

GRADES

140

D E P O

FIELD BOOK

No. 385

145
31 4/176
176

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

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DIETERICH-POST CO.

75 NEW MONTGOMERY ST.
SAN FRANCISCO, CALIF.

AGENTS FOR

"BERGER" TRANSITS and LEVELS

"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS

"CHICAGO" STEEL TAPES, etc.

MICROFILMED

APR 8 1965

cbR = 3570 LANTANA Dr. Grading 1/2 mt Moore
 S.L. STA.

ST.	✓ CB	N CB
- 6905 = P. Cor. NL	341.6	340.68 = curb NL
00 = P.C. S.L. LANTANA	341.80	340.80
0 + 1595	341.90	340.91
0 + 9190	342.0	341.0
1 + 3785	342.10	341.10
1 + 83.80 = BREAK	342.20	341.20
2 + 2325	342.05	341.05
2 + 627 = PC	341.90	340.90
3 1 = 22' 00"	341.84	340.83
3 2 = 18' 00"	341.78	340.75
3 3 = 12' 00"	341.73	340.68
3 4 = 6' 00"	341.67	340.61
3 5 = 0' 00"	341.61	340.54
3 6 = 6' 00"	341.56	340.47
3 7 = 12' 00"	341.50	340.40
3 8 = 18' 00"	341.43	340.35
3 9 = 24' 00"	341.37	340.30
3 10 = 30' 00"	341.30	340.25
3 11 = 36' 00"	341.23	340.20
3 12 = 42' 00"	341.16	340.15
3 13 = 48' 00"	341.09	340.10
3 14 = 54' 00"	341.02	340.05
3 15 = 60' 00"	340.95	340.00
3 16 = 66' 00"	340.88	339.95
3 17 = 72' 00"	340.81	339.90
3 18 = 78' 00"	340.74	339.85
3 19 = 84' 00"	340.67	339.80
3 20 = 90' 00"	340.60	339.75
3 21 = 96' 00"	340.53	339.70
3 22 = 102' 00"	340.46	339.65
3 23 = 108' 00"	340.39	339.60
3 24 = 114' 00"	340.32	339.55
3 25 = 120' 00"	340.25	339.50
3 26 = 126' 00"	340.18	339.45
3 27 = 132' 00"	340.11	339.40
3 28 = 138' 00"	340.04	339.35
3 29 = 144' 00"	340.00	339.30
3 30 = 150' 00"	339.95	339.25
3 31 = 156' 00"	339.90	339.20
3 32 = 162' 00"	339.85	339.15
3 33 = 168' 00"	339.80	339.10
3 34 = 174' 00"	339.75	339.05
3 35 = 180' 00"	339.70	339.00
3 36 = 186' 00"	339.65	338.95
3 37 = 192' 00"	339.60	338.90
3 38 = 198' 00"	339.55	338.85
3 39 = 204' 00"	339.50	338.80
3 40 = 210' 00"	339.45	338.75
3 41 = 216' 00"	339.40	338.70
3 42 = 222' 00"	339.35	338.65
3 43 = 228' 00"	339.30	338.60
3 44 = 234' 00"	339.25	338.55
3 45 = 240' 00"	339.20	338.50
3 46 = 246' 00"	339.15	338.45
3 47 = 252' 00"	339.10	338.40
3 48 = 258' 00"	339.05	338.35
3 49 = 264' 00"	339.00	338.30
3 50 = 270' 00"	338.95	338.25
3 51 = 276' 00"	338.90	338.20
3 52 = 282' 00"	338.85	338.15
3 53 = 288' 00"	338.80	338.10
3 54 = 294' 00"	338.75	338.05
3 55 = 300' 00"	338.70	338.00
3 56 = 306' 00"	338.65	337.95
3 57 = 312' 00"	338.60	337.90
3 58 = 318' 00"	338.55	337.85
3 59 = 324' 00"	338.50	337.80
3 60 = 330' 00"	338.45	337.75
3 61 = 336' 00"	338.40	337.70
3 62 = 342' 00"	338.35	337.65
3 63 = 348' 00"	338.30	337.60
3 64 = 354' 00"	338.25	337.55
3 65 = 360' 00"	338.20	337.50
3 66 = 366' 00"	338.15	337.45
3 67 = 372' 00"	338.10	337.40
3 68 = 378' 00"	338.05	337.35
3 69 = 384' 00"	338.00	337.30
3 70 = 390' 00"	337.95	337.25
3 71 = 396' 00"	337.90	337.20
3 72 = 402' 00"	337.85	337.15
3 73 = 408' 00"	337.80	337.10
3 74 = 414' 00"	337.75	337.05
3 75 = 420' 00"	337.70	337.00
3 76 = 426' 00"	337.65	336.95
3 77 = 432' 00"	337.60	336.90
3 78 = 438' 00"	337.55	336.85
3 79 = 444' 00"	337.50	336.80
3 80 = 450' 00"	337.45	336.75
3 81 = 456' 00"	337.40	336.70
3 82 = 462' 00"	337.35	336.65
3 83 = 468' 00"	337.30	336.60
3 84 = 474' 00"	337.25	336.55
3 85 = 480' 00"	337.20	336.50
3 86 = 486' 00"	337.15	336.45
3 87 = 492' 00"	337.10	336.40
3 88 = 498' 00"	337.05	336.35
3 89 = 504' 00"	337.00	336.30
3 90 = 510' 00"	336.95	336.25
3 91 = 516' 00"	336.90	336.20
3 92 = 522' 00"	336.85	336.15
3 93 = 528' 00"	336.80	336.10
3 94 = 534' 00"	336.75	336.05
3 95 = 540' 00"	336.70	336.00
3 96 = 546' 00"	336.65	335.95
3 97 = 552' 00"	336.60	335.90
3 98 = 558' 00"	336.55	335.85
3 99 = 564' 00"	336.50	335.80
3 100 = 570' 00"	336.45	335.75
3 101 = 576' 00"	336.40	335.70
3 102 = 582' 00"	336.35	335.65
3 103 = 588' 00"	336.30	335.60
3 104 = 594' 00"	336.25	335.55
3 105 = 600' 00"	336.20	335.50
3 106 = 606' 00"	336.15	335.45
3 107 = 612' 00"	336.10	335.40
3 108 = 618' 00"	336.05	335.35
3 109 = 624' 00"	336.00	335.30
3 110 = 630' 00"	335.95	335.25
3 111 = 636' 00"	335.90	335.20
3 112 = 642' 00"	335.85	335.15
3 113 = 648' 00"	335.80	335.10
3 114 = 654' 00"	335.75	335.05
3 115 = 660' 00"	335.70	335.00
3 116 = 666' 00"	335.65	334.95
3 117 = 672' 00"	335.60	334.90
3 118 = 678' 00"	335.55	334.85
3 119 = 684' 00"	335.50	334.80
3 120 = 690' 00"	335.45	334.75
3 121 = 696' 00"	335.40	334.70
3 122 = 702' 00"	335.35	334.65
3 123 = 708' 00"	335.30	334.60
3 124 = 714' 00"	335.25	334.55
3 125 = 720' 00"	335.20	334.50
3 126 = 726' 00"	335.15	334.45
3 127 = 732' 00"	335.10	334.40
3 128 = 738' 00"	335.05	334.35
3 129 = 744' 00"	335.00	334.30
3 130 = 750' 00"	334.95	334.25
3 131 = 756' 00"	334.90	334.20
3 132 = 762' 00"	334.85	334.15
3 133 = 768' 00"	334.80	334.10
3 134 = 774' 00"	334.75	334.05
3 135 = 780' 00"	334.70	334.00
3 136 = 786' 00"	334.65	333.95
3 137 = 792' 00"	334.60	333.90
3 138 = 798' 00"	334.55	333.85
3 139 = 804' 00"	334.50	333.80
3 140 = 810' 00"	334.45	333.75
3 141 = 816' 00"	334.40	333.70
3 142 = 822' 00"	334.35	333.65
3 143 = 828' 00"	334.30	333.60
3 144 = 834' 00"	334.25	333.55
3 145 = 840' 00"	334.20	333.50
3 146 = 846' 00"	334.15	333.45
3 147 = 852' 00"	334.10	333.40
3 148 = 858' 00"	334.05	333.35
3 149 = 864' 00"	334.00	333.30
3 150 = 870' 00"	333.95	333.25
3 151 = 876' 00"	333.90	333.20
3 152 = 882' 00"	333.85	333.15
3 153 = 888' 00"	333.80	333.10
3 154 = 894' 00"	333.75	333.05
3 155 = 900' 00"	333.70	333.00
3 156 = 906' 00"	333.65	332.95
3 157 = 912' 00"	333.60	332.90
3 158 = 918' 00"	333.55	332.85
3 159 = 924' 00"	333.50	332.80
3 160 = 930' 00"	333.45	332.75
3 161 = 936' 00"	333.40	332.70
3 162 = 942' 00"	333.35	332.65
3 163 = 948' 00"	333.30	332.60
3 164 = 954' 00"	333.25	332.55
3 165 = 960' 00"	333.20	332.50
3 166 = 966' 00"	333.15	332.45
3 167 = 972' 00"	333.10	332.40
3 168 = 978' 00"	333.05	332.35
3 169 = 984' 00"	333.00	332.30
3 170 = 990' 00"	332.95	332.25
3 171 = 996' 00"	332.90	332.20
3 172 = 1002' 00"	332.85	332.15
3 173 = 1008' 00"	332.80	332.10
3 174 = 1014' 00"	332.75	332.05
3 175 = 1020' 00"	332.70	332.00
3 176 = 1026' 00"	332.65	331.95
3 177 = 1032' 00"	332.60	331.90
3 178 = 1038' 00"	332.55	331.85
3 179 = 1044' 00"	332.50	331.80
3 180 = 1050' 00"	332.45	331.75
3 181 = 1056' 00"	332.40	331.70
3 182 = 1062' 00"	332.35	331.65
3 183 = 1068' 00"	332.30	331.60
3 184 = 1074' 00"	332.25	331.55
3 185 = 1080' 00"	332.20	331.50
3 186 = 1086' 00"	332.15	331.45
3 187 = 1092' 00"	332.10	331.40
3 188 = 1098' 00"	332.05	331.35
3 189 = 1104' 00"	332.00	331.30
3 190 = 1110' 00"	331.95	331.25
3 191 = 1116' 00"	331.90	331.20
3 192 = 1122' 00"	331.85	331.15
3 193 = 1128' 00"	331.80	331.10
3 194 = 1134' 00"	331.75	331.05
3 195 = 1140' 00"	331.70	331.00
3 196 = 1146' 00"	331.65	330.95
3 197 = 1152' 00"	331.60	330.90
3 198 = 1158' 00"	331.55	330.85
3 199 = 1164' 00"	331.50	330.80
3 200 = 1170' 00"	331.45	330.75
3 201 = 1176' 00"	331.40	330.70
3 202 = 1182' 00"	331.35	330.65
3 203 = 1188' 00"	331.30	330.60
3 204 = 1194' 00"	331.25	330.55
3 205 = 1200' 00"	331.20	330.50
3 206 = 1206' 00"	331.15	330.45
3 207 = 1212' 00"	331.10	330.40
3 208 = 1218' 00"	331.05	330.35
3 209 = 1224' 00"	331.00	330.30
3 210 = 1230' 00"	330.95	330.25
3 211 = 1236' 00"	330.90	330.20
3 212 = 1242' 00"	330.85	330.15
3 213 = 1248' 00"	330.80	330.10
3 214 = 1254' 00"	330.75	330.05
3 215 = 1260' 00"	330.70	330.00
3 216 = 1266' 00"	330.65	329.95
3 217 = 1272' 00"	330.60	329.90
3 218 = 1278' 00"	330.55	329.85
3 219 = 1284' 00"	330.50	329.80
3 220 = 1290' 00"	330.45	329.75
3 221 = 1296' 00"	330.40	329.70
3 222 = 1302' 00"	330.35	329.65
3 223 = 1308' 00"	330.30	329.60
3 224 = 1314' 00"	330.25	329.55
3 225 = 1320' 00"	330.20	329.50
3 226 = 1326' 00"	330.15	329.45
3 227 = 1332' 00"	330.10	329.40
3 228 = 1338' 00"	330.05	329.35
3 229 = 1344' 00"	330.00	329.30
3 230 = 1350' 00"	329.95	329.25
3 231 = 1356' 00"	329.90	329.20
3 232 = 1362' 00"	329.85	329.15
3 233 = 1368' 00"	329.80	329.10
3 234 = 1374' 00"	329.75	329.05
3 235 = 1380'		

LANTANA Dr. Seabrook Cont.

34346 X

SL STA.	S of	N of
8+46.76 = PC	339.0	338.50
① 4 = 40' 26"	338.85	338.38
② WLF = 15886	338.70	338.26
③ WL ch = 1495	338.55	338.14
④ EL n = 189	338.40	338.02
⑤	338.20	337.90
⑥	338.10	337.80
⑦ S of dell = 03965	337.70	337.60
⑧	337.30	337.20
⑨	337.0	336.90
10 9+96.59 = EC	336.50	336.30
10+16.57 (BRK)	335.80	335.70
10+36.57 (H)	335.00	334.90
10+68.57 (M)	333.40	334.0
11+04.95	331.50	332.0

BREAK ON EAST OR NORTH

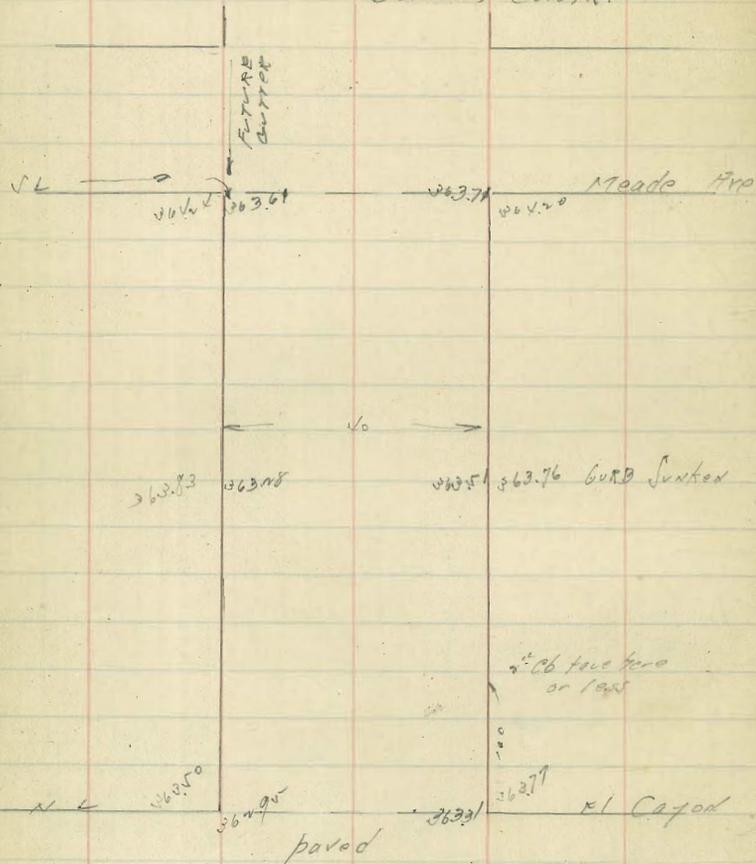
2.26
2.39.20
70 BREAKS

S	38.6 +2.4	38.3 +2.2	38.0 +2.1	37.6 +2.2	37.2 +2.2	36.9 +2.2	36.5 +2.2	36.2 +2.2
N	38.3 +2.6	38.1 +2.5	37.9 +2.3	37.7 +2.2	37.5 +2.1	37.1 +2.0	36.7 +1.9	36.3 +1.8
S	35.8 +2.7	35.5 +2.5	35.2 +2.3	34.8 +2.1	34.5 +2.0	34.2 +1.9	33.8 +1.8	33.5 +1.7
N	35.9 +2.6	35.5 +2.5	35.2 +2.3	34.8 +2.1	34.5 +2.0	34.2 +1.9	33.8 +1.8	33.5 +1.7
S	35.8 +2.7	35.5 +2.5	35.2 +2.3	34.8 +2.1	34.5 +2.0	34.2 +1.9	33.8 +1.8	33.5 +1.7
N	35.9 +2.6	35.5 +2.5	35.2 +2.3	34.8 +2.1	34.5 +2.0	34.2 +1.9	33.8 +1.8	33.5 +1.7
S	37.0 +2.9	36.5 +2.8	36.0 +2.7	35.5 +2.6	35.0 +2.5	34.5 +2.4	34.0 +2.3	33.5 +2.2
N	36.9 +2.8	36.4 +2.7	36.0 +2.6	35.5 +2.5	35.0 +2.4	34.5 +2.3	34.0 +2.2	33.5 +2.1

7/3/25 Copeland ST PAVING 5" Brown
 Moore EL Cajon to 5' Meado M'face
 DENNIS, CONTR.

363.56 SWBP EL Cajon & Van Dyke
 363.95
 5.15
 363.79
 4.15
 368.04

4



John
Moore

Lincoln Five Paving

8" cb face
6" crown

B. Carroll

PARK

Valley
paved

DIV.

321.10 = NEBP

321.09	320.76	321.67	321.10
321.06	321.0	321.1	321.0
	1733	1733	1733

321.69	321.07	321.83	321.7	321.14	321.37
--------	--------	--------	-------	--------	--------

321.90	321.93	321	321	321.28	321.91
321.30	321.35	321	321	321.0	321.28

321.71	321.75	321	321.74	321.07	321.07
--------	--------	-----	--------	--------	--------

321.87	321.87	321	321	321.07	321.76
--------	--------	-----	-----	--------	--------

321.61	321.92	321	321	321.07	321.43
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BREAK

321 321.6

This section to be figured from curb cuts

Georgia

paved

ST

316.84
12.63
329.47
0.00
329.47
0.01
329.48

NEBP UNIV. & PARK DIV

5

47.9
321.15
5.18
327.09
8.77
328.82
1.22
329.74

7/1/28 Retaining Wall. Filex 137 U.H.
Moore

FOR STONEBRICKER LINT Cleveland
Anderson = CONTR.

WINON SEBP Tylon
Cleveland
12.97
322.99
0.00
322.99
12.01
337.83

300' S of SL Van Buren W 333.85
350 " " " " " 331.0 = PREXX
391 " " " " " 329.85

331.0 333.85 334.87 = RIM M.H.
6.83 3.98 3.26
✓ ✓ ✓
329.85
5.77
8.77
- 3.00

PAC. Beach Sewer
TANK & OUTFALL
F.L.

002 DMH (#2)	27.94	
" " = DRAP	23.82	
0450	23.61	
1	23.40	
1 + 27.33 = MH (#1) = 5' x 9' LT	23.29	
1 + 61.83	23.13	eleven footings
1 + 98.33 = 5' end 1st Trestle #1 Pier	22.97	20.00
2 + 10.33	42 "	16.00
2 + 22.33	18" dia pipe #3 "	13.00
2 + 34.33	#4 "	15.00
2 + 46.33 = 5' end Trestle #5 "	22.77	19.00
2 + 58.33	22.56	
3 + 44.33 = MH (#6)	22.36	
3	22.13	
3 + 11.33	21.90	
3	21.66	
3	21.43	
3 + 16.33 = 5' end trestle #4	21.20	
6 + 28.33 = Conc pier 18" dia pipe		17.00
6 + 40.33 = 5' end trestle	21.10	
6 + 52.33 = 5' end trestle Conc pier	20.91	19.00
6 + 97.33 = Conc pier 24" dia pipe		12.00
7 + 09.33 = 5' end trestle Conc pier	20.81	19.00
7 + 25.33 = MH (#8) 5' x 9' LT	20.72	
7	20.57	
7	20.31	

5' x 9' x 7' max

5' x 9' x 7' max

PAC. Beach Sewers

	EL.	EL. FOOTINGS
20.09	20.09	
29 + 0.49 = Sand Tranche (Pier #1	19.88	17.00
15' 14" C.I. pipe		13.00
" #2		6.60
" #3		15.00
" #4		17.00
4 + 70.33 = Sand Tranche	19.67	Higher
10 + 11.33 = DMH # (12)	DROP = 19.50	21.60 = F.L.
+ 61.33	19.30	
11 + 11.33	19.10	
+ 61.33	18.89	
19 + 11.33	18.68	
14 + 59.73 = INTAKE of TANK	18.50	

SEWER IN BIK 1 NEIGHBORHOOD - Tye TRACT #1

DMH # 12 21.60

2		
3		
4 = MH # (11)	25.85	Rim 33.00
20.90		
12 = MH # (16)	28.55	
4		
5		
6		
7 = DE	38.67	

$$\begin{array}{r} 22.00 \\ + 9.85 \\ + 5.85 \\ + 24.97 = \text{SE TOP TANK} \\ \hline 62.67 \\ + 29.25 \\ + 5.00 \\ + 24.81 = \text{NE " " } \\ \hline 121.73 \end{array}$$

$$\begin{array}{r} 7.96 = \text{DM pipe} \\ + 10.31 \\ \hline 20.27 \end{array}$$

$$\begin{array}{r} 1.50 = \text{EIV OUTLET} \\ + 18.77 \\ + 4.60 \\ + 14.13 \\ \hline 38.90 \end{array}$$

$$\begin{array}{r} 10.65 = 7 \\ - 11.10 = \text{BREAK} \\ \hline 21.75 \\ + 10.88 \\ + 8.87 \\ \hline 41.50 \end{array}$$

Bench Marks - Pacific Beach

NE Mon	803	25.83		17.80	Cass + Ground
T.P.	868	33.34	119	42.64	
NE BP			4.44	48.55	Garnet Cass
10' CT. TR. SW COR = BM	8965	41.045	1.24	37.08	Felton Cass
NWBP			3.045	38.00	Emerald Cass
T.P.	506	41.315	479	36.255	
NWBP			3.76	37.555	Diamond Bayard
T.P.	11.705	52.165	0.855	40.46	
T.P.	10.54	62.685	0.00	52.165	
NWBP			3.795	58.89	LAW Bayard
T.P.	2.77	59.525	5.93	56.755	
CT. IN CURB NW COR			5.705	53.84	LAW + Allison
T.P.	0.14	50.125	7.54	50.005	
CT. IN CURB NW COR	5.25	44.15	8.325	41.80	ONLAW + DIXIE DRIVE
T.P.	766	48.46	3.35	40.80	
BM. 8400 Rd/line			10.25	38.41	on Boulder
T.P.	7.395	51.755	6.10	42.36	
SEBP			5.769	45.992	Loring + Ocean Blvd

38.41
+ 0.02
38.43
- 13.16
25.27
+ 1.57
26.64
- 12.47
14.17
+ 0.67
14.84
- 10.76
4.08
6.57
10.65
2.69
+ 7.96 = 11.50

6.05
4.60 OK
4.60
check
to BM
on shore

BM.
1" pipe on Shore line approx. 40' North of OUTFALL 7.96

SEWER CONSTRUCTION
LARK ST. & WALNUT.

