.95	40.70	34.26	+ 6.44 ✓
4+56.40 ⊐ △ 17°-48' L				3.81	40.84	35.68	+ 5.16 ✓
4+96 ⊐				3.32	41.33	37.00	+ 4.33 ✓

℄ Nordica ℄ 42nd E. to ℄ Alley Blk 11

00=M.H ℄ 42nd St		9.81	30.17		20.30 Page 64	15.74	+ 4.56
+42.5				7.23	22.94	15.93	+ 7.01
+85.				7.42	22.75	16.12	+ 6.63
1+27.5				4.80	23.37	16.31	+ 7.06
M.H Alley Blk 11 1+70				4.72	25.45	16.50	+ 8.75

Con Page 69

1+70 M.H. & Nordica 50	30.17	4.72	25.45	16.50	+8.95
2+20		6.54	23.63	16.75	+6.88
2+70		9.84	20.33	17.00	+3.33
3+20		10.12	20.05	17.25	+2.80
3+70 Brk 35		7.97	22.20	17.50	+4.70
4+05		6.00	24.17	18.00	+6.17
4+40 M.H. & E+W Alley 40		6.53	23.64	18.50	+5.14
4+80		6.05	24.12	19.67	+4.45
5+20		5.63	24.54	20.84	+3.70
5+60 DE		2.91	27.26	22.00	+5.26

E+W Alley Brk 11 N.H. #2

00 M.H. 4+40 above CTP 6.13	30.36	6.57	23.69	18.50	+5.14
+49.8		6.12	24.24	18.71	+5.53
+99.6		6.24	24.12	18.92	+5.20
1+49.4 ✓		6.06	24.30	19.13	+5.17
1+99.2 ✓		5.70	24.66	19.35	+5.31
2+49		5.32	25.04	19.56	+5.48
2+98.5		5.08	25.28	19.78	+5.50
3+48 # MH & N-S Alley.		4.81	25.55	20.00	+5.55
3+98 5				19.84	
4+48 # M.H. Alley E+W S				20.00	

100 Shorter than plan

N & S. Alley E. End Blk 11 N.H 2

30.36 Pc

00=D.E. 110's of N.H. & E+W Alley			3.53	26.89	21.00	+5.89
+55			4.30	26.04	20.80	+5.56
1+10=M.H. & E+W Alley 30			4.81	25.55	20.00	+5.55
1+40			4.54	25.82	20.37	+5.45
2+10			5.28	25.08	20.75	+4.33
2+60			4.05	26.31	21.12	+5.19
3+10 DE in Nordica St			00	30.36	21.50	+8.86

42nd from M.H. & Nordica S. Thence Thru Blk 10, N.H. 2

00=M.H. & 42nd						
+Nordica	6.81	27.11		20.30 page 65	15.74	+4.56
+40			4.50	22.61	15.94	+6.67
+80			4.61	22.50	16.14	+6.36
1+20			4.51	22.60	16.34	+6.26
1+40 MH 45.25			4.30	22.81	16.54	+6.27
2+05 25			4.65	22.46	16.78	+5.68
2+50 5			5.17	22.00	17.02	+4.98
2+95 75			5.09	22.02	17.26	+4.76
3+41 M.H. & Collonwood 34.45			5.39	21.72	17.50	+4.22
3+75 55			4.36	22.75	18.25	+4.50
4+10 Brk T.P. 35	8.73	34.39	1.45	25.66	19.00	+6.66
4+45			4.93	29.46	23.00	+2.46
4+80 MH			2.13	32.26	27.00	+5.26

	Cont. 71	℄ Collonwood W To DE E. of 41st 34.39				
4+80 = M.H. (47.8)			2.23	32.26	27.00	+ 5.26
5+27			0.35	34.04	27.25	+ 6.79
5+75			0.68	33.71	27.50	+ 6.21
6+23			1.05	33.34	27.75	+ 5.59
6+71			1.01	33.38	28.00	+ 5.38
7+19			0.33	34.06	28.25	+ 5.81
7+66 DE E of 41st.			0.43	33.96	28.50	+ 5.46
		S. on Collonwood 34.39				
00 = M.H						
2+41½ Page 71			12.67	21.72	17.50	+ 4.22
+45			12.23	22.16	17.82	+ 4.34
+90			12.10	22.29	18.15	+ 4.14
1+35			11.27	23.12	18.47 33	+ 4.65
1+80 = BrK (36.42)			8.61	25.78	18.80	+ 6.98
2+16			4.94	29.45	22.40	+ 7.05
	T.P. 12.87	46.65	0.61	33.78		
2+52 M.H (47.14)			11.65	35.00	26.00	+ 9.00
	T.P. 8.94	50.17	5.42	41.23		
3+20. DE N. of Division			2.87	47.30	36.00	+ 11.30