SEWER PITCH/BAUGH
LARK

FL.

11

Station	FL.	Notes
N.S. of S.L. PITCH/BAUGH = DE. = 00	250.40	16.99 5.13 +11.86
0+46	249.27	18.06 1.11 +16.95
1+14	248.13	19.00 1.33 +7.84
1+68 = M.H. (#1)	247.0	7.27 1.30 +5.97
0	246.40	11.87 4.20 +7.67
0 4.33 6 TIMES	237.81	16.46 12.83 +3.63
0	233.00	5.09 4.84 +0.25
0	228.63	12.68 2.01 +10.67
0	224.04	5.36 1.95 +3.41
0 4+58 = D.M.H. (#2)	219.65	9.95 4.91 +5.04
" " " = DROP	207.0	20.40 4.41 +15.99
0	207.40	41.98 7.00 +14.98
0 5.75 4 TIMES	207.85	41.55 9.28 +12.27
0	208.27	41.13 8.14 +12.99
0 = 90° S = D.E.	208.70	20.70 5.26 +15.44
00 = D.M.H. (#2)	207.0	+17.49
07.30 = P.V.C.	205.20	12.91 0.68 +12.23
0+40	204.08	14.03 5.40 +8.63
0+50	201.90	16.21 4.27 +11.94
0+60	198.68	19.63 9.73 +9.90
0+70 = E.V.C.	194.40	33.71 12.68 +21.03
1+10 = BREAK	175.20	18.06 10.55 +7.51
0 4.75 1 TIME	166.07	15.15 3.12 +12.03
0	156.85	14.37 12.27 +2.10

③ = BREAK	147.67	21.80 8.33 +13.47
④ = 1+77 = M.H. (#3) = UNION ST.	138.50	
" " DROP	137.0	20.13 9.51 +10.62

Station	FL.	Notes
Culv. #3 + #4		
66 INLET #3 BOTTOM BOX	221.00	14.30 6.55 +7.75
" " #4 " " = 00	219.80	16.45 10.25 +6.20
0+45	205.40	18.84 5.84 +13.00
0+90	191.00	19.90 7.25 +12.65
		TOP CURB
		S. END
		N. END
66 INLET #2	227.40	8.9 6.48 +2.42
" " #4	226.80	9.48 10.05 -0.57

27.00	27.00	26.24	27.00
11.19	10.12	11.97	11.19
9.24	9.38	13.24	9.24
14.02	14.02	10.77	14.02

6.10 below
send drawing

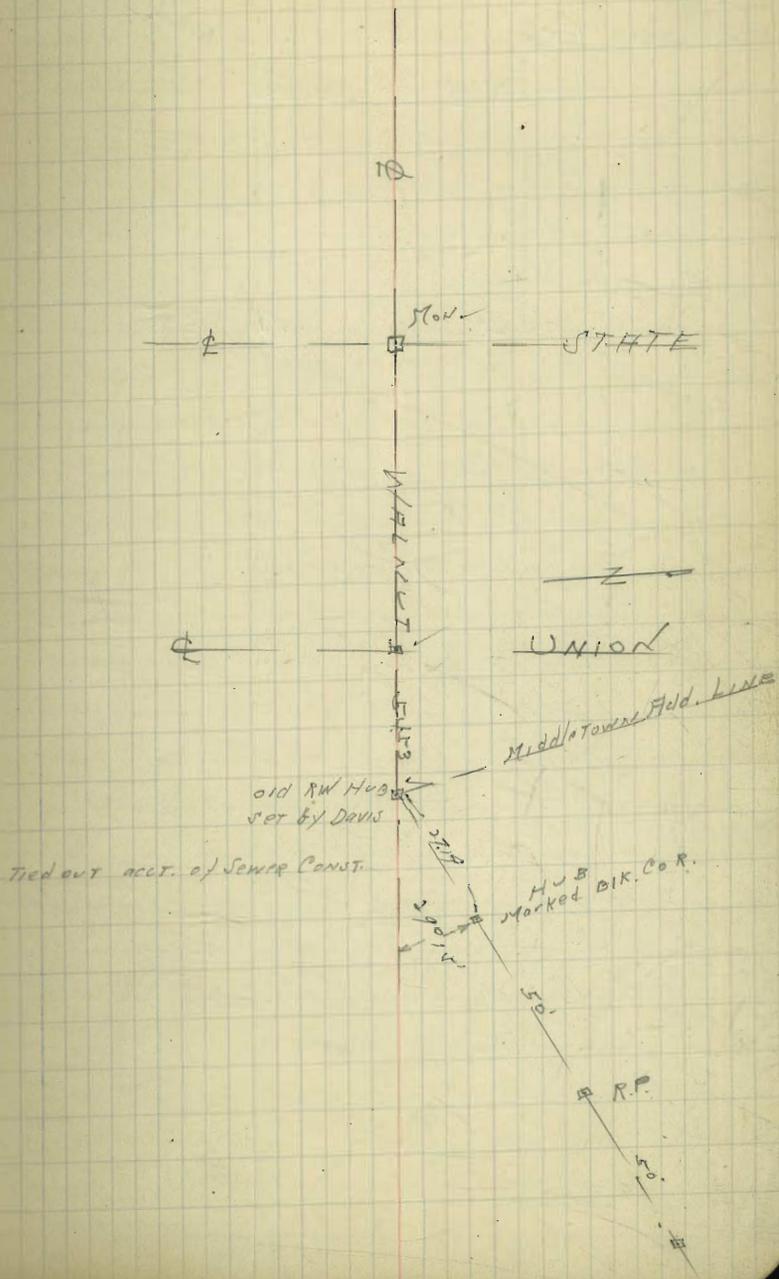
218.76 T

	FL.		
CB. inlet #6 = 00 BOTTOM BOX	215.0	3.76 0.69 +1.05	
0+20 = BREAK	207.0	11.74 3.08 +3.70	
0+40 = CB. inlet #7	203.0	15.74 7.70 +8.04	
0+80 = BREAK	196.0	9.84 4.50 +5.3	305.54 = T
0+97 = A = CLEANOUT 40° L	188.0	17.8 2.5 +18.3	197.0
1+50 = BREAK	170.0	23.26 3.5 +19.76	193.26 = T
1+65	159.50	11.7 1.3 +13.0	181.2 T
2+10 = BREAK	149.0	20.47 3.65 +16.82	169.87
2+48 = A 27° L	146.43	10.7 6.7 +17.0	152.13
2+84	144.0	13.1 10.7 +23.8	or -1.5 above Road

	N	E	S
CURB. inlet #6 Top curb	4.25 223.75 5.01 2.69 -7.70	223.50	222.15 223.05 4.81 3.07 -6.53
" " #7 " "	210.25 8.49 7.70 +0.79	210.20	210.20 8.54 8.32 +0.22

Culvert #1 + #2

	FL.	
CURB inlet #1 BOTTOM BOX	239.00	225.97 1.16 227.13 13.06 240.19 = TP 1.09 241.16 11.60 252.76 0.78 253.54 13.06 266.60 0.28 266.88 2.08 268.96
" " #2 " " = 00	237.2	
0+44	220.7	
0+90 = OUTLET	204.0	



HORTON AVE PAVING

BREAKS NOT OPPOSITE

W.L. STA.	WCB	EL STA.	ECB
JL Upas	225.50		226.4
NL " ON WEST = 00	226.50		227.0 ON EAST = 00
0 + 10.5 = PC RETURN	227.40	0 + 35.28	229.90
0 + 68.4 = BREAK	232.40	0 + 70.86	232.80 BREAK
0 + 75.89 = PC ON WEST	232.64	0 + 81.76	232.53 = P.C.
0 + 88.04 = BREAK	233.30	0 + 90.56	234.10 = BREAK
0 + 99.04	233.80	1 + 00.56	234.52
1 + 08.04 = BREAK	234.30	1 + 10.56	235.0 = Horton Line
1 + 22.72	234.80		
1 + 37.4 = Horton Line	235.30		

W.L. chords	chords	def.	EL chords	defl.
12.14	def. = 2° 00' 51"	8.80	2° 03' 10"	
10.0	" = 3° 40' 21"	10.0	4° 23' 08"	
9.99	" = 5° 19' 51"	10.0	6° 43' 06"	
14.67	" = 7° 45' 51"		= Horton Line	
14.67	" = 10° 11' 51"			

$A = 36^{\circ} 06'$
 $\Phi R = 147.80$
 $T = 48.16$

W	225.5	226.5	227.4	228.4	229.6	230.3	230.8	231.3
	10.8	9.2	7.9	6.1	3.7	3.0	2.4	2.0
	10.8	7.5	7.2	5.0	4.9	2.8	2.7	2.0
	-1.2	+2.3	+1.7	-1.1	1.2	-1.1	-1.4	-2.0

PC RETURN
 225.5
 10.8
 10.8
 -1.2
 226.5
 9.2
 7.5
 +2.3
 227.4
 7.9
 7.2
 +1.7
 228.4
 6.1
 5.0
 -1.1
 229.6
 3.7
 4.9
 1.2
 230.3
 3.0
 2.8
 -1.1
 230.8
 2.4
 2.7
 -1.4
 231.3
 2.0
 2.0
 -2.0

235.04 = 82 Mile + Horton

1374
1368.14

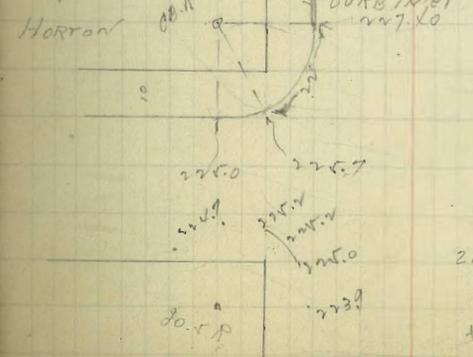
FINISH STAKES

E	225.70	226.00	226.80	227.80	228.58	229.10	230.55	231.00
	10.71	8.41	6.51	3.61	2.88	2.31	1.86	1.41
	10.79	8.31	5.81	3.58	3.18	2.66	2.25	1.85
	-0.58	+2.10	+1.14	+0.05	-0.30	-0.35	-0.39	0.00 low

PC
 225.70
 10.71
 10.79
 -0.58
 226.00
 8.41
 8.31
 +2.10
 226.80
 6.51
 5.81
 +1.14
 227.80
 3.61
 3.58
 +0.05
 228.58
 2.88
 3.18
 -0.30
 229.10
 2.31
 2.66
 -0.35
 230.55
 1.86
 2.25
 -0.39
 231.00
 1.41
 1.85
 0.00 low

W	225.50	226.00	226.80	227.80	228.58	229.10	230.55	231.00
	10.71	10.86	10.86	7.01	4.21	3.77	3.11	2.61
	11.26	10.86	10.86	7.51	4.78	4.64	3.75	3.59
	-0.65	+0.05		-0.50	-0.77	-0.87	-0.84	-0.78

225.50
 10.71
 11.26
 -0.65
 226.00
 10.86
 10.86
 +0.05
 226.80
 10.86
 10.86
 227.80
 7.01
 7.51
 -0.50
 228.58
 4.21
 4.78
 -0.77
 229.10
 3.77
 4.64
 -0.87
 230.55
 3.11
 3.75
 -0.84
 231.00
 2.61
 3.59
 -0.78



225.20	225.20	225.00
12.41	12.41	12.61
12.04		12.71
+0.35		-0.16

7/24/58
Stoore

ALLEY PAVING BRK 461
Winder Sub.

	S		N	30' wide	
ELKITE = 00	266.10		266.11		} Profile
0+20	263.9	BREAK	264.2		
0+40	262.4	"	262.70		
0+69	260.77		260.82		
0+98	259.14	258.71	258.94	= W/L JACKMAN on paving	

BROWN - CONTR.

	S		N
EL KITE	266.0		266.10
0+20	263.20 = Drive		263.50
0+40	261.60		261.90
0+69	260.77		261.07
0+98 = W/L Jackman	259.14		259.00

266.81
3.20
270.01
NW Top Wall TORRENCE & KITE

S	266.0 4.77	263.20 7.57	261.60 9.17	260.27 10.00	259.14 11.63
		7.56	8.17	9.66	
		+0.01	+1.00	+0.34	
		ON DRIVE			
N	266.10 4.67	263.50 7.27	261.90 8.87	261.07 9.70	258.94 11.83
		6.63	7.97	8.78	
		+0.64	+0.90	+0.97	

* LARK St. Cont.

Moore

4-9-25

Location of Garage in Walnut
at Lark St.

Indexed

C.S.K.

21

~~ST. LARK~~



Walnut
St.

Lark

Pac. Beach Sewer
AT MILITARY School

alley North
of Garnot
CARNOT
Ingraham

8" LINE	F.L.	
E. Ingraham = Ex. Sewer = 00	59.38	13.97 7.32 +6.70
0 + 50	59.79	13.67 6.50 +7.17
1	60.08	13.77 6.15 +7.13
+ 50	60.43	14.97 6.23 +6.29
2	60.78	14.87 5.61 +6.96
+ 50 = M.H. # 163	61.13	14.87 5.56 +6.66
3	61.48	11.87 5.18 +6.69
+ 50	61.83	11.87 5.08 +6.39
4	62.18	11.17 5.00 +6.17
+ 50	62.53	10.87 4.91 +4.91
5	62.88	10.27 3.22 +4.00
+ 50 = M.H. # 164	63.16	10.19 3.20 +6.49

alley North of Teispar 6" LINE

E. Ingraham = 00 = Ex. Sewer	66.32	10.31 4.88 +6.06
0 + 50	66.67	9.96 4.32 +4.91
1	67.04	9.61 4.17 +4.91
+ 50	67.37	9.26 3.93 +4.93
2	67.72	8.91 3.84 +4.97
+ 50 = M.H. # 181	68.07	8.56 3.51 +4.97
3	68.42	8.21 2.83 +4.95
+ 50	68.77	7.86 1.62 +6.24
4	69.12	7.51 1.06 +6.45
+ 50	69.47	7.16 1.08 +6.08
5	69.82	6.81 0.91 +6.20
+ 50 = M.H. # 182 = Jewell	70.10	6.49 1.11 +6.17

10.25
73.35
1.64
71.73 TP

1875
1500

① = 7 + 15 = Jewell Emerald M.H. # 183

② = 7 + 15 = EAST ON Jewell

③ = 9 + 15 = M.H. # 184

④ = 9 + 15 = M.H. # 184

⑤ = 11 + 15 = M.H. # 185

⑥ = 11 + 30 = M.H. # 185

⑦ = 11 + 30 = M.H. # 185

⑧ = 11 + 30 = M.H. # 186

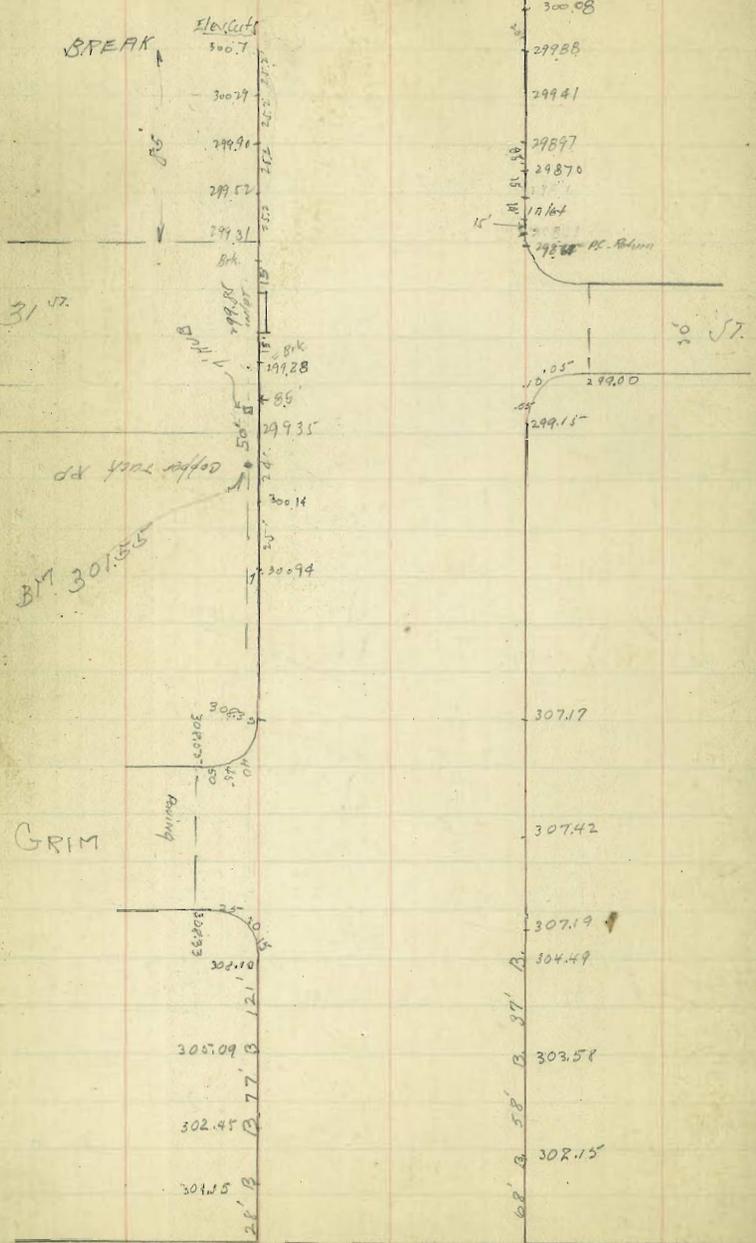
⑨ = 11 + 30 = M.H. # 186

⑩ = 17 + 15 = D.E.