8" Line ℄ Cottonwood 39th St East

Continued from Page 27

13.22

12+37.5	MH ℄ Cottonwood			5.00	8.22	4.44	+3.78
40.7							
12+78.5				4.75	8.47	4.54	+3.93
13+19.2				4.46	8.76	4.65	+4.11
13+59.2				4.13	9.09	4.75	+4.34
14+00.7	MH ℄ Osborn			4.20	9.02	4.85	+4.17
40.7							
14+41.4				3.83	9.39	4.95	+4.44
14+82.1				3.54	9.68	5.05	+4.63
15+22.2	T.P. 5.86		16.00	3.08	10.14	5.15	+4.99
15+63.4	MH ℄ Alley			4.95	11.05	5.25	+5.80
41.2							
16+04.8				4.86	11.14	5.56	+5.58
16+46.6				4.76	11.24	5.87	+5.37
16+87.2				4.40	11.60	6.18	+5.42
17+28.4				4.06	11.94	6.49	+5.45
17+69.6				3.71	12.29	6.80	+5.49
18+10.8				3.22	12.78	7.11	+5.67
18+52.6				5.36	10.64	7.42	+3.22
	T.P. on Sta. 18+52 7.76		18.40.	5.36	10.64		
18+93.2	MH ℄ Alley △ 35°08'			5.77	12.63	7.72	+4.91
					1.0 CY		
19+39.26				5.65	12.75	8.06	+4.69
19+85.33				4.85	13.55	8.40	+5.15
20+31.40	X ℄ Cottonwood 36° 00'			4.71	13.69	8.74	+4.95
20+77.5	MH ℄ 40th △ 57° 14'L			3.79	14.61	9.09	+5.52
.45							
21+22.5				4.03	14.37	9.29	+5.08
21+67.5				3.76	14.64	9.49	+5.15
	T.P. 5.81		20.45	3.76	14.64		
22+12.5				5.74	14.74	9.69	+5.05
22+57.5				5.47	14.98	9.89	+5.09
23+02.5				5.22	15.23	10.09	+5.14

Page 27

2045

23+41.6 MH. & HO 25 + Nordica		4.08	1637	10.29	+ 6.08
T.P. Nails 17 Blue " 573 " 21.68		4.50	1595		
6-46.67 23+94.97		5.70	15.98	10.49	+ 5.49
24+40.94		5.61	1607	10.69	+ 5.38
+87.61		5.53	1615	11.91	+ 4.74
25+34.28		5.40	1628	11.11	+ 5.17
+80.95		5.11	1657	11.32	+ 5.25
26+27.6 = MH. 6-48.03		5.08	1660	11.53	+ 5.07
+75.63		4.99	1669	11.74	+ 4.95
27+23.66		4.10	1758	11.95	+ 5.63
+71.89		4.23	1745	12.16	+ 5.29
28+19.72		4.13	1755	12.38	+ 5.17
+67.75		3.80	1788	12.60	+ 5.28
29+15.8 = MH & 41st + Nordica 7-47.14 T.P. 7.37 25.40		3.48	1820	12.81	+ 5.39
29+62.94		3.65 6.92	1803 1848	13.03	+ 5.45
30+10.88		6.43	1897	13.25	+ 5.72
30+57.22		6.33	1907	13.48	+ 5.59
31+04.36		6.03	1937	13.70	+ 5.67
+51.5		5.56	1984	13.92	+ 5.92
31+98.64		5.03	2037	14.15	+ 6.22
32+45.8 = & M.H. 7-47.26		4.83	2057	14.37	+ 6.20
32+93.06		5.06	2034	14.57	+ 5.77
33+40.32		4.50	2090	14.77	+ 6.13
33+87.58		3.91	2149	14.97	+ 6.52
34+34.84		3.73	2165	15.16	+ 6.49
34+80.10		3.67	2173	15.35	+ 6.38
35+29.36		2.74	2266	15.55	+ 7.11
35+76.6 = & M.H. 42nd + Nordica		9.65	15.75	15.75	= Von Flow Line