F.L.	
71.06	13.09 7.06 +4.97
72.02	11.09 6.91 +4.86
72.98	11.11 4.81 +6.30
73.94	10.14 3.80 +6.34
74.31	15.87 9.50 +6.07
74.67	15.57 9.30 +6.13
75.03	15.14 9.09 +6.17
75.39	14.79 8.73 +6.06
75.75	14.43 8.37 +6.12
77.50	12.68 7.08 +4.62
79.25	10.93 5.69 +4.92
81.00	9.11 4.23 +4.93
82.75	7.43 2.39 +4.82
84.50	5.68 0.99 +4.06
85.27	4.26 1.77 +4.61
86.04	3.59 0.73 +6.23
86.81	1.78 0.46 +6.34
87.58	1.04 0.22 +4.81
88.36	11.27 5.40 +6.27
89.13	10.50 4.98 +6.12
89.90	0.73 3.66 +6.07
90.67	8.96 2.96 +6.00
91.44	8.19 2.07 +6.17
92.21	7.41 1.87 +5.86

Redwood St. Paving

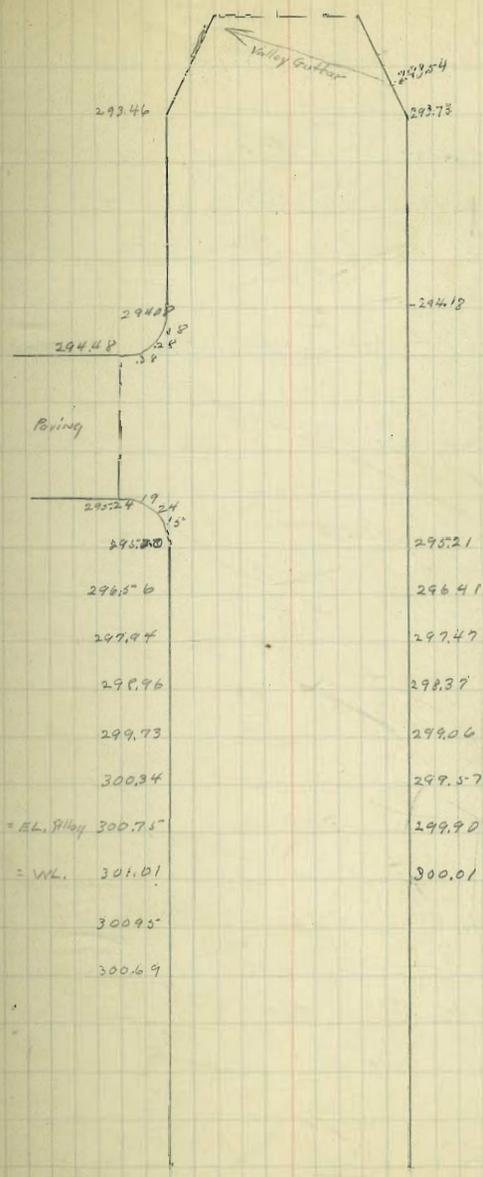
Elev. Cuts
300.00



50+7

Bridge

24



BREAK

301.55
301.50
301.50

Redwood St

GRADES

EL + W 3/10T	0445	0425	1405	2110	2125
N. 300.0 4.50 L	300.75 3.75	301.55 4.95	301.81	301.82	
WL N. 300.0 4.50 L	EL + W 3/10T 299.40 2.10	EL 299.00 2.95 2.74	300.80 3.70	300.88 3.62	
1/301.65	301.25	300.61	299.76	298.69	297.60
1/300.75	300.85	299.95	299.01	298.30	297.20
WL N. 296.0	EL Herman 295.0				
1/296.0	295.0				

CURB CONSTRUCTION N. side Imperial
FRONTING ON Jewish Cemetery

130/78

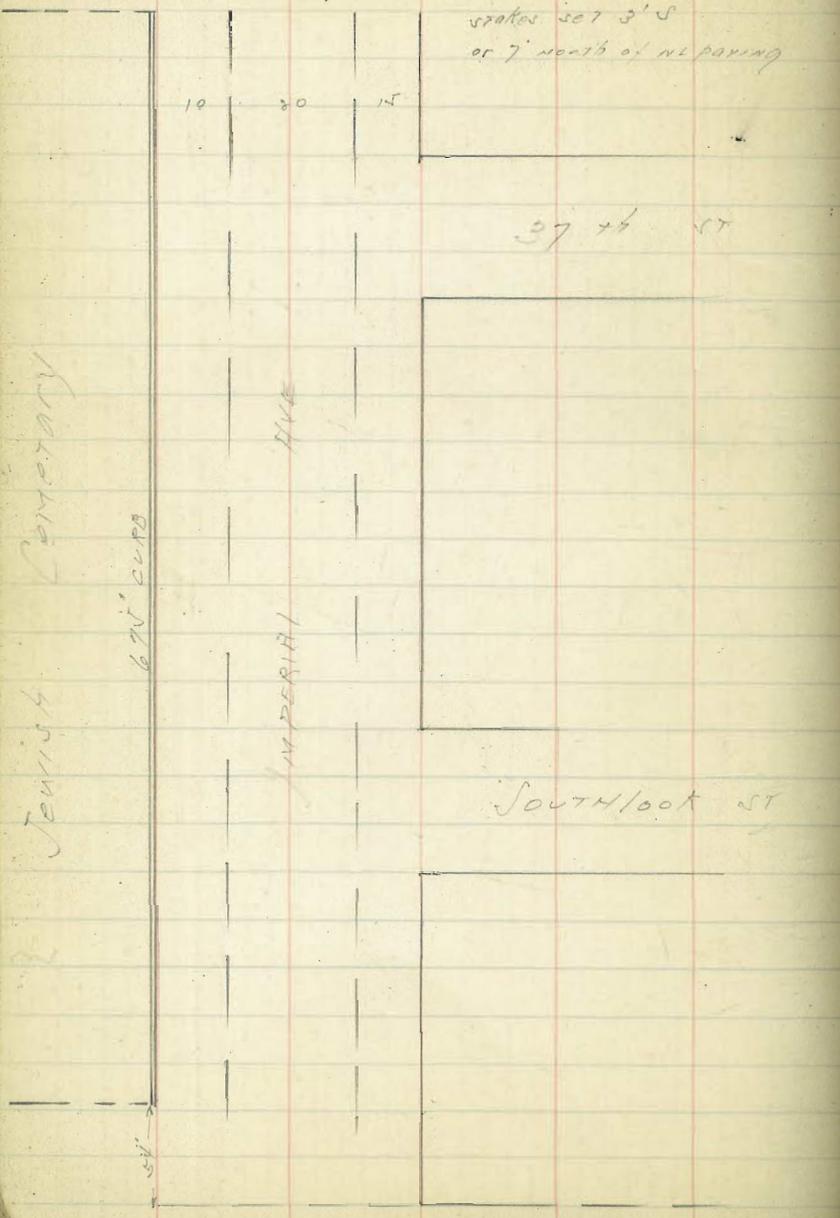
MOORE
OSBORNE
POOR

SET 25 44

Imperial
38x5

22.5
5.5
102.07
2.29
99.03
4.16
103.19

26



Station	paring	curb	Notes
EL 96 ⁺ 200			
0 + 74 =	95.33	95.93	WL Jewish Cemetery +0.60
0 + 70 =	95.56	96.16	BREAK +0.60
0 + 90 =	96.56	97.16	" +0.60
1 + 10 =	97.26	97.84	" +0.60
1 + 30 =	97.62	98.22	" +0.60
1 + 50 =	97.80	98.40	BREAK +0.60
2 + 69 =	98.11	98.71	WL Southlook ✓
3 + 79 =	98.58	99.18	EL " ✓
4 + 98 =	99.57	100.17	WL 37th ST ✓
6 + 24 =		100.30	" " ✓
6 + 54 =	99.57	100.17	EL " " ✓
7 + 79 =	99.15	99.85	EL Jewish Cemetery ✓
5 + 64 =			+0.60 WLT 5 + 61.5 = 50.10
0 + 70 =			+0.60 5 + 92 = -0.60 = WL 37th
0 + 90 =			+0.60 6 + 24 = -0.60 = " "
1 + 10 =			+0.60 6 + 54 = -0.60 = EL " "
1 + 30 =			+0.50 6 + 91 = 0.0
1 + 50 =			+0.30 7 + 79 = 0.0
2 + 10 =			+0.50
2 + 69 =			0.0 WL Southlook
3 + 79 =			0.0 EL " "
3 + 79 =			-1.10
4 + 79 =			-1.30
4 + 79 =			-1.10
5 + 29 =			-0.80

Quince st Paving

8" curb face

5" Crown

E.L. Alloy Top of Curb =

Alm + 30th SW. RA. BM. 301.00

12.84

313.94

10.10

303.84 - T.P.

3.19

307.03

7.65

299.38

0.33

299.71

Culvert No. 1. Top of Curb = 303.0 Bottom of box = 298.75

4.03

7.65

-3.62

27.5

1.68

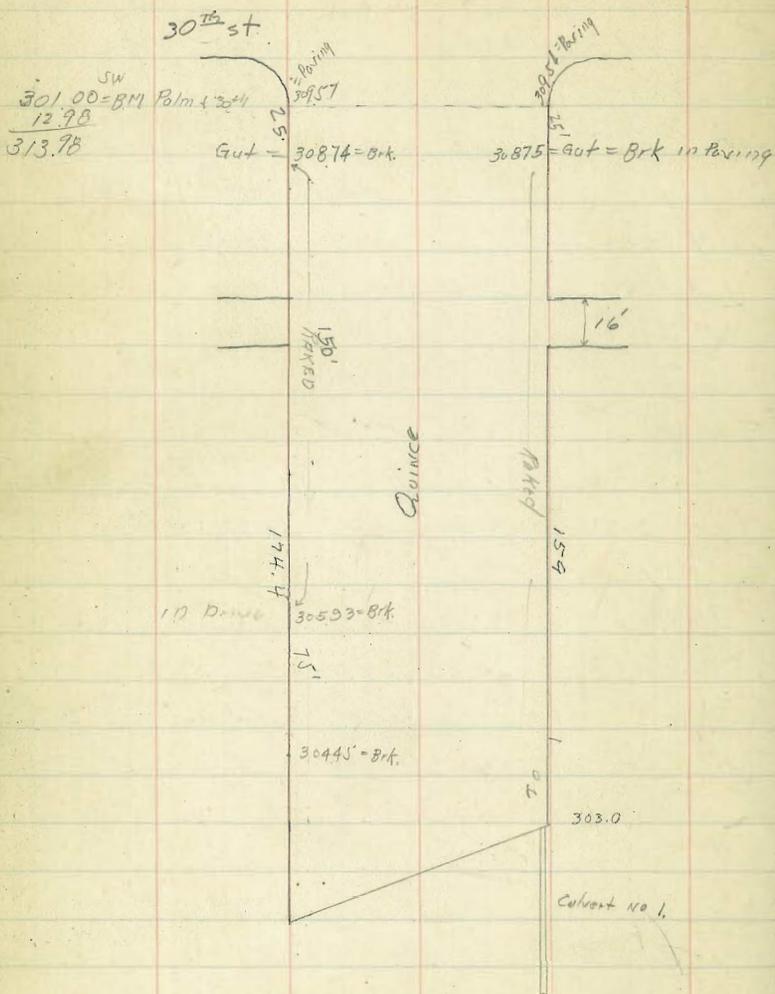
1.71

Outlets 1.41

End of curb on South = 303.70

3.28

Set to 300.85

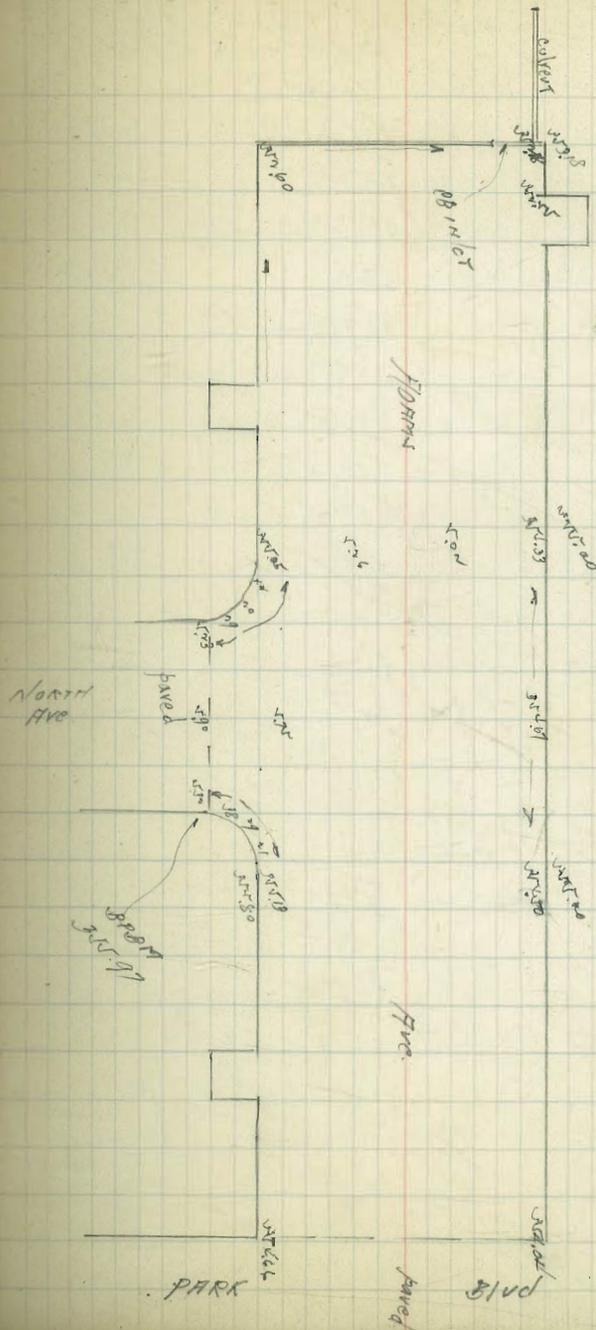


11/20/28 ADAMS Ave PAVING Floyd & GRIMES
Moore Park Blvd to Campus 6" crown

top 06 Fl. of Box Fl. outlet
w 3.40 w 4.50 w 4.80

28

Template = 17.33 length with .06 crown



11/10/88 WATER STAKES IN MILLS FLOYD & GRIMES CONTROL.
 Moore 69-80-96-108-125 CITY HATS
 stakes offset 2' east

Flowline	35.7	35.2	35.2
-30 EXISTING 10" MAIN	335.7	9.1	35.2
.00 = SL NIGHTMAN = (B)	335.7	6.5	35.2
0+15 (B)	331.2	4.2	35.2
0+50 (B)	327.5	3.7	35.2
1+00	327.0	1.0	35.2
1+50 (B)	326.3	2.8	35.2
2+10 (B)	321.4	7.4	35.2
2+45	321.4	4.2	35.2
2+80 (B)	313.5	27.0	35.2
3+20 (B)	305.6	8.2	35.2
3+65 (B)	305.3	5.5	35.2
4+10 (B)	305.0	2.7	35.2
4+50 (B)	305.0	21.4	35.2
5+85	315.8	13.1	35.2
5+20 (B)	314.3	9.2	35.2
5+40 (B)	320.8	4.6	35.2
5+60 (B)	329.3	13.5	35.2
6+00 = NL LANDIS	330.5	9.0	35.2
6+67.11 = FIRE PLUG	330.5	6.9	35.2
6+80 = SL " "	330.5	2.1	35.2
7+40 = (B)	327.3	0.5	35.2
7+85 = (B)	327.0	1.2	35.2
8+35	331.6	1.7	35.2
8+85	333.0	0.5	35.2
9+35	332.5	0.5	35.2
9+85	332.0	0.5	35.2

117 Bends

10+35	330.80	9.0	330.80
10+85	330.80	3.9	330.80
11+35	327.89	2.9	327.89
11+85	329.80	3.4	329.80
12+40 = (B)	329.0	3.3	329.0
12+80 = NL DWIGHT = (B)	327.2	11.1	327.2
13+47.11 = FIRE PLUG	327.0	5.0	327.0
13+60 = SL DWIGHT = (B)	326.5	5.7	326.5
14+10	326.0	3.7	326.0
14+60	325.5	6.7	325.5
15+10	324.9	3.2	324.9
15+60	324.4	7.8	324.4
16+10	320.9	3.5	320.9
16+60	320.3	8.9	320.3
17+10	322.8	9.4	322.8
17+60	322.3	9.7	322.3
18+10	321.8	6.5	321.8
18+60	321.3	10.9	321.3
19+05 = (B)	318.4	16.0	318.4
19+60 = NL MYRTLE (B)	317.8	18.3	317.8
20+10 = CI CROSS	316.8	1.6	316.8
20+27.11 = FIRE PLUG	315.9	6.7	315.9
20+40 = SL MYRTLE (B)	314.9	1.9	314.9
20+90	314.9	7.7	314.9
21+40	314.9	4.5	314.9
21+90	314.9	2.9	314.9

F.L.	39
336.13	336.13
335.94	335.94
335.75	335.75
335.56	335.56
335.37	335.37
335.18	335.18
334.99	334.99
334.80	334.80
334.61	334.61
334.42	334.42
334.23	334.23
334.04	334.04
333.85	333.85
333.66	333.66
333.47	333.47
333.28	333.28
333.09	333.09
332.90	332.90
332.71	332.71
332.52	332.52
332.33	332.33
332.14	332.14
331.95	331.95
331.76	331.76
331.57	331.57
331.38	331.38
331.19	331.19
331.00	331.00
330.81	330.81
330.62	330.62
330.43	330.43
330.24	330.24
330.05	330.05
329.86	329.86
329.67	329.67
329.48	329.48
329.29	329.29
329.10	329.10
328.91	328.91
328.72	328.72
328.53	328.53
328.34	328.34
328.15	328.15
327.96	327.96
327.77	327.77
327.58	327.58
327.39	327.39
327.20	327.20
327.01	327.01
326.82	326.82
326.63	326.63
326.44	326.44
326.25	326.25
326.06	326.06
325.87	325.87
325.68	325.68
325.49	325.49
325.30	325.30
325.11	325.11
324.92	324.92
324.73	324.73
324.54	324.54
324.35	324.35
324.16	324.16
323.97	323.97
323.78	323.78
323.59	323.59
323.40	323.40
323.21	323.21
323.02	323.02
322.83	322.83
322.64	322.64
322.45	322.45
322.26	322.26
322.07	322.07
321.88	321.88
321.69	321.69
321.50	321.50
321.31	321.31
321.12	321.12
320.93	320.93
320.74	320.74
320.55	320.55
320.36	320.36
320.17	320.17
320.00	320.00
319.83	319.83
319.66	319.66
319.49	319.49
319.32	319.32
319.15	319.15
318.98	318.98
318.81	318.81
318.64	318.64
318.47	318.47
318.30	318.30
318.13	318.13
317.96	317.96
317.79	317.79
317.62	317.62
317.45	317.45
317.28	317.28
317.11	317.11
316.94	316.94
316.77	316.77
316.60	316.60
316.43	316.43
316.26	316.26
316.09	316.09
315.92	315.92
315.75	315.75
315.58	315.58
315.41	315.41
315.24	315.24
315.07	315.07
314.90	314.90
314.73	314.73
314.56	314.56
314.39	314.39
314.22	314.22
314.05	314.05
313.88	313.88
313.71	313.71
313.54	313.54
313.37	313.37
313.20	313.20
313.03	313.03
312.86	312.86
312.69	312.69
312.52	312.52
312.35	312.35
312.18	312.18
312.01	312.01
311.84	311.84
311.67	311.67
311.50	311.50
311.33	311.33
311.16	311.16
310.99	310.99
310.82	310.82
310.65	310.65
310.48	310.48
310.31	310.31
310.14	310.14
310.00	310.00

FL.

322.7

19.23

309.76

6.66

310.42

12.91

297.51

6.04

297.54

12.56

284.67

0.06

284.74

14.91

271.82

3.54

275.36

22+40 = (A)

314.0

3.6

+5.3

+90

313.4

9.9

+5.3

23+40

314.5

10.1

+5.6

+90

311.7

10.9

+5.5

24+40

311.0

11.6

+5.8

+90

310.4

14.2

+5.9

25+40 = (A)

309.5

13.7

+5.6

25+45 = (B)

309.0

13.6

+5.0

26+40 = (B) = NL THORN = (B)

305.5

17.1

+5.9

27+07.11 = FIRE PUG

27+20 = SL THORN = (B)

304.8

5.6

+5.9

27+60 = (B)

305.9

4.5

+5.9

28

304.4

6.0

+5.5

29

302.8

7.6

+5.9

30

301.2

9.4

+5.4

31

299.6

10.5

+5.0

32

295.0

12.4

+5.0

31+20 = (B) = (B)

296.4

14.0

+5.9

31+47.5

293.8

13.0

+5.7

31+95 = (B)

291.2

6.3

+5.7

32+45 = (B)

281.0

17.0

+5.7

32+87.5

271.0

13.7

+5.5

33+20 = (B) = NL Redwood = (B) = 261.0

261.0

14.4

+5.5

33+87.11 = FIRE PUG

34+00 = SL Redwood

268.40

6.3

+5.9

275.36

0.37

274.99

12.76

262.23

0.04

262.27

12.36

249.91

10.84

239.07

0.04

239.11

9.44

229.67

1.57

228.10

330.00 NWBP DWIGHT & CENTRAL

0.01 error

279.4 = El. of STUB 3' S of F.H.

Blas
Duermit
Jacobson
Kramer
Hester

Curb Grades on Garnet Events
to Inq. HZ. - ERV

BM NW B P
Events Garnet 4.75 44.28 39.53

84.2 47.95 39.53

F.P. 5.14 50.75 2.34 95.61

BM SW 70TK
Fanuel r. Garnet 9.39 53.00 45.61

Set 8M SWV.
70TK Gresham 2.49 52.51

10.25 62.76 52.51

TP 9.49 72.10 0.15 62.61

Set 8M SW
70TK Haines r. Garnet 3.57 68.53

6.57 59.08 52.51

59.08
5.54
53.54

59.08
5.95
53.13

Bxk. 190-N. of the W. Line of Gresham

2.07 59.58 52.51

Waik. S side

59.58 54.58
4.93 4.98
49.65 49.60

Waik. N. Side

59.58 59.58
4.93 4.98
50.15 50.10

Events

31

44.28
4.20
Prop 40.08

44.28
39.91
4.37
4.24
Cox 13
meat walk Co 10

44.28
39.78

44.28
39.66 PC
4.62
4.50
4.40
Cox 10

44.28
4.68
39.60

50.75 1

N Side Prop 44.28
3.66
40.62

Fanuel

SW
50.75
5.23
45.52 Prop SW
50.35
5.18
45.16

NW
45.61
6.19
51.78 H.I.
5.27
46.11 Prop NW

SE Prop E

45.61 50.35
4.74 3.78
50.35 46.57
P.
50.35
4.18
46.17

N.E. Return

45.61 BM
6.82
52.43
5.31
47.12 Waik
52.93
5.36
47.07 CB

BM 52.51

6.91
59.42
±1 Prop

59.42
5.25
6.86 Prop

Gresham
SW Return

59.42
5.25
7.26

SE Return

E Prop 52.51
6.37
58.88 HZ
53.63
5.25

S Prop 58.88
53.23
5.65

NW Return

59.42
5.34
6.34

NE Return

58.88 HZ
54.4
4.44

58.88
54.14
4.74

#2
7210
Haines + Garnet

	3.76	72.29	68.53
3M SW 72 TR	4.53	73.06	68.53
	2.73	71.26	68.53
T.P.	3.65	68.99	5.92 65.39
			6.91 62.58
	5.25	67.79	62.59
	67.79	67.79	67.79
	4.71	4.51	5.77
	63.08	63.28	62.02

SW Return

7210	72.29
3.61	3.86
68.99	68.43

7210
3.08
69.02

32

NE Return

7306	7306
4.48	4.30
68.58	68.76

NW
73.06
4.11

SE Return

73.06	dropped	73.06
5.12		5.28
67.94	- E Prop	67.78

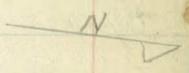
S.W.

7306
4.88
68.48

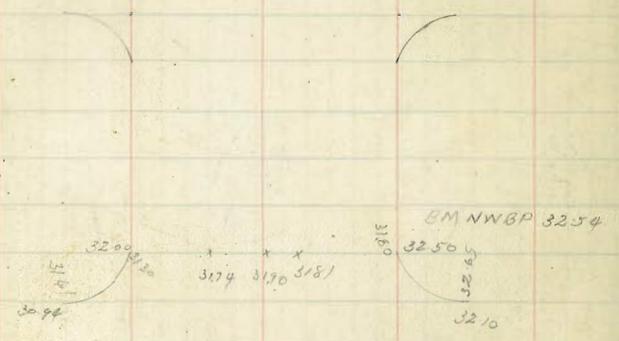
Bill Bliss
Overmit
Jacobson
Kiernan
11/17/9

+ HI Eke
Garnet Ave Paving from
Cass to Pendleton

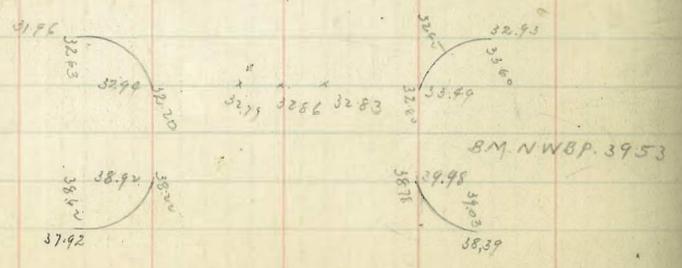
Cass



st



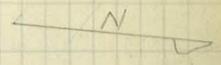
Daves



street

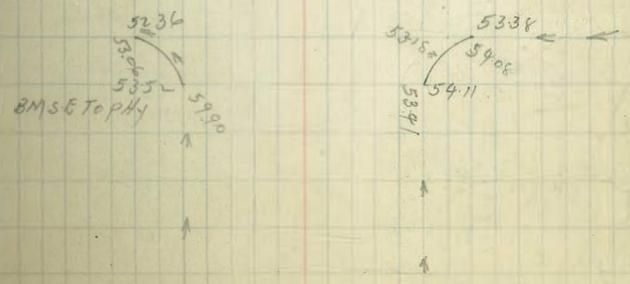
Events

Manuel



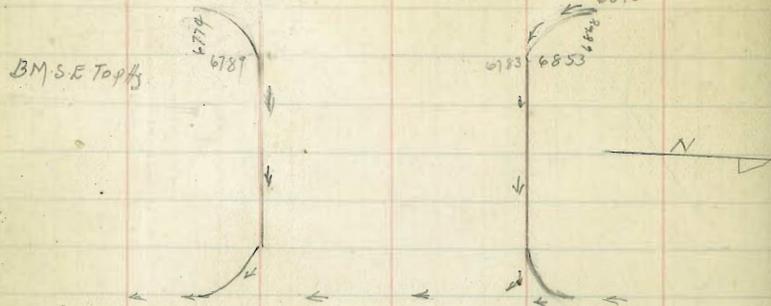
st

Gresham

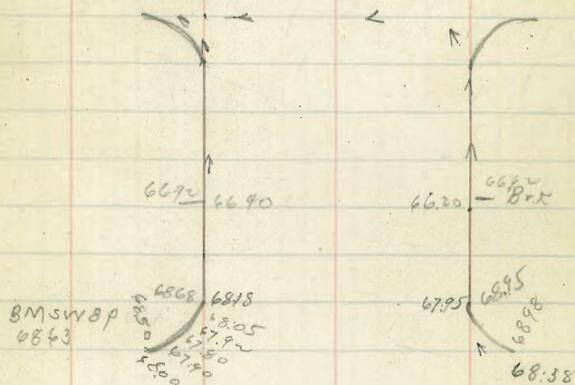


st

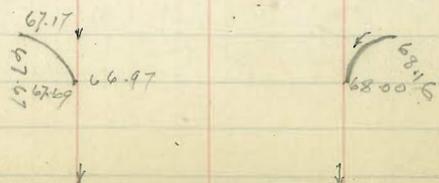
Haines



Torgreham

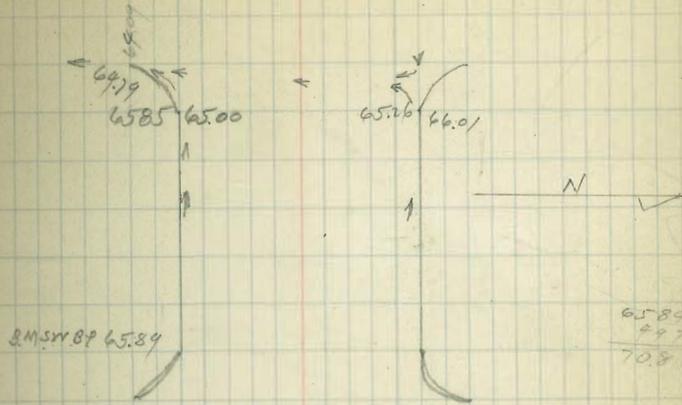


Jewell

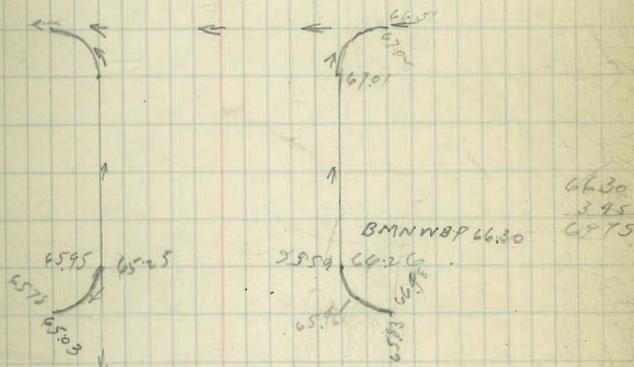


BM SW BP 6582, 6522, 6517

Kendall



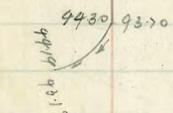
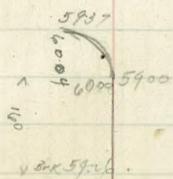
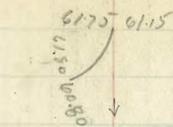
Lamont



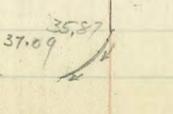
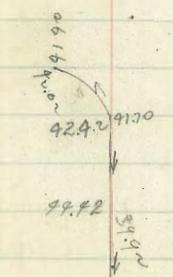
Marvell



Noyes

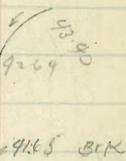
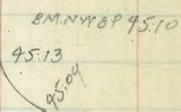
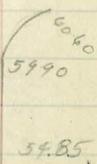
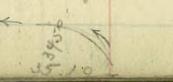


Olney



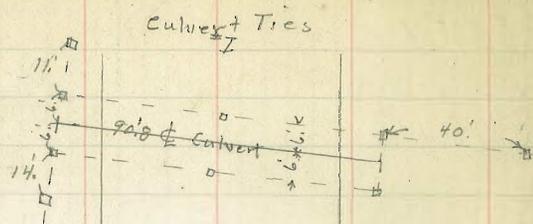
Set BM SE top of 37.09

Pendleton



3664
3587
c.77

Eads Ave Pavmt Etc



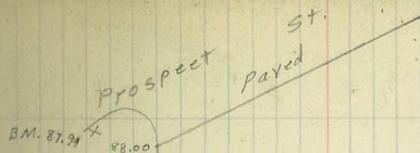
0.91 79.83 78.92

East End of Culvert 68.48 11.35

15.7 W 67.75 12.08

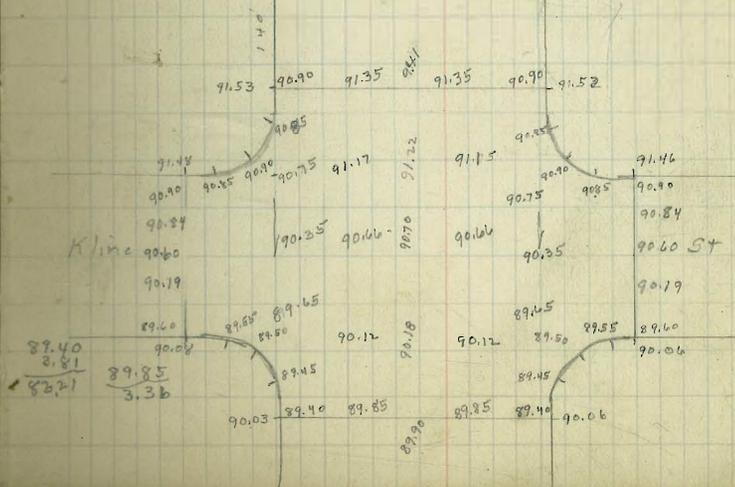
90.8 W End of Culvert 67.02 12.81

90.90	91.35	91.35	90.90		89.40
2.57	1.82	1.82	2.27		3.77
					93.17
90.90	90.75	91.17	90.75	90.90	
2.12	2.42	2.00	2.42	2.27	
90.84				90.84	
2.33				2.32	
90.60	90.35	90.66	90.66	90.35	5.64
2.57	2.82	2.51	2.51	2.82	47
					5.17
90.19				90.19	
2.98				2.78	
89.40	89.65	90.12	90.12	89.65	
3.57	3.52	3.05	3.05	3.52	
					3.59
89.40	89.85	89.85	89.40		
3.77	3.32	3.32	3.77		
					3.72
					3.50



Silverado paved St.

96.00	95.50	6.48	6.41	96.20	97.00	10.20	40.60	50.40	20
	95.70	6.38	6.61	96.40		37.02	50.42	42.22	
	95.80	6.48	6.71	96.50		70	80	70	65
						72	82	72	62
96.2	95.70	6.45	6.75	96.60	97.20	1.14	3.91	3.97	5.37
	95.60	6.31	6.58	96.40		75.43	91.52	91.46	90.00
	95.30	6.03	6.28	96.10	97.0		3.90	3.95	5.25
	94.80	5.51	5.78	95.60			91.52	91.44	90.00
							.20	.85	60
							.53	.58	.73
									.84
									.77
									.74
									.03



	W. cb		E. cb
00 = S. Line Rushville	129.00 3.72 3.63	131.00 1.72 132.72	130.00 2.72 2.56
+ 52.35	28.3 4.4 1.6 + 2.8		29.3 3.4 1.9 + 1.5
1 + 04.20	27.5 5.2 5.4 - 0.2		28.5 4.2 4.1 + 0.1
1 + 57.05	26.8 5.9 7.9 - 2.0		27.8 4.9 2.3 + 2.6
2 + 09.40	126.1 6.6 4.40 - 5.7		127.1 5.6 4.2 + 1.4

52.35
4.40
47.95

	W. cb	Culvert #2	E. cb
600 ft inlet 3 Torch	26.07 5.69 9.69 - 4.00	131.76	131.00 26.07
gutter grating			25.07
F.L.		20.85 10.91 8.65 + 2.26	20.85
Bottom Box			20.35
0 + 12.8 W. Lin +	20.40 11.36		20.40
0 + Toe slope outlet		20.00 11.8 10.7 + 1.1	20.00 26.37
E. End. cb. inlet	26.37 5.39 7.39 - 2.00		26.37
2.5 N. of E. end.		26.11 5.65 8.65 - 3.00	26.11

2.5
27.5
4.3
4.4
26.8
5.0
6.9
1.9

31.4
24.3
3.3
1.4

26.8
20.3
6

.01923
15.5
9615
9615
1923
298065

52 / 01923
100
52
480
468
120
104
160

Eads Ave Sewer Stakes

B.M.	0.67	131.67	130.00			
00 = D.E. - 56.4 s. of Ruskyville			4.05	27.62	123.20	+4.42
0+52			5.33	26.34	121.97	+4.37
1+04			6.59	25.08	120.73	+4.35
1+56 M.H. 1			5.34	26.33	119.50	+6.83
0+49 25			11.30	20.37	118.13	+2.24
0+98 50			12.07	19.60	116.75	+2.85
1+47 75			10.17	21.50	115.37	+6.13
					116.10 <small>cmh</small>	
1+97 ²³ D.M.H.R.T.P. 157	122.27	13.95	120.72	114.00		+6.72
0+30			2.55	15.74	113.70	+2.04
0+60 connection			6.48	15.81	113.40	+2.41

89.40
 7.13
 96.53
 0.56
 95.97
 3.23
 99.20

 7
 (4)
 90.1
 9.1
 7.0
 +5.1

Sewer Laterals

131.67

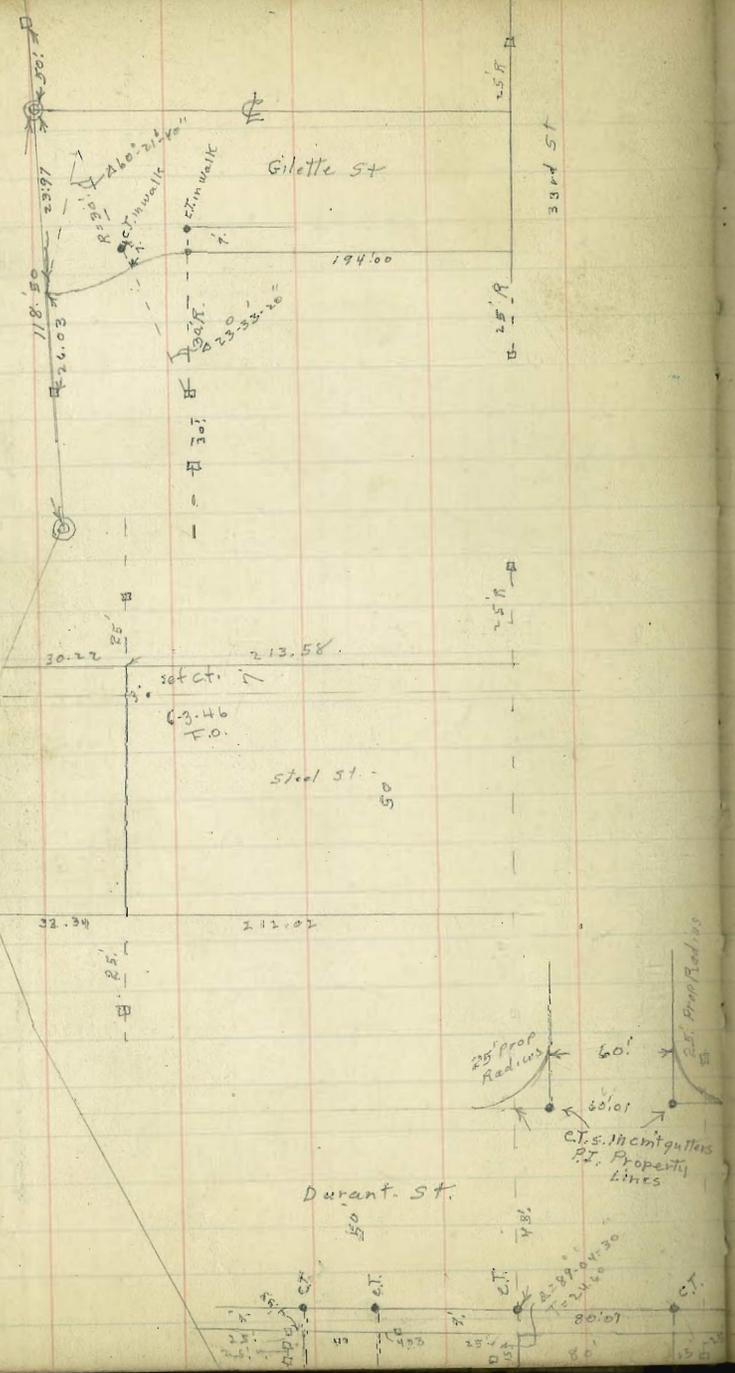
 3
 (4)
 88.6
 7.9
 7.9
 +5.0

 4
 (6)
 124.2
 7.5
 7.5
 +6.0

 5
 (6)
 122.7
 7.6
 1.4
 +8.2

 6
 (4)
 83.5
 13.0
 8.1
 +4.9

Based on Tie Point Sheet 150
6-24-32. L.B.H.



Gillette St Grades
+4-

	40' 0' 48' 5'	48' 5'	48' 5'	48' 5'	48' 5'	P.C. S.	P.R.C.	End.
S	21.4	21.5	21.7	21.8	22.0	22.04	22.1	22.1
	4.8	5.1	4.9	4.8	4.6	4.0	4.1	4.1
	20.9	20.7	20.4	20.4	20.3	20.4	20.3	20.3
	21.4	21.5	21.7	21.8	22.0		22.2	22.2
	5.2	5.1	4.9	4.8	4.6		4.4	4.4
	4.0	4.2	3.8	3.9	4.1		4.1	4.1
	24.75	24.7	24.7	24.7	24.7		24.7	24.7

Steel St +4-

S	20.4	20.5	20.7	21.1	22.0	23.5	24.1	24.1
	4.2	4.1	5.9	3.5	4.6	3.1	2.5	2.5
	5.7	5.6	5.9	6.0	4.8	4.4	4.6	4.6
	+0.5	+0.5	0.0	-0.5	-0.2	+1.4	0.4	0.4
N	20.6	20.7	20.9	21.3	22.4	24.0	24.1	24.1
	4.0	5.4	5.3	5.3	4.2	2.0	2.0	2.0
	5.4	5.4	5.4	5.5	3.1	4.0	4.3	4.3
	+0.6	+0.5	+0.3	0.2	+1.1	+3.0	3.5	3.5

Durant.