Alley Bet. Earle + 40th
From E Cottonwood to Birch St. Sheet 4 Profile 13

18+93.2 Page 73	11.15	23.78		12.63 Sec Sta. 18+93.2 Page 73	7.72	
= 0+00 = E Cottonwood + Alley MH.						
6-40						
+40			1340	1038	8.02	+2.36
+80			979	1399	8.32	+5.67
1+20			1037	1341	8.62	+4.79
+60			1033	1345	8.92	+4.53
2+00			1005	1378	9.21	+4.57
2+40 = MH.			951	1427	9.50	+4.77
+80			822	1556	11.00	+4.56
3+20			607	1771	12.50	+5.21
+60 = Brk.			332	2046	14.00	+6.46
TP 341	26.12		1.03	22.75		
4+00 = D.E. Approx 40'S.Sh. Birch 104			25.12		18.00	+7.12

Alley Bet. Osborne + Earle St.
From E Cottonwood to Birch St

13+63.5 Page 73	12.13		508	1105	5.25	+5.80
= 0+00 = MH. E Cottonwood + Alley						
+40			554	1054	5.71	+4.83
+80			521	1092	6.17	+4.75
1+20			496	1117	6.63	+4.54
+60			488	1125	7.09	+4.16
2+00			415	1198	7.55	+4.43
+40 = MH.			255	1358	8.00	+5.58
TP 12.81	26.75		0.19	1594		
+80			1130	1745	13.00	+4.45
3+20			568	2307	18.00	+5.07
TP 3.22	31.41		0.36	28.19		
3+60			2.54	28.87	23.00	+5.67
TP 3.41	33.62		1.20	30.21		
4+00			1.46	31.96	28.00	+3.96

Page 73
MH. Stub. at Sta. 18+93.2 = 18.63
350+
1413=TP
508
1105
1613
019-
1594 = TP
12.81+
26.75
054-
2819 = TP
3224
31.41
120-
3021 = TP
341+
3362
1773-
2189 = TP
Page 73
Sta. 15+43.6
Stub MH Stub = 1105+

Birch St. From E Alley west of Osborne St (Profile 13) (Sheet 3)

East 390'

38.33

M.H.E Alley west of Osborne = 0+00		7.30	31.03	25.00	+6.03
3-46.67 0+46.67		7.74	30.59	25.33	+5.26
+93.33		7.82	30.51	25.67	+4.84
1+40 = Brk.		7.30	31.03	26.00	+5.03
+90		4.33	34.00	27.70	+6.30
2+40		2.18	36.15	29.40	+6.75
+90		0.97	37.36	31.10	+6.26
T.P. 4.34	41.70	0.97	37.36		
3+40		3.43	38.27	32.80	+5.47
3+90 = D.E.		1.77	37.93	34.50	+5.43

Bottom of Elev. DE 4+00 Page 73 = 31.96

chk 0.01

38.33
0.97
37.36 = H.I.
4.34 +
41.70 = H
9.73 −
31.97

Elev. Stub Sta 156-5 Page 73 = 11.05

2.87 +
13.92 = H
0.77 −
13.15 = T.P.
12.73 +
25.88 = H
6.41 −
25.47 = T.P.
0.86 −
38.33

This H.I. transfered to top of page

Alley West of Osborne St. (Profile 13 Sheet 3)

From E Cottonwood to E Birch St.