	P.C.	P.S.	Payne	P.C.	P.R.C.	End.
S	19.4	19.6	19.8	19.8	19.9	19.9
	5.3	5.1	4.9	4.9	4.8	4.8
	5.6	5.7	5.2	5.2	1.2	1.2
	-0.3	-0.6	-0.4	-0.4	+3.6	+3.6
N	19.6	19.8	20.0	20.2	20.2	20.2
	5.1	4.9	4.7	4.5	4.5	4.5
	4.6	4.6	4.7	1.8	4.3	4.3
	+0.5	+0.3	0	+3.5	3.5	3.5

Gillette s/a stakes

27.62	S	21.40	21.55	21.70	21.85	22.00	22.04	22.10	22.15	22.20
20.77		6.2	6.07	5.92	5.77	5.62	5.47	5.32	5.17	5.02
4.88										
25.65										

Steel St s/a stakes

	B	A	B	B	B	B	End		
N	20.60	20.75	20.90	21.04	21.24	21.74	22.38	23.13	24.03
	5.05	4.90	4.75	4.61	4.31	3.82	3.27	2.52	1.77

S	20.40	20.55	20.70	20.83	21.10	21.51	22.05	22.72	23.54
	5.15	5.10	4.95	4.82	4.65	4.14	3.66	2.93	2.11
									1.81
									71.60

Durant St s/a stakes

N	19.60	19.70	19.80	20.00	20.20		
	6.05	5.95	5.85	5.65	5.45		
					8.43		
					+2.00		
S	19.40	19.50	19.60	19.80	19.90		
	6.25	6.15	6.05	5.85	5.75		
					5.75		
					+0.50		

25.65

S.W. Ret Steel

W	20.40	20.35	20.30	20.25	20.20	19.90
	5.25	5.30	5.35	5.40	5.45	5.75

S.E. Ret Steel

E	20.40	20.35	20.30	20.25	20.20	19.90
	5.25	5.30	5.35	5.40	5.45	5.75

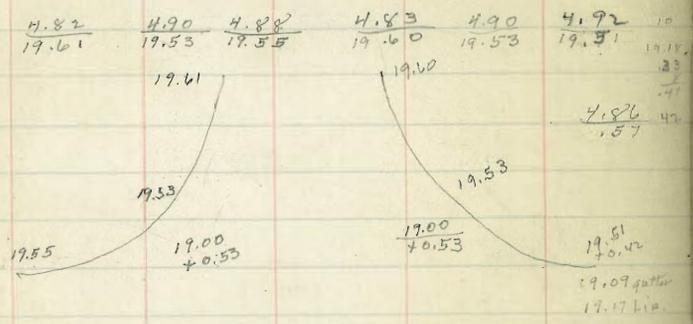
N.W. Ret Durant

W	19.65	19.62	19.60	19.60	19.60	19.40	19.33	19.26	19.20
	6.00	6.03	6.05	6.05	6.05	6.25	6.32	6.39	6.45

N.E. Ret Durant

E	19.65	19.62	19.60	19.60	19.60	19.40	19.33	19.26	19.20
	6.00	6.03	6.05	6.05	6.05	6.25	6.32	6.39	6.45

20.77
3.66
24.43



Durant

19.65
21.90
7.22
31.02

35.50
11.16
34.24
44.68

110.02
64.64
41.34

s/c

sw. Ret Imperial

43

28.95	28.70	28.55	28.34	28.12	27.86	27.58	27.27	26.97
2.95	2.25	2.47	2.68	2.90	3.16	3.44	3.75	4.05
		-0.50	-0.50	-0.50	-0.50	-0.50		

S.E. Ret Imperial

27.05	27.11	27.15	27.11	27.05	26.95	26.85	26.68	26.43
3.97	3.91	3.87	3.91	3.97	4.07	4.17	4.34	4.59

21.97
7.05
31.02

22.65
8.38
31.03

Sewer Grades

BIK A

B.M.	4.55	26.53	21.98	sw. 25' Rad Hub 33rd St
D.F. E. Line 33rd			4.72	21.83 15.66
M.H. 1			5.35	21.18 15.52
1			4.63	21.90 15.85
2			4.55	21.98 16.19
3			4.76	21.77 16.52
4			4.42	21.71 16.85
5			4.76	21.77 17.19
6 = DE			1.86	24.67 17.52

62.84.75
47.46

BIK C

B.M.	3.98	24.75	20.77
D.F. E. Line 33rd			4.00 20.75 14.57
M.H. 2			4.26 20.49 14.44
1			4.09 20.66 14.77
2			4.24 20.51 15.11
3			4.24 20.51 15.44
4			4.54 20.21 15.78
5 = DE			2.39 22.36 16.12

5
R 40.0
48.0

34.3 288.5 15

24.75

44

36.4 W	208.8	11.88	12.87
26.85	10.70	11.33	
15.52	7.5	10.70	
71.33	11.45	.63	
5.66	0.8		
+5.67	11.53		
5.85	10.00		
11.00	10.06		
16.19	9.6		
10.66	7.75		
16.52	4.33		
10.53	9.39		
17.60	12.30		
12.30	5.30		
1018	1.0052	285	
	5.300	209	
	5.090	494	
	2100		
	2036		
	64		
	288.5	209	
	52	52	
	5770	418	
	14425	1045	
	150020	10868	
		12.30	
		11.50	
		13.80	
		1.09	
		14.89	
		2.72	
		17.61	
20.77			
3.50			
24.27			
14.044	9.83		
8.83	9.21		
3.97	.62		
6.06			
10.18			
4.94			
5.24			
52			
1048			
2620			
27248			

FL 12.45 sewer MH
12.30 & Webster

FL 17.60 M.H. of Imp

54.0
54.8
100
208.8

33rd 51 Water Grades

26.85

BA. 25 Rad Hub	4.87	21.98	s.w. 33rd Gillette	
P.C. S. of Imp	1.5	25.3	23.0	+2.3
o + 69 B	4.0	22.8	20.0	+2.8
1 + 09 B S. 4	5.1	21.7	18.8	+2.9
1 + 54.4 N. line Gillette	5.2	21.6	18.2	+3.4
+ 1 in Gillette	5.8	21.0	18.0	+3.0
P.C. S. of Gillette	5.9	21.0	17.9	+3.1
o + 54.5	6.4	20.4	17.6	+2.8
1 + 09 P.C. N. of Steel	6.7	20.1	17.3	+2.8
+ 1 in Steel	6.6	20.2	17.0	+3.2
P.C. S. of Steel	8.4	19.7	16.9	+2.8
+ 54.5	8.7	19.4	16.6	+2.8
1 + 09 P.C. N. of Durant	9.1	19.0	16.3	+2.7
+ 1 in Durant	8.8	19.3	16.1	+3.2
+ 15 @ S. line Durant	8.8	19.3	16.0	+3.3
+ 69 Connection L. Main				

Gillette Water Grades

26.85

P.C. S. of 33rd	5.3	21.5	18.0	+3.5
+ 1 in 33rd	5.8	21.0	18.0	+3.0
@ N. line 33rd	5.5	21.3	18.0	+3.3
o + 53	5.5	21.3	18.1	+3.2
1 + 06	5.5	21.3	18.3	+3.0
1 + 59	5.6	21.2	18.4	+2.8
2 + 12	5.2	21.6	18.6	+3.0
2 + 65 End	4.8	22.0	18.7	+3.3

20.77
6.08
26.85

F.H. 52.33rd Steel

20.25
6.60
5.90
+0.70

45

57264 238
53 83

Steel St Water Grades

BM SW. 25' Rad.

26.85

P.C. E. of 33 rd St		6.5	20.3	17.0	+3.3
+ 1 st 33 rd St	28.07	6.6	20.2	17.0	+3.2
⊕ W. line 33 rd St		7.8	20.3	17.0	+3.3
0+58.5		7.5	20.6	17.2	+3.4
1+17 P.C. B.		7.5	20.6	17.4	+3.2
1+57 B		7.4	20.7	17.7	+3.0
1+97 B		6.2	21.9	18.7	+3.2
2+37 End		3.7	24.4	20.2	+4.2

Durant Water Grades

BM SW. 25' Rad

7.30

28.07

20.77

33rd + Steel

P.C. E. of 33 rd St		8.9	19.2	16.1	+3.1
+ 1 st 33 rd St		8.8	19.3	16.1	+3.2
⊕ W. line 33 rd St		8.7	19.4	16.1	+3.3
+45		9.2	18.9	16.2	+2.7
+90 = T. in Payne		9.2	18.9	16.3	+2.6
1+57 = End		8.2	19.9	16.6	+3.3

33rd St Gutter Grades
Durant - South.

20.77
2.62
23.39

E. c. S. of Durant 0+00 0+54.5 N. line Weber S. line Webster 0+50

W	18.7 4.7 3.9 <u>+0.8</u> (4.3)	18.4 5.0 4.3 <u>+0.7</u> (4.7)	18.1 5.3 4.2 <u>+0.7</u> (4.8)	17.9 5.6 4.5 <u>+1.1</u> (5.0)	17.5 5.9 4.9 <u>+1.0</u> (5.4)
E	18.7 4.7 3.7 <u>+1.0</u> (3.9)	18.4 5.0 3.7 <u>+1.3</u> (4.6)	18.1 5.3 4.3 <u>+1.0</u> (4.6)	17.9 5.6 4.3 <u>+1.3</u> (4.7)	17.5 5.9 4.6 <u>+1.3</u> (5.1)

1+00 1+50 2+00 2+50 3+00

W	17.3 6.1 5.0 <u>+1.1</u> (5.7)	17.1 6.3 5.5 <u>+0.8</u> (5.7)	16.9 6.6 5.5 <u>+1.1</u> (6.0)	16.6 6.9 5.9 <u>+0.9</u> (6.1)	16.4 7.0 5.8 <u>+1.2</u> (6.3)
E	17.3 6.1 4.8 <u>+1.3</u> 5.4	17.1 6.3 5.0 <u>+1.3</u> (5.6)	16.9 6.6 5.2 <u>+1.4</u> (5.8)	16.6 6.8 5.7 <u>+1.1</u> (6.0)	16.4 7.0 5.9 <u>+1.2</u> (6.3)

3+50 4+00 4+55

W	16.2 7.2 5.9 <u>+1.3</u> (6.8)	16.0 7.4 6.6 <u>+0.8</u> (7.1)	15.7 7.7 7.3 <u>+0.6</u> (7.3)	—	—
E	16.2 7.2 6.0 <u>+1.2</u> (6.6)	16.0 7.4 6.5 <u>+0.9</u> (7.1)	15.7 7.7 7.1 <u>+0.6</u> (7.7)	—	—

Allys BIKs 71-78-98-106-127 City HTS 2-2-31

Water Grades. BIK 71

48

BM.BP	7.83	354.92	347.09	N.W. Marlborough & Wightman		
connection in Wightman				346.65	4.1	4.2
oo: Shine Wightman		5.3	49.6	346.63	+3.0 [✓]	$\begin{matrix} 2.15 \\ 1.75 \\ \hline 4.90 \end{matrix}$ +3.4
0+50		4.9	50.0	46.0	+4.0 [✓]	$\begin{matrix} 1.75 \\ 1.75 \\ \hline 3.50 \end{matrix}$ +4.5
1+00		5.3	49.6	45.4	+4.2 [✓]	$\begin{matrix} 2.15 \\ 2.55 \\ \hline 4.70 \end{matrix}$ +3.8
+50		5.7	49.2	44.8	+4.4 [✓]	$\begin{matrix} 2.6 \\ 2.7 \\ \hline 5.3 \end{matrix}$ +4.1
2+00		6.9	48.0	44.2	+3.8 [✓]	$\begin{matrix} 3.4 \\ 3.8 \\ \hline 7.2 \end{matrix}$ 3.8
+50		8.2	46.7	43.6	+3.1 [✓]	$\begin{matrix} 5.1 \\ 4.1 \\ \hline 9.2 \end{matrix}$ +3.5
3+00 T.P.	2.05	48.14	8.81	46.09	43.1	+3.0 [✓]
+50		2.4	45.7	42.5	+3.2 [✓]	$\begin{matrix} 6.1 \\ 6.3 \\ \hline 12.4 \end{matrix}$ +3.0
4+00		3.0	45.1	42.0	+3.1 [✓]	$\begin{matrix} 6.7 \\ 6.5 \\ \hline 13.2 \end{matrix}$ +3.3
+50		3.3	44.8	41.4	+3.4 [✓]	$\begin{matrix} 7.0 \\ 6.1 \\ \hline 13.1 \end{matrix}$ +3.7
5+00		3.8	44.3	40.9	+3.4 [✓]	$\begin{matrix} 7.5 \\ 7.3 \\ \hline 14.8 \end{matrix}$ +3.6
+50		4.3	43.8	40.3	+3.5 [✓]	$\begin{matrix} 8.0 \\ 8.3 \\ \hline 16.3 \end{matrix}$ +3.3

N. line hand's
4+00 connection

339.83

chk B.M.
St line hand's T.P. 2.26
oo: connection
BIK 78

5.77 342.37
7.53 340.61
339.53

N.W. 42nd

hand's

339.53

0+52		1.3	341.6	38.8	+2.8 [✓]
1+04		2.3	40.6	38.0	+2.6 [✓]
+56		2.0	40.9	37.3	+3.6 [✓]
2+08		2.9	40.0	36.6	+3.4 [✓]
+60		3.5	39.4	36.0	+3.4 [✓]
3+12		4.4	38.5	35.3	+3.2 [✓]
+64		4.9	38.0	34.6	+3.4 [✓]
4+16		5.9	37.0	33.9	+3.1 [✓]
+68		6.3	36.6	33.2	+3.4 [✓]
5+20 BIK		7.0	35.9	32.53	+3.4 [✓]

342.87

5+60 M. line Dwight		7.6	35.3	31.3	+4.0 ✓
6+00 ⊕		9.6	33.3	330.13	+3.2 ✓
T.P.	335.28	10.35	332.52		
50S=6X8 ⊕		2.9	32.4	329.63	+2.8 ✓
Fire Hydt.					
S. line Dwight					
0+00 ⊕		2.2	33.1	329.33	+3.8 ✓
0+40 Brk		1.8	33.5	330.33	+3.2 ✓
0+80 Brk		2.4	32.9	330.13	+2.8 ✓
1+40		3.1	32.2	28.6	+3.6 ✓
2+00		4.4	30.9	27.2	+3.7 ✓
2+60		6.4	28.9	25.8	+3.1 ✓
3+20		7.7	27.6	24.4	+3.2 ✓
3+80		8.7	26.6	23.0	+3.6 ✓
4+40 B		10.7	24.6	321.53	+3.1 ✓
4+80 B	322.86	11.6	23.7	320.13	+3.6 ✓
5+20 B		1.3	21.5	318.03	+3.5 ✓
5+60 N. line Myrtle		4.0	18.9	315.4	+3.5 ✓
6+00		6.4	316.4	312.93	+3.5 ✓
Fire Hydt.	322.76				
B.M.	1.14	7.19	315.57	315.40	+0.17 curb grade
S. line Myrtle				N.W. Myrtle	
0+00	322.76		321.62	+42.00	
0+40 Brk		6.2	16.6	311.93	+4.7 ✓
0+80 Brk		4.5	18.3	313.63	+4.7 ✓
1+30 Brk		4.9	17.9	313.63	+4.3 ✓
1+80 Brk		6.7	16.1	311.73	+4.4 ✓
T.P.	0.64	9.6	13.2	307.33	+5.9 ✓
2+35	310.15	13.25	309.51		
2+90 Brk		4.7	305.4	99.5	+5.9 ✓
				291.73	

332.52
6.10
338.62
334.71
3.91

49

321.62
1.24
322.86
0.20
322.66
12.62
335.28

2.75 CHK T.P. opp page.
332.53 = 332.52

15.1
5.5
7.5
7.5
4.3
9.7
5.800

11915.6
1.41
5.5
7.05
7.5
7.75
92.7
99.4

310.15

285.12
 0.11
 285.01
 11.73
 296.74
 0.90
 295.84
 8.35
 304.19

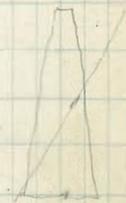
300.95
 3.24
 301.92
 2.37

297.3
 6.9

10.6
 93.6

310.15

8.3



2+90 Brk		12.1	98.0	291.73	+6.3✓
7P	0.27	13.14	297.01		
3+50 Brk T.P.	1.03	13.19	284.09	283.0	+1.1✓
		4.44	280.68	F.L. 283.0	-2.32✓
3+66 Pier		4.44	280.68	Bottom 279.0	+1.48✓
		4.80	280.32	F.L. 283.0	-2.68✓
3+82 Pier		4.80	280.32	279.0	+1.32✓
4+16		2.6	282.5	283.0	-0.5✓
4+50 Brk		3.8	81.3	283.0	-1.7✓
	297.28				
4+85		12.8	84.5	286.1	-1.6✓
5+20 Brk		3.7	93.6	289.33	+4.3✓
	310.15				
5+60		9.1	301.0	293.3	+7.7✓
4 line Thru					
6+00 ⊕ T.P.		9.20	300.95	297.2	+3.7✓
	304.19				
50 S. +		4.0	300.2	297.3	+2.9✓
Fire Hydt.		4.69	299.50	299.90	-0.50
5 line Thru					
0+00 ⊕		5.7	98.5	297.33	+1.2✓
				FL 297.40	-6.17✓
0+20 Pier.		12.96	91.23	B.M. 291.00	+0.3 lowered 2.0
				FL 97.44	-7.21✓
0+33 Pier.		14.00	90.19	90.00	+0.19✓ " 2.0
				FL 97.48	-5.87✓
0+46 Pier.		12.58	91.61	91.00	+0.61✓ " 1.0
				FL 97.52	-5.04✓
0+59 Pier		11.71	92.48	93.00	-0.52✓ OK
				FL 97.56	-2.74✓
0+72 Pier		9.37	94.82	94.00	+0.82✓ " 1.0
				FL 97.60	-1.71✓
0+85 Pier Entry		8.30	95.89	94.00	+1.89✓ Entry Pier
1+32.5		4.4	99.8	97.76	+2.1✓
1+80 Brk.		2.6	301.6	297.93	+3.7✓
2+20		2.9	301.3	297.73	+3.6✓
2+60 Brk.		3.4	300.8	297.53	+3.3✓
3+10		4.2	300.0	96.7	+3.3✓
	T.P. 1.47	3.95	300.24		
3+60 Brk		2.2	99.5	295.93	+3.6✓
4+00 Brk				294.83	

Ground of Pipe 298.6

11.5
Ground 92.7 at Pipe

11.00
Ground 93.2 at Pipe

9.3
Ground 94.9 at Pipe

8.6
Ground 95.6 at Pipe

301.71

4+00 Brk	3.1	98.6	294.83	+3.8 ✓✓
4+50	4.7	97.0	93.1	+3.9 ✓✓
5+00 Brk	6.3	95.4	291.43	+4.0 ✓
5+40 Brk	7.9	93.8	289.13	+4.7 ✓
N. line Redwood	10.7	91.0	283.33	+7.7 ✓
6+00 Brk	12.65	89.06	288.4	+0.66 ✓
Fire Hydt.	13.2	88.5	283.25	+5.3 ✓
14' South. connection				

888
213
11.01
6.90
4.11

51

Fire Hydt S.W. Main + Woden

10.46 B.M. N.W. Main + Woden	S. line Main W. cl. Woden	6.41
5.53		9.58
15.99	W " Woden S. edge Pavmt	4.32
	W " " 8' N.E. " "	9.67
		6.03
		9.76
	10' d. H. W. Main + Woden cl. Grade	10.09
		5.90
		4.85
		11.05

Fire Hydt S.E. Main + Yama 4 ± 10' E of E Yama

10.46 B.M. N.W. Main + Woden	E. line Yama S. edge Pavmt	4.30
2.23		5.78
12.69	C " " 8' N.E. " "	4.24
5.79	E " " cl. Grade	5.64
6.90 B.M. SpK loc Pole 3999 S.W. (Yama + Main)		6.00
4.12		
11.02	10' E of E " " " "	6.05
CH 2.13		4.23
8.89-8.88		6.11
B.M. B.P.K.H. Main + Division		-1.88
6.90		
3.38		
10.28		

8.00 Division

6.00
4
415 12.00
1060
3400

Alley BIK 22 Teralta
Grades

363.58 B.M. S.M. & Casin + Van Dyke

	v.	e.	e.
00. S. line & Cap	363.58 4.46	363.58 4.46 368.04	363.15 4.89 368.04
+7.8 B.	363.50 4.54 4.02 +0.52		363.40 4.64 2.64 +2.00
0+42.8	363.62 4.42 3.62 +0.80		363.50 4.54 2.54
0+77.4	363.75 4.29 3.69 +0.60		363.60 4.44 3.94 +0.55
1+12.8	363.87 4.17 4.70 -0.53		363.70 4.34 3.34 +1.00
1+47.8 B	364.00 4.04 4.15 -0.14		363.80 4.24 4.51 -0.27
1+57 End	364.05 3.99 3.87 +0.12		363.89 4.15 3.88 +0.27
sewer hat #		358.80 9.24 4.09 +5.15	

4.40
3.5
7.8
2.5
42.4
77.4
35.
112.8
147.8
9.2
157.0

7.8
1.40
4.7
57.0
46.5
7.2

17
14
13.6
5
10.6

6.35
6.55
0.69
0.70

52

Water Grades Main -
Fire Hydt S.E. Main + Thor

13.46 B.M. S.E. Main + Una
3.21
16.67
7.62
7.05 B.M. B.P. S.E. Main + Thor
6.16
13.21

S. line Main e. el. Thor 6.14
7.07
E. line Thor S. Edge Pavmt. 6.06 7.15
7.18 6.90
E. " " S. N. of s. edge " 5.75
7.46

15.13
4
14.83

7.59
5.62
4.90
+0.70

Fire Hydt S.E. Main + Vesta

15.52 B.M. N.W. Main + Vesta
3.96
19.48

S. line Main - e. el. Vesta 4.40
15.08
E. " Vesta s. edge Pavmt 4.35
15.13
E. " " S.W. s. edge " 4.06
15.42
10. e. E. line Vesta e. grade 15.25
4.23
3.53
0.70

Fire Hydt S.E. Main + Woden

10.46 B.M. N.W. Main + Woden
3.69
14.15

S. line Main e. el. Woden 5.09
9.06
E. " Woden s. edge Pavmt. 5.00
9.15
E. " " S.W. " " 4.64
9.47
10. e. E. line Woden e. grade 9.30
4.85
3.77
+1.08

See Page 51

Alley BIK 29. La Jolla Park 3-6-31
Grades. mlla

3.01
117.60
10.44
1.16
E

53

				N.W. Fay + Silverado
BM.BP	9.71	109.23	99.52	3+80
T.P.	5.63	114.41 W	0.45 E	108.78 2
S. db... Line Silverado	108.96 5.45	109.10 5.31	109.35 5.06 5.14	4+20
oo=S. Line Silverado	109.60 4.81 4.56 +0.25	109.30	109.60 4.81 3.81 +1.00	4+60
0+32.5	114.41 3.94 110.47 4.85 115.32	9.73 4.68 3.26 +1.42	9.74 4.67 3.67 +1.00	5+00 N line R line
0+65	9.86 4.55 3.55 +1.00	9.88 4.53 4.43 +1.10		
0+97.5	9.99 4.42 3.42 +1.00	10.02 4.89 4.17 +0.22		
1+30	10.12 4.29 4.32 -0.03	10.17 4.24 3.85 +0.39		
1+62.5	10.25 4.16 4.12 +0.04	10.31 4.70 7.00 +0.10		
1+95	10.38 4.94 4.80 +0.14	10.45 3.96 3.26 +0.70		
2+27.5	10.51 4.81 3.81 +1.00	10.59 4.73 4.93 -0.20		
2+60 Brk	110.64 4.68 4.82 -0.14	110.44 110.74 4.52 4.07 +0.51		
3+00 Brk	110.78 4.54 4.40 -0.06	110.58 110.90 4.42 3.80 +0.62		
3+40 Brk	110.68 4.64 5.11 -0.47	110.80 4.52 2.52 +2.00		

	W	E
3+80	115.32 4.52 110.78 3.50 114.28 4.22	10.56 4.76 5.20 -0.44 10.44 4.88 3.69 +7.19
4+20	108.06 2.32 110.38 4.37 104.01	10.44 4.88 3.69 +7.19
4+60	104.01	10.32 3.96 4.32 -0.36
5+00 N line R line	110.20 4.09	110.00 110.40 3.88

Header chK 3-24-31

110.60 3.64 114.24 3.46 110.78 3.84 114.62	W	109.60 4.64	9.73 4.51	9.86 4.38	9.99 4.25	10.12 4.12	10.25 3.99 3.35 +0.04	10.38 3.86	10.51 3.23
114.62	E	109.60	9.74 4.50	9.88 4.36	10.02 4.22	10.17 4.07	10.31 3.23	10.45 3.79	10.59 3.53
	W	B	B	B					
	10.64 3.60	10.78 3.84	10.64 3.94	10.56 4.05	10.44 4.18	10.32 4.30	10.20 4.42		
	E	10.74 3.88	10.90 3.72	10.80 3.82	10.70 3.94	10.60 4.02	10.50 4.12	10.40 4.22	

Monte Vista + Olivitas
Paving, Water, Sewer etc

4-11-31
mill

47.32 BM. NW. 1st St. + Arenas + Monte Vista
70.51 BM. NE. St. Sea View + La Jolla Blvd. gate
67.74 BM. NW. 1st St. + Arenas + La Jolla Blvd.
46.04 BM. NE. St. " + Monte Vista

5.31

47.22

6.148
46.04

54

Monte Vista Sewer Cons.

#					
00 = P.D. M.H. 1	52.52	5.34	47.18	44.13	+ 3.05
07 31.16 N. Line Arenas		6.60	45.92	42.13	+ 5.05
07 31.16 S. " "		6.12	45.90	41.91	+ 4.01
1+22 ^{3y} Connection		6.22	46.30	41.56	+ 4.34
				41.27	+ 5.03

BM. 67.74

0.32

68.06

11.29

BM. Nails in Pole 56.775 w. + Arenas

3.39

60.16

12.62

47.54

4.98

52.52

Olivitas Sewer Cons.

M.H. 1 & Olivitas	64.91	6.98	57.93	52.80	+ 5.13
-------------------	-------	------	-------	-------	--------

Sewer Laterals

#	#	#	#	#
1	2	3	4	5
63.81	63.81	64.91	63.81	63.81
52.50	53.67	55.20	53.10	52.70
10.31	10.14	9.71	10.71	11.11
2.79	6.04	5.80	5.49	4.63
+ 7.52	+ 4.19	+ 3.91	+ 5.22	+ 6.48
#	#			
6	7			
52.52	52.52			
44.70	42.70			
7.82	7.82			
1.68	6.48			
+ 6.14	+ 3.34			

45.00 46.00

7.52 6.52

7.29

5.7

8.36

44.16

Monte Vista Water Main Cons.

52.52

55

00 = Connection S. Line & Sealand	1.95	50.57	47.00	
0+60	2.2	50.3	46.8	+3.5
1+20	2.3	50.2	46.6	+3.6
1+80	2.5	50.0	46.4	+3.6
2+40	2.7	49.8	46.2	+3.6
3+00	2.9	49.6	46.0	+3.6
3+60 B	3.7	48.8	45.9	+2.9
3+80 B	3.9	48.6	45.5	+3.1
4+15	4.8	47.7	44.1	+3.6
4+50 B { slow N. Line - Archas	6.2	46.3	42.6	+3.7
+	4.9	45.6	42.3	+3.3
5+12 End. { 2' S. Line - Archas	6.6	45.9	42.2	+3.7

E. gutter
Grades
50.0
3.0

49.67

48.90
3.9
48.50
3.5
45.5

48.60

48.35

45.75
3.7
45.7

45.35
3.0
42.3

45.57

45.17

64.91
4.84
60.07
0.96
61.03

⊕ gutter s. ch.

Sealand Water Grades
61.03

E. Line Obvitas To N	00	61.0	57.5	+3.5	60.67	<u>60.55</u> 3 57.5	<u>61.05</u> +0.02
⊕ +29 in "	0.5	60.5	56.9	+3.6			
+54		60.0					
00 = W Line "	1.0	60.0	56.5	+3.5	59.3	<u>59.5</u> 3.1 56.5	<u>60.00</u> 11.03
0+50	3.3	57.7	54.2	+3.5			
1+00	5.6	55.4	52.0	+3.4			
1+66 ⁵⁰ Connection ⊕	8.53	52.50 <u>3.50</u> 49.00	49.0				

Olivitas Water Grades.

						± Grades	E. Gutter Grades.	C. ch Grades.
BM Nails Pol.	8.14	64.91	56.77	Arenas SW. Olivitas				
007 S. line Sealane		4.50	60.41	56.9	+3.5	59.9	59.9	60.50
0258		4.6	60.3	56.7	+3.6		$\frac{31}{56.7}$	4.41
1416		4.8	60.1	56.5	+3.6			
1474		5.5	59.4	56.4	+3.0			
2+32		5.1	59.8	56.2	+3.6			
2+90 Brk		5.2	59.7	56.1	+3.6	59.1	59.2	59.78
3+40 Brk		5.8	59.1	55.7	+3.4	$\frac{3}{56.1}$ 58.72	58.75	59.25
4+00		6.9	58.0	54.3	+3.7	$\frac{3.8}{55.7}$		$\frac{5.66}{5.8}$
Brk BM.	7.04	63.81	56.77					
4+60 N. line Arenas		7.2	56.6	53.0	+3.6 ✓	56.15	56.15	56.75
+		7.8	56.0	53.1	+2.9 ✓	$\frac{3.0}{53.1}$		$\frac{7.25}{7.25} 0.14 \text{ low}$
007 S. line Arenas		7.1	56.7	53.1	+3.6 ✓			
0+50		6.3	57.5	53.8	+3.7 ✓	56.2	56.25	56.75
1+00		5.5	58.3	54.6	+3.7 ✓			$\frac{7.06}{7.06}$
1+50		4.7	59.1	55.3	+3.8 ✓			
2+00		4.0	59.8	56.1	+3.7 ✓			
2+50		3.1	60.7	56.8	+3.9 ✓			
3+00		2.5	61.3	57.6	+3.7 ✓			
3+25 Φ45 Plug		2.6	61.2	58.0	+3.2 ✓	61.05	61.1	
3+36 cl.						$\frac{3}{58}$		$\frac{62.0}{7.81}$

5.

Sea Lake 725

50.00	49.25	49.67	50.00	50.50
49.42	49.80	50.00	50.00	49.97

46.14	7.34	2.29	2.34	2.37
53.35	7.38	7.39		

45.45	45.40	44.25	44.37	44.45
7.90	7.95	7.10	7.98	8.79
6.02	5.14	5.66	5.26	5.33
47.33	48.21	47.69	48.09	48.02
48.85	3.78	2.95	3.48	3.55
49.80	49.57	50.40	49.87	49.80

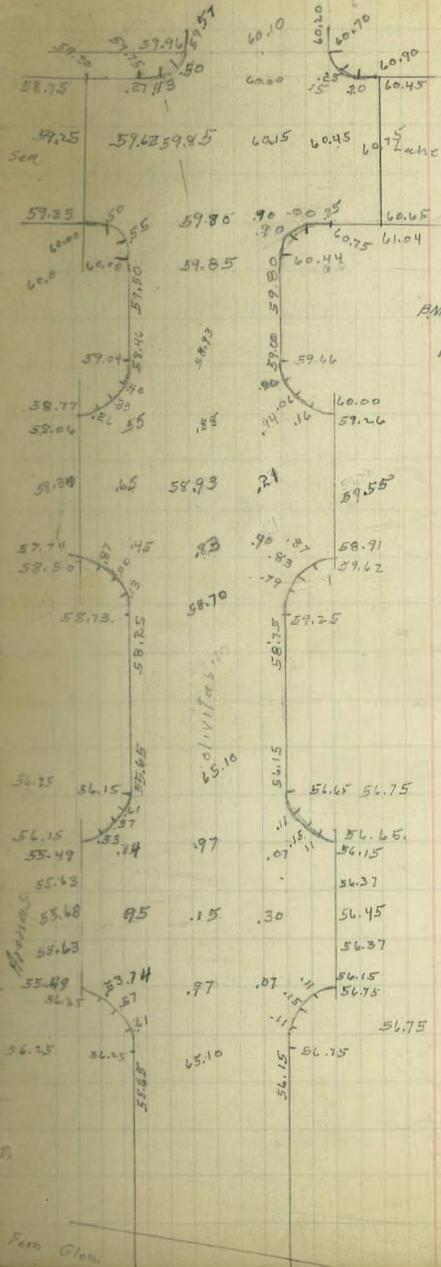
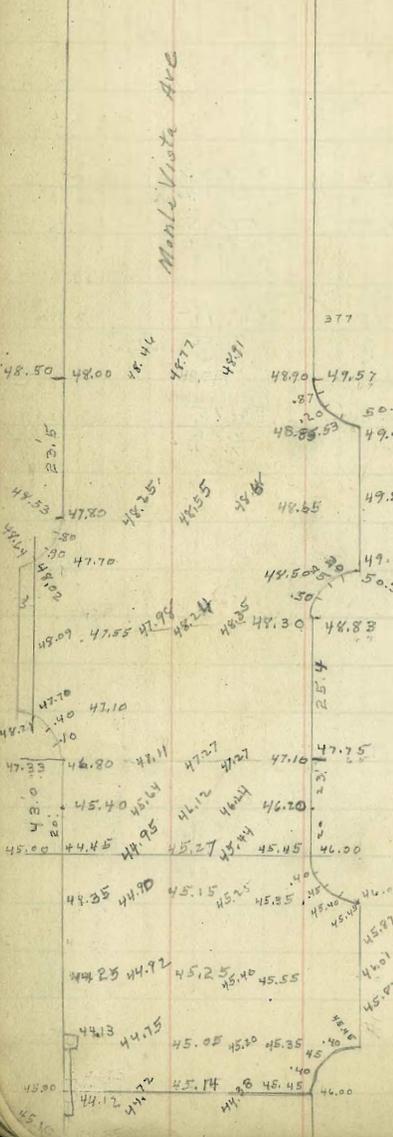
3.05	4.52	5.70	4.35	4.75	5.60
50.30	48.83	44	32	15	47.75

80	10	40	90	80	80	90	82	20	53
55	25	95	45	55	59	48	48	15	48

10	70	30	20	240
25	65	05	14	

20	85	50	30	10	5.95
15	50	85	05	25	5.75
					5.29

46.14				
4.96				
51.10	44.45	6.10	6.00	
	6.25	45.00	48.10	
		75	75	
		44.25	44.35	



60.00	4.25	3.94	3.65	3.80	
4.68	60.44	75.6	1.04	70	
64.69					
3.98	4.49	5.12	4.73	4.94	5.39
60.70	.20	59.57	59.96	59.75	51.30
4.24	4.04	5.24	5.94		
.45	60.65	59.35	7.75		
.75	2.7	4.3	5.0	5.7	25
.94	4.2	2.6	1.9	1.2	4.4
65	25	10	95	80	90
.04	.44	.59	1.74	.89	7.9
					.19
					1.14
					3.4
AM 56.77	5.79	5.79	5.27	5.27	15
52.6	56.24	56.24	56.76	56.75	78
62.03					
5.38	5.38	5.88	5.88		
56.65	56.65	56.15	56.15	56.15	56.15
.15	.11	.65	.61	.57	.53
.88	.72	.38	.42	.46	.50
					.54
2.78	2.41	3.12	2.72	2.03	
59.25	59.62	58.91	59.26	60.00	
2.37	2.19	3.24	3.92	4.29	
59.66	59.04	58.77	58.06	57.74	
3.53	3.30				
58.50	58.73				
.00	.00	.06	.16	.21	.91
.03	.03	.97	.87	.77	.12
					.76
					2.02
					.28
					.41
					.41
.25	.13	.90	.87	.74	.04
.78	.90	.03	.16	.17	.97
					.47
					.57
					.4

Fern Glen

Water Line Alley BIK. 21. Normal Hts.

7-24-31
Miles
Walker
Bliss
Season

85.2
5.0

385.78 BM. 55. Adams + Cherokee
4.43
390.21

58

	S. Line Grade	Water Grade 3.8 Below S.									
0+00: E. Line Cherokee	385.2	381.4		81.7	81.2	80.2	79.2	76.9	74.6	72.8	72.1
0+40 B.	385.5	381.7		81.5	81.0	80.0	79.0	76.7	74.4	72.6	72.1
0+80 EVC	385.0	381.2		81.0	80.5	79.5	78.5	76.2	73.9	72.1	72.1
1+17.5	384.0	380.2		80.5	80.0	79.0	78.0	75.7	73.4	71.6	71.6
1+55 B	383.0	379.2		80.0	79.5	78.5	77.5	75.2	72.9	71.1	71.1
1+97.5	380.7	376.9		79.5	79.0	78.0	77.0	74.7	72.4	70.6	70.6
2+40 RVC	378.4	374.6		79.0	78.5	77.5	76.5	74.2	71.9	70.1	70.1
2+80 B.	376.6	372.8		78.5	78.0	77.0	76.0	73.7	71.4	69.6	69.6
3+20 EVC	375.9	372.1		78.0	77.5	76.5	75.5	73.2	70.9	69.1	69.1
3+70	375.6	371.8		77.5	77.0	76.0	75.0	72.7	70.4	68.6	68.6
4+20	375.2	371.4		77.0	76.5	75.5	74.5	72.2	69.9	68.1	68.1
4+56 W. Line Mt View	374.8	371.0		76.5	76.0	75.0	74.0	71.7	69.4	67.6	67.6

Water Grades
Alley BIK 44 Normal Hts.

10-14-31
Miller
Walker
Bliss

59

E Line Cherokee	± Grades		Water Grades	N. of 385.82 7.65
0+40 B	382.9	3.3 B.M. 385.78 1.69	379.6 7.9 4.6 +3.3	
0+60 B	381.9	387.47 11.17 376.30 3.32	378.6 8.9 5.3 +3.4	
1+00		379.62	377.2 10.3 6.4 +3.9	
1+40 B	379.1		375.8 11.7 7.9 +3.8	
1+80 B	377.7		374.4 13.1 9.2 +3.9	
2+20 B	376.8		373.5 14.0 10.1 +3.9	
2+40 B	376.2		372.9 14.6 10.6 +4.0	
3+00			372.5 15.0 11.2 +3.8	
3+40			371.1 7.5 3.7 +3.8	
3+80			371.7 7.7 3.8 +4.1	
4+20 B	374.5		371.7 8.4 4.5 +3.9	
4+40 B	374.3		371.6 8.6 4.4 +4.2	
				373.85 5.77

41.7
145

00 = S. line Sampson	<u>75.60</u> 5.08 5.11	<u>75.60</u>	<u>75.95</u> 4.73 4.23	BM. 80.57 0.44 80.68 1.01 74.67 4.31
0+20 Brk	<u>76.40</u> 4.28 2.28 +2.00	<u>76.20</u>	<u>76.50</u> 4.18 3.53 +0.65	78.98 5.45 73.53 3.82 77.35
0+40 Brk	<u>76.60</u> 4.08 3.08 +1.00	<u>76.30</u>	<u>76.60</u> 4.08 3.24 +0.80	
0+80	<u>76.26</u> 4.42 3.27 +0.75	<u>76.26</u>	<u>76.26</u> 4.42 3.42 +9.00	
1+20	<u>75.92</u> 4.76 3.52 +1.24	<u>75.92</u>	<u>75.92</u> 4.76 3.76 +1.00	
1+60	<u>75.58</u> 5.10 4.10 +1.00	<u>75.58</u>	<u>75.58</u> 5.10 4.10 +1.00	
2+00	<u>75.24</u> 5.44 4.44 +1.00	<u>75.24</u>	<u>75.24</u> 5.44 4.44 +1.00	
2+40	<u>74.90</u> 4.08 3.08 +1.00	<u>74.90</u>	<u>74.90</u> 5.78 4.78 +1.00	
2+80	<u>74.56</u> 4.42 3.42 +1.00	<u>74.56</u>	<u>74.56</u> 4.42 4.22 +0.20	
3+20	<u>74.22</u> 4.76 5.11 -0.35	<u>74.22</u>	<u>74.22</u> 4.76 3.06 +1.70	
3+60	<u>73.88</u> 5.10 5.37 -0.27	<u>73.88</u>	<u>73.88</u> 5.10 4.10 +1.00	
4+00	<u>73.54</u> 3.81 2.71 +1.00	<u>73.54</u>	<u>73.54</u> 3.81 2.81 +1.00	
4+40 Brk,	<u>73.20</u> 4.15 3.65 +0.50	<u>72.9</u>	<u>73.20</u> 4.15 3.15 +1.00	

4+60 B.	<u>72.90</u> 4.45 3.45 +1.00	<u>72.6</u>	<u>72.90</u> 4.45 3.45 +1.00
4+80 B.	<u>72.55</u> 4.40 3.80 +1.00	<u>72.25</u>	<u>72.55</u> 4.80 3.80 +1.00
5+20	<u>71.70</u> 5.65 4.23 +1.42		<u>71.76</u> 5.39 4.59 +1.00
5+60	<u>70.85</u> 6.50 5.50		<u>70.98</u> 6.37 5.37

6400 N. Line Secard

	<u>70.00</u> 7.35 7.41	<u>69.8</u>	<u>70.2</u> 7.15 7.21
ct.	157.48	314.96	157.48
0+00 B	9.7	10.3 To Ret.	
0+20 B	9.7	10.3	
0+40 B	9.7	10.3	
0+80	9.5	10.3	
1+20	9.5	10.4	
1+40	9.6	10.4	
2+00	9.7	10.3	
2+40	10.0	10.0	
2+80	10.1	9.9	
3+20	10.1	9.9	
3+60	9.7	10.3	
4+00	10.0	10.0	
4+40 B	10.1	9.9	
4+60 B	9.8	9.9	
4+80 B	10.0	9.6	
5+20	10.	10.	
5+60	9.8	10.2	
ct.	157.45	314.90	157.45
6400	9.9 To Ret	10.1	10.5 To Ret

Wilbur Ave Water Grades

4-28-31
 38
 38
 38
 38

BM. S.E. of E.	366	189.72	186.06	2amont + Wilbur	
0+00 = E. Line Lamont. connection	3.8	185.9	183.2		
+50	2.9	186.8	182.7		+4.1
1+00	3.0	186.7	182.2		+4.5
+50	3.9	185.8	181.7		+4.1
2+00	5.1	184.6	181.3		+3.3
+50	5.8	183.9	180.8		+3.1
3+00 Brk	6.1	183.6	180.3		+3.3
3+40 Brk	6.0	183.7	179.8		+3.9
3+80 Brk	5.8	183.9	179.1		+4.8
4+20 Brk	6.2	183.5	178.3		+5.2
4+60 Brk	7.8	181.9	177.2		+4.7
5+00 E. End. of Plug	9.5	180.2	175.9		+4.3

15' wide

Alley BIK 44 Park Villas
Bet. 32nd & Bancroft.