M.H.E Cottonwood = Sta. 12.39 Page 73 = 0+00	13.92	5.74	8.18	4.44	+3.74 (3.78 Page 73) (0.04 Probably disturbed)
+50		5.29	8.63	4.95	+3.68
1+00		4.75	9.17	5.47	+3.70
+50		4.27	9.65	5.98	+3.67
2+00 = Brk.		2.97	10.95	6.50	+4.45
2-31 +31		1.68	12.24	7.92	+2.32
T.P. 1.73	25.88	0.77	13.15		
2+62 = M.H.E alley's		11.40	14.48	9.35	+5.13
3-46 3+08		9.26	16.62	11.57	+5.05
3+54		7.71	18.17	13.78	+4.39
4+00 = Brk.		4.41	21.47	16.00	+5.47
2-40 4+40		0.41	25.47	20.50	+4.97
T.P. 2.86	38.33	0.41	25.47		
4+80 = M.H.E Birch = 0+00 at top of Page		7.30	31.03	25.00	+6.03

Alley Bet. Birch & Cottonwood sts (Profile 13 Sheet 3)

From Alley west of Osborne St. N W E X 100'

(M.H.E alleys opposite this column = 0+00	25.88	11.40	14.48	9.35	+5.13
+30		11.67	14.21	9.67	+4.54
+60 = Brk.		10.01	15.87	10.00	+5.87
1+00 = DE		18.32	24.05	17.00	+7.05

Cottonwood St. From ℄ 40th St. {Profile 12 Sheet 3}
Easterly 550'

Sta. 2e+77.5 Page 73 = 0+00	20.09	549.	1460	9.09	+ 5.51 chk. 0.01
6-45					
+45		546	1463	9.30	+ 5.33
+90		516	1493	9.51	+ 5.42
1+35		501	1508	9.73	+ 5.35
+80		459	1550	9.95	+ 5.55
2+25		426	1583	10.17	+ 5.66
+70 = MH		419	1590	10.38	+ 5.52
3-43.33					
3+13.33		434	1575	10.59	+ 5.16
3+56.66		433	1576	10.80	+ 4.96
4+00 = Brk		392	1617	11.00	+ 5.17
+50		278	1731	12.77	+ 4.54
5+00 TP 560	24.92	077	1932	14.54	+ 4.78
		077	19.32		
+50 = OE. West of 41st St.		360	2132	16.30	+ 5.02

41st St. From ℄ Nordica to ℄ 7th St.

29+15.8 Page 72 = 0+00	30.89			12.81	
+40		1179	1910	12.98	+ 0.17
+80		1160	1929	13.15	+ 6.14
1+20		1383	1706	13.32	+ 3.74
1+60 = Brk.		1203	1886	13.50	+ 5.36
2+00		1036	2053	14.87	+ 5.66
+40		699	2390	16.25	+ 7.65
+80 TP 793	38.52	030	30.59	17.62	+ 13.72
		718	31.34		
3+20 = OMH ℄ 43rd St.		134	3718	19.00 {27.00}	+ 18.18

O.M. Nail in Pole 40th + Nordica Elev = 15.95
4.14
20.09 = A
0.77
19.32 = TP
5.60
24.92 = A
6.72
18.20
Sta. 29+15.8 Elev St. b. Page 74 = 18.20
0.00

Sta. 29+15.8 MH ℄ 41st Nordica Elev = 18.20
12.89 +
30.89 = A
0.30
30.59 = TP
7.93 +
38.52 = A

+ 10.18

ETA - St.

From ℄ 41st East 390' + West 390'

			Rod. Ground		I. G.	Cut
3+20 Page 77 = ℄ 41st + Eta =		38.52 = HI. from Page 77				
= 0+00 = DMH S-48.75			6.76	31.76	19.00	
+ 48.75			10.86	27.66	19.25	+ 12.51
+ 97.5 TP	5.78	31.39	12.71	25.81	19.50	+ 8.16
1+46.25			6.36	25.23	19.75	+ 5.48
+ 95.00			6.67	24.92	20.00	+ 4.92
2+43.75			7.92	23.67	20.25	+ 3.42
2+92.50			8.59	23.00	20.50	+ 2.50
3+41.25			7.97	23.62	20.75	+ 2.87
3+90 = D.E. East ℄ 41st st.			5.34	26.25	21.00	+ 5.25

Eta. St. from ℄ 41st 390' West.