	E		SW 52 nd Wrightman 8m.	W
00- <u>Line Wrightman</u>	<u>346.00</u> 4.54 4.55		<u>346.40</u> 4.14 350.54 2.25 348.29 5.77	<u>345.97</u> 4.57 4.57
0+10B	<u>346.35</u> 4.19 2.19 +2.09		<u>354.06</u> 4.67 349.39 4.70 354.09	<u>346.35</u> 4.19 3.62 +0.51
0+56	<u>46.96</u> 3.58 2.58 +1.00			<u>47.00</u> 3.54 2.32 +0.21
1+02	<u>47.57</u> 2.97 2.71 +0.26			<u>47.65</u> 2.99 2.75 +0.14
1+48	<u>48.18</u> 5.88 5.75 +0.13			<u>48.30</u> 2.24 2.24 0.0
1+94	<u>48.79</u> 5.27 3.02 +0.25 49.18	1+00		<u>48.95</u> 5.11 4.07 +1.04 49.36
2+40B.	<u>349.40</u> 4.86 4.98 +0.32	0+80		<u>349.60</u> 4.40 3.90 +0.56
2+60.B	<u>349.55</u> 4.51 5.44 -0.93	0+60		<u>349.75</u> 4.31 2.31 +2.00
2+80.B	<u>349.10</u> 4.96 4.66 +0.30	0+40		<u>349.30</u> 4.77 4.05 +0.74
3+00B.	<u>348.15</u> 5.91 6.09 -0.18	0+20		<u>348.35</u> 5.74 3.18 +2.56
3+20 B	<u>346.70</u> 7.36 6.44 +0.92	0+00		<u>347.00</u> 7.09 4.09 +3.00
3+24 ² S. Line Union	<u>346.20</u> 7.86			<u>346.85</u> 7.21

9 1/2
15
+6.07

63

Sewer Laterals

① 6" ② 4"

<u>341.23</u> 9.31 2.31 +7.00	<u>343.80</u> 10.26 4.24
--	--------------------------------

<u>349.40</u> -0.32 349.08 4.93 354.01
--

Grade change

S. Line Union

<u>346.85</u>	<u>349.60</u> +0.56 3.85 354.01
---------------	--

0+04.67 = 00

<u>346.20</u> 7.87
<u>346.55</u> 7.48 6.37 +1.07

0+05

<u>346.93</u> 7.09 4.09 +3.00
--

0+20

<u>347.47</u> 6.54 3.10 +3.44
--

<u>47.28</u> 6.73 6.06 +0.67

0+40

<u>348.28</u> 5.81 3.97 +1.84
--

<u>48.00</u> 6.07 4.60 +1.47

0+60B

<u>348.93</u> 5.08 2.12 +2.80
--

<u>348.73</u> 5.28 3.40 -0.12
--

0+70

<u>349.25</u> 4.76 3.66 +1.10
--

<u>349.03</u> 4.98 4.76 +0.22
--

0+80

<u>349.38</u> 4.63 5.85 +0.78
--

<u>349.18</u> 4.83 4.93 +0.10
--

0+90

<u>349.48</u> 4.53 4.66 +0.57
--

<u>349.28</u> 4.73 4.69 +0.04
--

1+00

<u>349.36</u> 4.65 4.33 +0.32
--

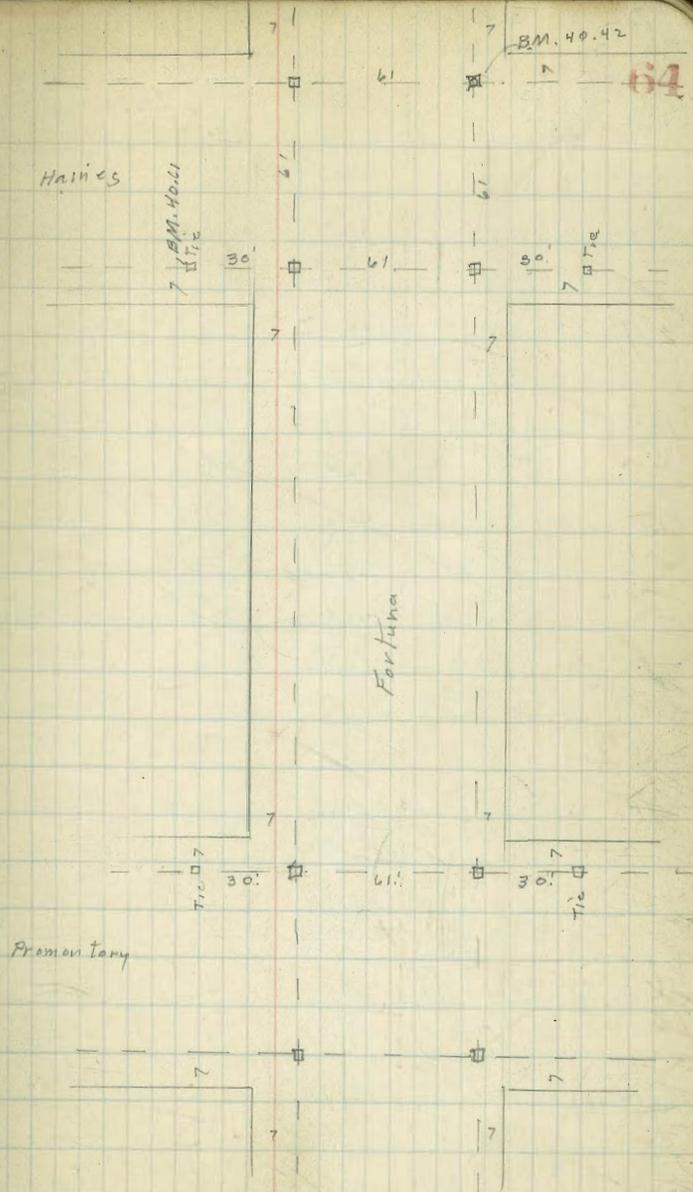
<u>349.18</u> 4.83 4.83

Fortuna bet. Haines & Promontory

M. L. Sommer
6-4-31

	S	BM. N.W. 7 Hub Fortuna & Haines	N
		40.42 8.34 48.76 8.15 40.61: BM.	
W. line Haines	38.0 10.8 10.7 +0.1	Tie Hub 30's. of S.E. 7. Hub. Haines & Fortuna	38.0 10.8 7.9 +2.9
E. line Haines	39.0 7.8 7.4 +2.4		39.5 7.3 5.0 +4.3
0+43	39.9 8.9 6.3 +2.6		40.3 8.5 4.9 +3.6
0+86	40.8 8.0 5.4 +2.6		41.1 7.7 5.2 +2.5
1+29	41.7 7.1 4.2 +2.9		41.9 6.9 5.2 +1.7
1+72	42.6 6.2 3.4 +2.8		42.7 6.1 5.5 +0.6
2+15: W. line Promontory	43.5 5.3 2.3 +3.0		43.5 5.3 4.7 +0.6

(Posted on Tie Point Sheet No. 1294)
L.S.H.
6-16-32



Alley BIK 82 Univ Hts
 Monroe to Meade bet Maryland New Jersey
 Grades

6-5-31
 Sullivan
 San. Marmey
 Osborn

342.05 S.W. Maryland Meade

65

	W.	E
0+00 = S. Line Monroe	339.65 6.51 6.53	339.80 6.36 6.37
0+50	40.52 5.64 3.64 +2.90	40.60 5.56 5.01 +0.55
1+00 B.	341.40 4.76 2.76 +2.00	341.40 4.76 4.26 +0.50
1+20 B	41.55 4.61 4.08 +0.53	41.55 4.61 3.94 +0.67
1+40 B	41.65 3.66 2.66 +1.00	336.86 0.35 336.51 8.20 345.31 5.13 342.18 3.92
1+60 B	41.55 3.76 3.32 +0.44	41.55 3.76 3.11 +0.65
1+80 B ↓ 40 ↓	41.40 3.91 2.91 +1.00	41.40 3.71 3.40 +0.51
2+20 B	40.80 4.51 4.98 -0.47	40.90 4.41 3.41 +1.00
2+40 B	40.35 4.96 5.60 -0.64	40.50 4.81 4.20 +0.61
2+50.7 S.I.		
2+60 B	39.60 5.71 5.87 -0.16	39.80 5.51 4.61 +0.90
2+80 B	38.70 6.41 7.01 -0.40	38.90 6.41 5.51 +0.90
3+20	36.60 8.71 8.46 +0.25	36.80 8.51 7.07 +1.44
3+60	34.50 2.36 2.36 0.00	34.70 2.11 1.81 +0.35

3+76 ³⁵ S. P.	4+00	32.40 4.46 4.46 0.00	32.60 4.26 2.26 +2.00
	4+26 ⁵² #	4.46 0.00	2.26 +2.00
	4+40	30.30 6.56 8.43 -1.87	30.50 6.36 4.09 +2.27
	4+80	28.20 3.48 4.15 -0.72	310.03 18.22 323.15 2.15 321.05 10.58
	5+20	26.10 5.58 5.86 -0.33	28.40 3.43 0.23 +3.00
	5+60 B	24.00 7.68 6.83 +0.80	26.30 5.33 2.88 +2.45
	5+80 Run W.	22.70 8.95 5.56 +1.37	324.20 7.43 4.43 +3.00
	5+90 B on W	21.70 9.93 7.59 +2.34	
	6+1.5 N. Line Meade.	320.10 8.05 8.06	20.51 2.64 2.64
			321.60 1.35 1.36

Sewer laterals

#	#	#	
1-6"	2-4"	3-4"	250.9
326.8	323.2	321.7	125.45
18.5	13.7	15.2	376.35
5.7	8.9	7.1	50.15
+12.8	+8.8	+8.1	426.50
2#50.9	125.45	50.18	

15' wide

Alley BIK 36 Teralta
El Cajon to Orange Bet 35th & Wilson
Grades.

Miller
S. J. Miller
Co. Berme.

66

	W	E	BM. S.W. Wilson & El Cajon	Water Grades	W	E		Water
00=S. Line El Cajon	380.79 2.92	380.54	380.64 3.07	380.08 4.54 384.62 5.50	4+20	78.09	77.97	388.78 75.0 8.8 5.0 +3.8
0+20 B	80.25 3.76 3.40 0.06H	80.15 3.50 3.52 0.04H	378.12 5.66 383.78	4+60	77.98	77.85	74.8 9.0 5.1 +3.9	
0+40 B	79.80 3.91 3.88 0.03H	79.65 4.06 4.01 0.05H	380.09 3.63 383.71 5.32	5+00	77.87	77.74	74.7 9.1 5.2 +3.9	
0+50			378.39 3.55 381.94	76.4 8.2 4.7 +3.5	5+40	77.76	77.62	74.6 9.2 5.2 +4.0
0+60 B	79.40 4.31 4.27 0.04H	79.25 4.46 4.40 0.02H						
0+80 B	79.20 4.51 4.51 0.K	79.00 4.71 4.44 0.07H			5+80 B 326 27 430	377.65 4.29 4.30	377.50 4.44 4.41	3.52 3.2 4.46 74.5 9.3 5.4 +3.9
1+00 B	79.00 4.71 4.73 0.02L	78.90 4.81 4.79 0.02H		75.9 8.7 5.4 +3.3	6+07 W. In Orange	377.40 4.54 4.50	377.19 4.75 4.80	377.38 4.54
1+40	78.88	78.79		75.8 8.8 5.2 +3.6				
1+80	78.77	78.67		75.7 8.9 5.7 +3.0				
2+20	78.66	78.55		75.5 9.1 6.0 +3.1				
2+60	78.54	78.44		75.4 9.2 6.5 +2.7	#1-6"	#2-6"	#3-4"	#4-6"
3+00	78.43	78.32		75.3 9.3 6.4 +2.9	375.75 9.87 3.17 5.00	374.32 10.30 6.66 +3.64	373.45 10.33 5.50 +4.83	373.11 10.67 6.19 3.48
3+40	78.32	78.20		75.2 8.6 5.8 +2.8				
3+80	78.20	78.09		75.1 8.7 5.3 +3.4				

Sewer Laterals

Alley BIK 1. J.T. Corcoran's Add.
Grades.

	W	E	BM. BR. NE. Eads + Center
00 = S. Line Center	137.53 4.65 OK 137.66*	137.65 4.66	138.11 4.92 38.19 OK
0+05 Brk	137.90 8.31 6.83 +1.48	137.7	138.10 8.11 4.96 +3.15
0+25 Brk	138.70 7.51 6.48 +1.03	138.90	138.90 7.31 4.67 +2.64
0+45 Brk	139.40 6.81 5.97 +0.84	139.60	139.60 6.61 4.14 +2.47
0+65 Brk	139.80 6.41 5.41 +1.00	140.00	140.00 6.21 4.32 +1.89
1+98	40.33 5.88 4.38 +1.53	40.53	40.53 5.68 4.01 +1.67
1+31	40.87 5.34 3.34 +2.00	E. Line 41.36 4.83 3.63 +1.22	41.07 5.14 4.00 +1.14
1+50 Eastonly	141.40 4.81 5.58 -0.77	141.60	141.60 4.21 3.55 +1.06
1+65 Brk	141.40 4.81 5.58 -0.77	141.60	141.60 4.21 3.55 +1.06
1+98	41.70 4.51 3.51 +1.00	41.90	41.90 4.31 2.31 +3.00
2+31	42.00 6.04 6.07 -0.03	42.20	42.20 5.84 4.80 +1.04
2+65 Brk	142.30 5.74 6.24 -0.50	142.50	142.50 5.54 4.39 +1.15
2+85 Brk	142.40 5.64 5.94 -0.30	142.60	142.60 5.44 4.15 +1.29
2+95 Brk	142.46 5.58 5.84 -0.26	142.66	142.66 5.38 4.18 +1.20

Excepted 1.0 on E.

3+05 Brk	142.40 5.64 5.67 -0.03	142.60 5.44 4.14 +1.30
3+25 Brk	142.30 5.74 5.69 +0.05	148.04 142.50 5.54 3.60 +1.94
3+45 Brk	142.00 6.04 5.58 +0.46	142.20 5.84 4.21 +1.63
3+65 Brk	141.60 6.44 5.84 +0.60	141.80 6.24 4.50 +1.74
3+85 Brk	141.10 6.94 6.47 +0.47	141.30 6.74 4.95 +1.79
4+21	40.00 8.04 8.11 -0.07	40.20 7.84 6.15 +1.69
4+58	38.90 7.14 9.76 -0.62	39.10 8.94 8.41 +0.53
4+75 Brk	137.80 10.24 10.77 -0.53	138.00 10.04 9.65 +0.39
5+00 = N. Line Rushville	137.35 10.69 10.59 137.45	137.58 10.46 10.46 138.16 9.88 9.25 138.29

Sewer laterals

①	②	③	④	⑤
134.9 11.3 4.3 +7.0	137.0 11.0 7.0 +6.0	134.6 13.4 6.5 6.9	134.6 13.4 9.5 +3.9	136.9 11.1 5.6 +5.5

10.51
137.53 = 137.53
W. Top of

Kellner Blvd B. St. to Bdu.

	Curve Grade	Wedge walk	E. & E. walk
5. line B. St	12.60 (12.57)	12.83 12.91	12.99
0+36 ^E			
0+73			
1+09 ^E Brk	12.32	12.36	12.46
1+49 ^E Brk A curb	12.38	12.42	(12.51) (12.49)
1+99 ^E			
2+49 ^E			
3+00 N. Line C.	12.40	(12.65) 12.45	(12.70) 12.50
5. line C. St	12.40	12.45	(12.70) 12.53
0+43 ^E	12.28		
0+86 ^E	12.16		
1+29 ^E	12.04		
1+72 ^E N. end dip	11.92	11.97	12.02
1+81 ^E dip		11.20	11.25
2+07 ^E S. end curb	11.83		
2+17 ^E dip		11.20	11.25
2+24 ^E S. end dip		11.83	11.88
2+69 ^E N. Line Bdu.	11.65	11.70	11.75

16.90 BM Indiana E. N.E. Cor.

	17.79	12.39	12.39	12.38	12.32	12.41	12.50
	5.38	5.40	4.68	4.69	4.75	4.46	4.57
	12.41	12.37					
	17.07						
	4.67						
	12.40						
	5.25	12.49	12.45	5.37	5.42	12.50	12.68
	17.65	5.20	4.62	12.42	12.36	4.58	4.39
		5.40	4.64			4.66	4.57
	12.40	40.10	-0.06			-0.11	-0.18
	4.73						
	17.13						
	5.15	12.60	12.55	5.28	5.33	12.63	12.80
	12.64	5.19	4.52	12.53	12.56	4.44	4.27
		5.40	4.64			4.66	4.57
		-0.21	-0.16			-0.23	-0.30
	5.51						
	5.19			11.65		11.83	
	12.60			5.49		5.50	
	11.96						
	12.83						
	11.70	11.83	11.20				
	5.43	5.30	5.93				
	5.48	5.80	5.88				
	-0.05	-0.50	+0.05				
	11.75	11.88	11.25				
	5.38	5.25	5.89				
	5.43	9.0					
	-0.07						
	11.92	12.04	12.16	12.28	5.25		
	5.21	5.09	4.97	4.85	12.40		
	11.20	11.97	12.09	12.21	12.33	5.20	
	5.93	5.46	5.04	4.92	4.80	12.45	
	5.43	5.21	5.02	4.97	4.85		
	+0.50	-0.05	-0.05	-0.05	-0.05		
	11.65	12.02	12.14	12.27	12.40	5.12	
	5.88	5.11	4.99	4.86	4.73	12.55	
	5.43	5.61	5.08	4.97	4.85		
	+0.45	-0.50	-0.10	-0.11	0.12		

Grado Fortuna
Promontory to Frontera

75' wide

	N	S	
HL Promontory	43.50	43.50	817 49.64
43 N	42.80	42.70	41.75
86 N	42.10	41.90	34.67
129 N	41.40	41.10	34.87
172 N	40.70	40.30	
215 N - E.L. Hairer	40.00	39.50	

HL Hairer	38.50	38.00	
40 N	35.92	35.10	
81-31 N	33.34	33.20	
122-04 N	30.76	29.30	
162-72 N	27.18	26.40	
181-96 N - Prop Cb Bc	26.96	25.03	
203-39 N - Cb Bc	25.60	23.50	
215 N - E.L. Frontera			

End of Curb Returns

N.E. Hairer + Fortuna	40.00	39.6	+3.8
S.F.	39.30	39.6	+1.0
N.N.	39.35	39.6	+2.5
S.N.	38.65	38.3	+0.6

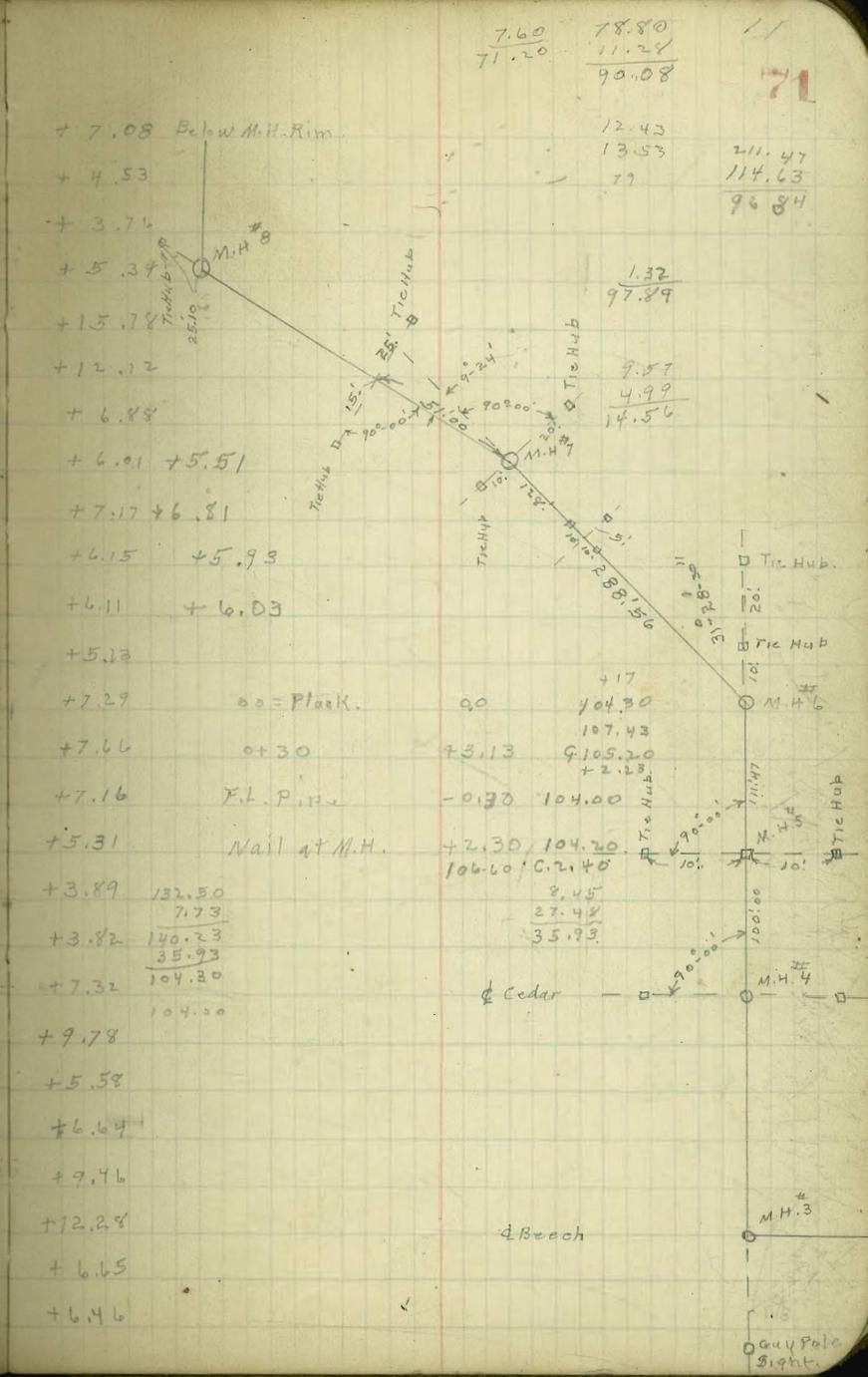
Note - For Proposed Curb Returns
Fortuna + Frontera Sec 1376 Page 64

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Scribble
Scribble
Scribble

S	43.50	42.70	41.90	41.10	40.30	39.50
	34	16	5.9	5.8	6.6	7.4
	04	15	2.6	3.2	1.5	5.6
	+32	+27	+2.6	+2.3	+3.1	+2.8
N	43.50	42.80	42.10	41.40	40.70	40.00
	34	31	2.8	5.5	6.9	6.9
	28	37	3.3	3.7	3.1	3.2
	+0.6	+0.4	+1.5	+2.7	+2.1	+2.7
S	38.00	35.10	32.20	29.30	26.40	23.50
	8.9	11.8	2.3	5.7	8.1	7.4
	0.0	0.0	-0.2	-0.3	2.0	1.0
					+1.1	+0.7
N	38.50	35.92	33.34	30.76	28.18	25.60
	8.1	11.9	13.6	3.7	6.3	8.9
	6.1	2.6	12.5	2.8	5.1	6.6
	+2.3	+2.6	+1.1	+0.9	+1.2	+0.9

Sewer Cons. Choats Add & Ravenna Park
Trunk Line S. of 3rd Ash to Nutmeg.

BM. M.H. Rim	11.28	90.08	78.80	72.22
Remains 0+00 2x M.H. Ash.			78.80	72.22
0+30			76.65	72.12
1+00			76.28	72.52
1+50			78.26	72.92
1+75			88.90	73.12
2+05			85.48	73.36
2+50 #1			80.60	73.72
2+85 ³⁵ M.H. #1 ³⁵ Ash. A 69° 15' 30" RT.	10.07	80.01	74.50	74.00
0+50			83.17	76.00
1+00			84.15	78.22
1+50 #2			86.11	80.00
1+40 M.H. #1 P. 12.88 99.21	3.75	86.33	81.20	81.20
0+50			89.64	82.35
1+00			91.16	83.50
1+50			91.81	84.65
2+00 #3			91.11	85.80
2+27 M.H. #2 Beech Δ 67° 15' 30" Lt.	8.90	90.31	86.42	86.42
0+50			91.39	87.57
1+50 #4 T.P. 12.47 110.36 #4 Beech	3.63	95.58	88.26	88.26
1+15.20 M.H. #3 20' E. of Whaley Δ 90° 05' RT. 110.36	11.51	98.85	89.07	89.07
0+50			95.80	90.22
1+00			98.01	91.37
1+50			101.98	92.52
2+00			105.95	93.67
2+50			101.47	94.82
3+00			102.43	95.97



7.60	78.80	
71.20	11.24	
	90.08	
	12.42	211.47
	13.53	114.63
	79	96.84

	1.32	
	97.79	
	9.57	
	4.99	
	14.56	
	+17	
	104.30	
	107.43	
	9105.20	
	+2.25	
	104.00	
	+2.30	
	104.20	
	106.60	
	8.45	
	27.42	
	35.93	

71

		179.56							
z T.P.	12.43	188.82	3.17	176.39					
M.H. 1500									
0+50			12.12	176.70	170.70		+6.00		
1+00			10.57	178.25	171.60		+6.55		
1+50	POIT. 7.94	189.18	7.62	181.20	172.50		+8.70		
1+80	T.P.	12.67	2.77	186.41	173.04		+13.37		
2+35	T.P.	7.48	5.31	193.77	174.03		+19.74		
			1.43	197.65					
			7.62	197.51 = 197.50					
3+18	M.H. 16		9.17	197.50	175.53 S.		+21.97	193.94	175.53 S. +18.41
3+18	AM.H. 16		9.17	197.50	180.94 N.		+16.56	193.94	180.94 N. +13.00
0+25								189.87	181.44 +8.43
0+50			17.17	189.50	181.94		+7.56		
1+00			17.12	189.55	182.94		+6.61		
1+50			16.69	189.98	183.94		+6.04		
2+00			15.12	191.55	184.94		+6.61		
2+25	M.H. 17		13.65	193.02	185.44		+7.58		
0+50	T.P.	13.09	11.61	195.06	187.44		+7.62		
		207.60	12.16	194.51					
1+00			10.84	196.76	189.44		+7.32		
1+50			10.56	197.04	191.44		+5.60		
2+00	M.H. 18		8.45	199.15	193.44		+5.71		
0+50			4.18	203.42	195.44		+7.98		
1+00			1.97	205.63	197.44		+8.19		
1+55			2.52	205.08	199.64		+5.44		
2+00	T.P.	14.80	0.11	207.47	201.44		+6.05		
2+23	M.H. 19		11.39	207.90	202.40		+5.50		
0+50			11.28	211.01	203.90		+7.11		
1+00			10.54	211.75	205.40		+6.35		
1+50			9.47	212.82	206.75		+6.07		
2+00			7.31	214.98	208.40		+6.58		

11.69	206.67	24
3.00	110.06	96
14.67	796.61	58
11.01	5.95	4
		220
14.01		
208.24		
222.27		
	208.28	
	13.90	
	197.50	
	7.61	
	205.11	11.17
	11.17	7.61
	293.94	3.56

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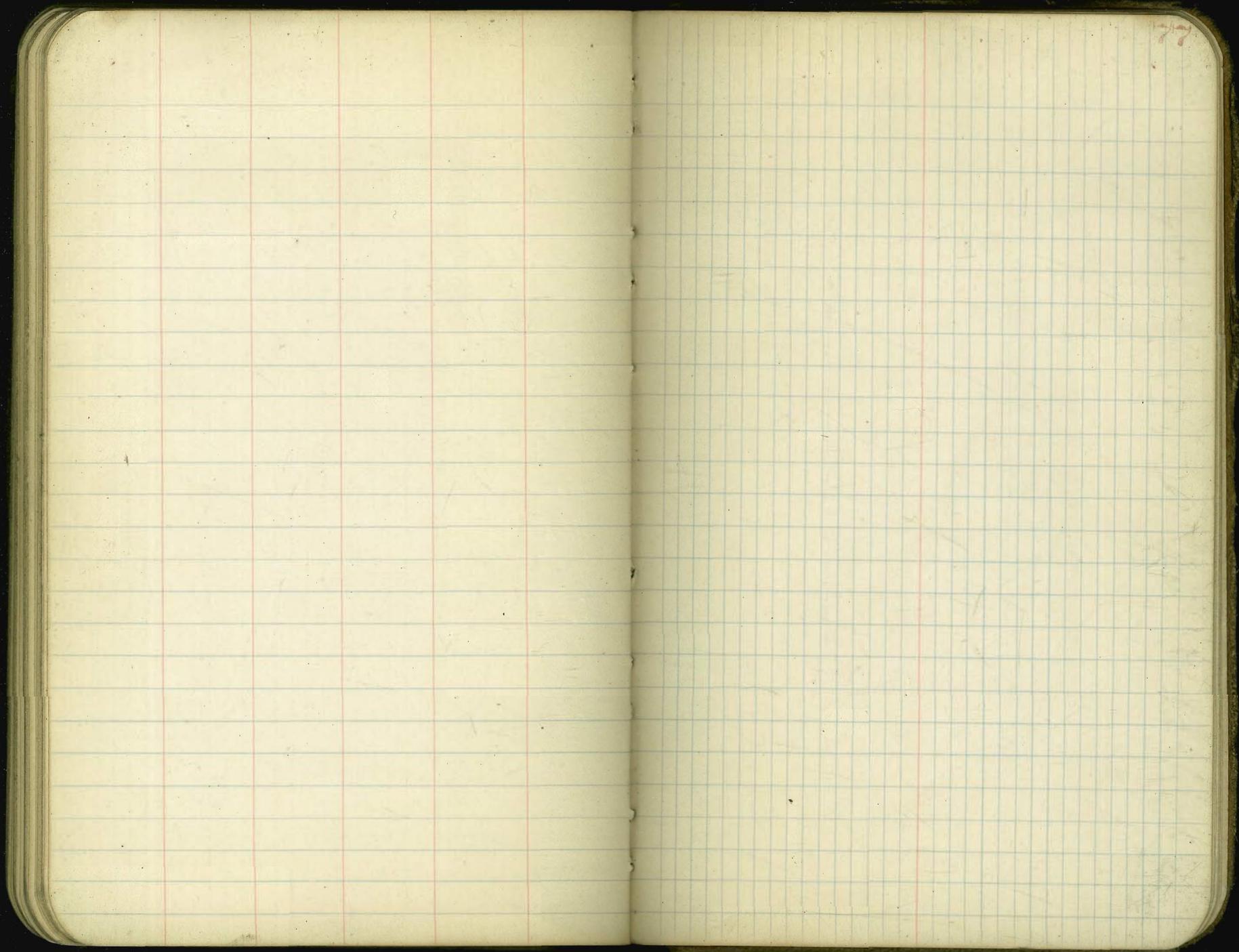
		222.29				
$\Delta 17.49-45$ #						
2+50 M.H. 20			4.76	217.53	209.90	+7.63
0+50	14.16		3.61	218.68	211.40	+7.28
1+00 T.R.	14.16	234.35	2.10	220.19	212.90	+7.29
1+50			10.91	23.44	214.40	+9.04
2+00			10.43	23.92	215.90	+8.02
2+50			7.45	26.90	217.40	+9.50
3+00			6.95	27.40	218.40	+8.50
					220.40	+8.43
3+50 M.H. 21			5.12	29.23	222.40	+6.83
	13.91	247.29	0.97	233.38		
0+50			10.12	37.17	225.40	+11.77
1+00			11.26	36.03	228.40	+7.63
1+50			9.67	37.62	231.40	+6.22
2+00			5.80	41.49	234.40	+7.09
2+50			2.24	45.05	237.40	+7.65
$\Delta 12.03-15$ #	11.87	258.21	0.55	246.74		
3+00 M.H. 22			10.41	48.20	240.40	+7.80
0+50			9.79	48.82	243.40	+5.42
1+00			3.00	55.61	246.40	+9.21
1+35 Ex. M.H. in Walnut St.			0.34	259.25	248.50	+9.75

Line from M.H. 16 to D.M.H. 25

206.67

236.74
7.90
228.84

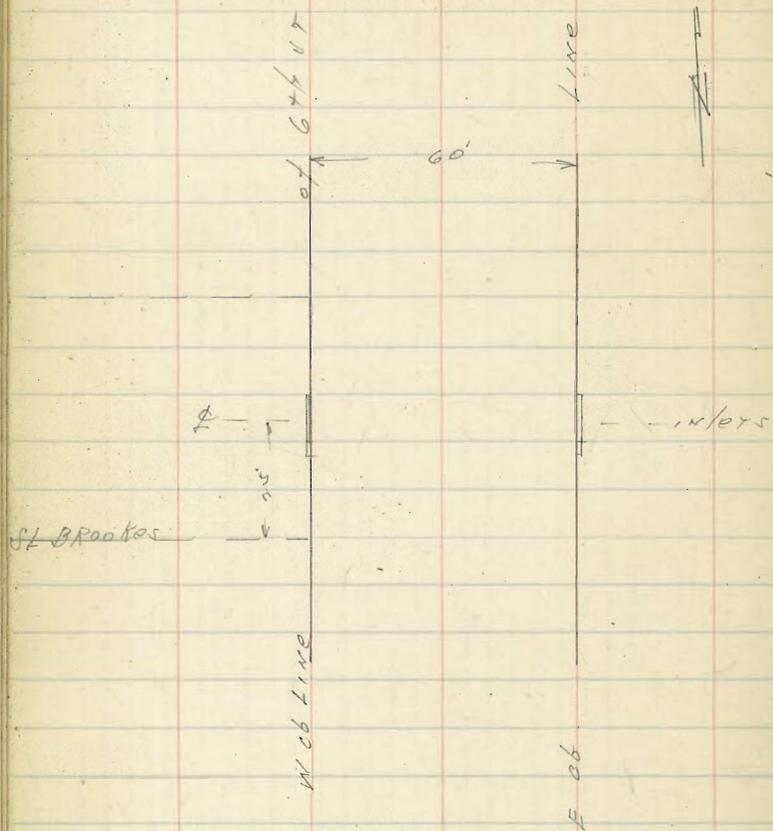
0+00 = M.H. 16			9.17	197.50	182.50	+15.00
0+50			14.56	192.11	186.50	+5.61
1+00			12.51	194.16	190.50	+3.66
1+27 ³⁵ M.H. 23			10.35	196.32	192.69	+3.63
T.P. & M.H. stake	14.56	210.40	10.83	195.84		
0+50			10.71	99.69	194.69	+5.00
1+00			7.12	203.28	196.69	+6.59
1+50			5.03	205.37	198.69	+6.68
2+00			3.19	207.21	200.69	+6.52
T.P.	12.00	222.22	0.18	210.22		
2+50			10.16	12.06	202.69	+9.37
2+89 ³⁰ M.H. 24			9.39	12.83	204.26	+8.57
0+50			4.36	17.86	207.76	+10.10
T.P.	14.71	236.74	0.19	222.03		
1+00			12.41	24.83	211.26	+13.07
1+50			9.72	27.02	214.76	+12.26
1+75			9.07	27.67	216.51	+11.16
2+15			9.23	27.51	219.21	+8.20
2+50			1.48	35.26	221.76	+13.50
2+85			3.93	32.81	224.21	+8.60
T.P.	9.41	245.93	0.22	236.52		
3+10 M.H. 25			4.88	241.05	225.96	+15.09
" " connection			12.93	233.00	233.00	
M.H. 16 =	205.11	205.11				
0+25			11.51	193.60	184.50	+9.10



6th + BROOKES

CURB INLET STAKES

Stakes set on ct line



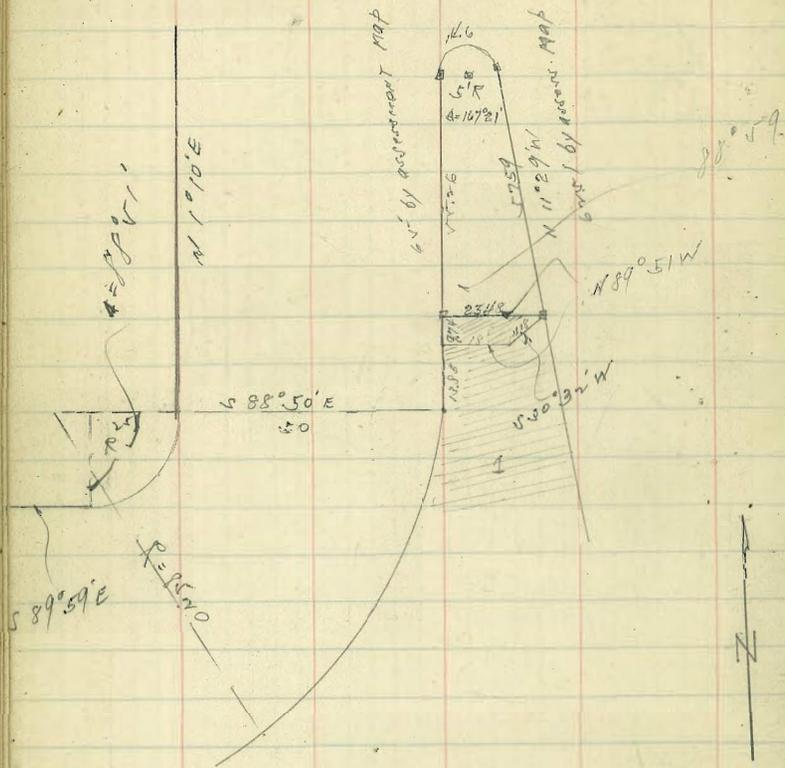
379.91 NW 1/4 BROOKES & 5th ST
 $\frac{10.46}{780.46}$

272.60 - top curb
 7.86

7/27/26

SURVEY of NORTH PORTION
of LOT 1 BIKH Impairment HqTS
check former Survey of Wm. Runsey but does
not check assessment map sketch.

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12/18
 Moore C ST Kettner to Calif
 for W.J. Dailey

2.96 = SWBP G of Kettner

7.30

8.00	2.75	2.50	2.20
4.00	4.45	4.80	4.90
4.40	4.50	4.80	4.90
1.10	4.50	4.80	4.90
cb. low	✓		

-0.34 = paving @ Calif
 xl cut.

-0.32 = Rail xl cut
 of KETTNER

34986 K CURB STAKES - Elev.

30th + UNIV NECOR

	Grade	Elev. desired
NECOR	356.0	356.14
100' North of UNIV	356.75	356.96 EX. CURB
100' E of 30th	355.56	355.79 EX. CURB

DIRECTIONS FOR USE OF TABLES

257.8
 58
 4199.8
 499.5

257.8
 78
 4179.8
 499.5

0 + 20
 4495
 6495

Distance of stake from side stake
 stake for any roadway, the cut or fill at side
 found is nearly level, the cut or fill at side
 located by the double entry method in
 left column and top row. The number in body
 of table in same row and column gives the distance
 from side stake to slope stake. If ground is not
 level, the distance from side stake to slope stake
 the side stake and slope stake lower target by the
 amount it cut, elevate if fill. Add this amount
 to cut or fill and find in table. Set up
 rod at this point and line of sight should cut
 target.

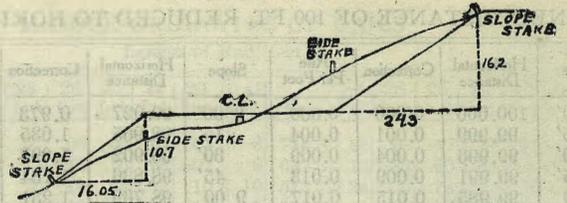
IMPROVED TABLES AND INFORMATION

The distance from a point on the tangent to
 the curve is very nearly the square of the tangent
 length divided by twice the radius.

Degree of curve with a given I may be found
 by dividing tangent (or external) opposite I by
 given tangent (or external).

add correction found in column of corrections.
 any other degree, divide by degree of curve and
 To find Tangent and External for curve of

TABLE XI
 ALL LAYERS OF THE REDUCED TO HORIZONTAL



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	73 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

BM S.E. Loring + Ocean Bl. 96.08
 1317
 47.39 HZ
 1055 -
 36867.P
 550 +
 42.36 HZ
 390 -
 38.96 XP
 279 +
 41.20 HZ
 573 -
 35.97

110.
 27.23
 82.67