℄ 41st + Eta = 0+00 = DMH S-50		24.41			19.00 / 22.00	
+ 50			4.37	40.04	28.25	+ 11.79
1+00			9.94	34.47	29.50	+ 4.97
1+50			12.61	31.80	30.75	+ 1.05
2+00 = Brk. 4-47.5			4.11	40.30	32.00	+ 8.30
+ 47.5			0.35	44.06	34.00	+ 10.06
+ 95.00 TP	5.13	39.19	0.35	44.06		
			4.76	41.43	36.00	+ 8.43
3+42.5			3.42	45.77	38.00	+ 7.77
3+90 = D.E. W ℄ 41st st.			1.75	47.44	40.00	+ 7.44

3.65 2 = T
1.71
25.81 = TP
5.78 +
31.59 = T
13.39

Sta. 0+00 Stg. b. M.E. 41st Nicollet = 18.20

Sta. 3+20 Page 77
Elev. Stub DMH ℄ 41st Eta. = 37.16
7.23
44.41 = T
0.35
44.06 = TP
5.13
49.19 = T
1.20
Bk. 00 above Stub 37.18

℄ Osborn St

℄ Cottonwood South to Alley S. of Marin View

13.04

00 MH ℄ Cottonwood ℄ Osborn	13.04	22.06		9.02	4.85	+4.17
+39			12.43	9.63	5.04	+4.59
+78			12.40	9.66	5.23	+4.43
1+17			12.40	9.66	5.41	+4.25
1+37 MH ℄ Alley (40)			13.08	8.98	5.60	+3.38
1+97			12.12	9.94	5.80	+4.14
2+37			10.12	11.94	6.00	+5.94
					6.20	7.78
2+79 DMH 45.6			8.08	13.98	10.00	+3.98
3+27.6	T.P.	12.67	34.47	1.73 / 0.06	20.33 / 22.00	11.60 +8.73
3+68				8.72	25.95	13.20 +12.75
4+13.8				5.62	29.65	14.80 +14.25
4+59.4				4.41	30.26	16.40 +13.86
5+05 MH S of Marin View Ave 40				5.00	29.67	18.00 +11.67
5+45 BrK 56.8				4.27	30.40	19.00 / 3.5 +11.40
6+01.8				3.62	31.05	22.50 +8.55
6+58.6 MH ℄ N+S Alley 51.7				2.77	31.90	26.00 +5.90
7+10.3				2.00	32.67	27.50 +5.17
7+62	T.P.	10.15	44.68	0.14	34.53	29.00 +5.53
8+13.2				7.73	36.95	30.50 +6.45
8+65.4				6.13	38.55	32.00 +6.55
9+17.1				5.34	39.34	33.50 +5.84
9+68.8				4.63	40.05	35.00 +5.05
10+20.4 MH ΔL 37.6				3.48	41.20	36.50 +4.70
10+58.0 MH. 57.5				4.00	40.68	37.00 +3.68
11+15.5				1.30	43.38	38.00 +5.38
11+73 D.E				0.97	43.71	39.00 +4.71

Page 73

34.47 Page 79.

00=6+58 M.H Page 79	2.77	31.90	26.00
+45	3.75	30.92	26.25
+90=DE	5.07	29.60	24.50

Alley But Cottonwood Marine View

Osborn East

00=1+57 =M.H. Page 79	5.60
+50	5.90
1+00	6.20
+50	6.50
2+00	6.80
+50	7.10
3+00	7.40
+50	7.70
4+00=M.H. 52 55	8.00
4+52 55	15.25
5+05 1 MH 57 45 A L	22.50
5+62 55	31.75
6+20 00 B.K 30	41.00
6+50 D.E	41.50

+5.90

+4.67

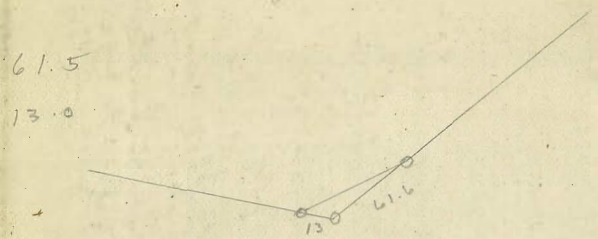
+3.10

IMPROVED TABLES AND INFORMATION

540

529

8.66 9.26 9.00



750
690
60

2666
2666
5333
80.00

9.27
9.81

53
144
197
203

641
340
981

3143.5
47.8
47.5
95.6
47.9
143.5

1208
132
1340

3.46

9.57
.06
.951
1820.