

C-175

PASTS

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FIELD BOOK

No. 385

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Entire Book indexed 3-11-35.  
c.s.h.  
Pages 58 to 72 not used at this time.

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**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.  
MICROFILMED

APR 9 1935



Fire Hads

S.E. Byron + Locust.

29.43

26.20 d. at P.C.

26.28  
~~3.15~~  
 2.86  
 + 0.29

S.E. Byron + Evergreen.

36.95  
 31.80 d. at P.C.  
~~5.95~~  
 36.95  
~~31.88~~  
 5.07  
~~4.73~~  
 + 0.34

S.E. Byron + Roscerans.

20.55  
~~8.80~~  
 29.35  
~~0.12~~  
 29.23  
~~7.57~~  
 36.80

2.14  
~~27.21~~  
 5.06  
 31.74

27.53  
~~7.26~~  
 36.79  
~~5.02~~  
 31.77

4.8  
~~32.0~~

20.55  
~~3.35~~  
 23.90

Wgutter  
 17.87

6.37  
~~17.53~~  
 17.85 17.75  
 17.37

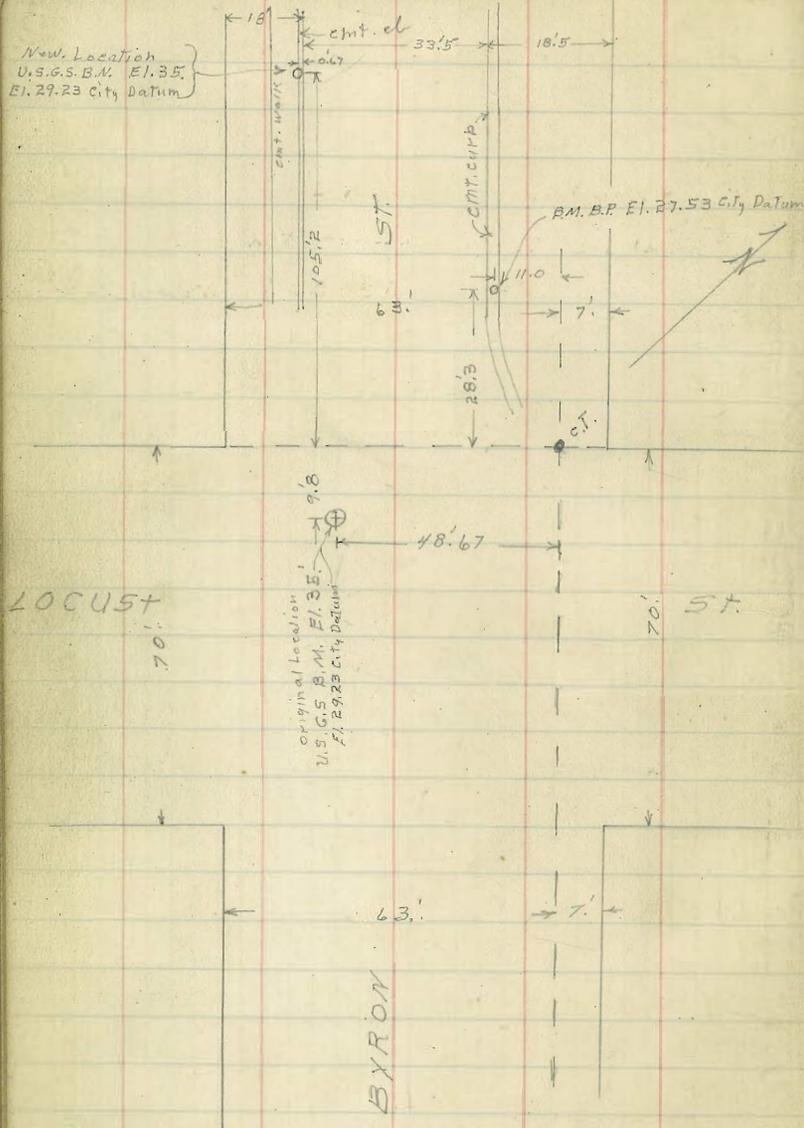
8.90  
~~15.00~~

77.23  
~~13.12~~  
 84.11  
~~0.30~~  
 84.41  
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~~0.73~~  
 72.59  
~~13.00~~  
 59.59  
~~0.01~~  
 59.60  
~~12.68~~  
 46.92  
~~0.57~~  
 47.49  
~~13.10~~  
 34.39  
~~1.97~~  
 36.36  
~~5.59~~  
 31.77

11.43  
~~61.16~~

21.77  
~~5.59~~

Location of U.S.G.S. B.M. Cor Byron + Locust  
Roseville



indexed-CSV.

3

B.M. B.P. N.W. Byron + Locust  $\times$  29.35  
 $\frac{1.82}{27.53}$   
 $\times$  29.35  
 $\frac{0.17}{29.23}$  on U.S.G.S. B.M.

U.S.G.S. B.M. Datum

29.23

U.S.G.S. B.M. City Datum.

+ 6.179

35.349

35.259

.09

29.28

6.119

35.399

35.259

Bulletin Dated  
May 19-1934

Stakes 45 x d.

to W.W. Davis 7-25-31 - 4 Bundles

30 stakes.

27.53  
6.41  
33.94

29.56 28.10  
4.36 5.84  
4.40 5.87  
6.04 6.05

28.05 27.93 27.80  
5.19 5.34 5.44

27.53  
5.71  
33.24

29.23  
4.01

B.M. 27.53 4.61 29.23  
6.34 4.61  
33.84

Tie in between City B.M.s. + U.S.G.S. B.M.

B.M. B.P. 6.47 27.11

20.64

T.P. 10.16 32.19

5.08 22.03

B.M. B.P. N.W. Locust + Byron S.W.

4.61 27.58 = 27.53

U.S.G.S. B.M. Locust + Byron

2.91 29.28 = 29.23

B.M. B.P. N.E. Evergreen + Byron

0.36 31.83 = 31.79

T.P. 3.21 31.68

3.72 28.47

Orig. B.M.

11.04 20.64

S.W. Corner Rd + Rosecrans.

Page 1.

Indexed  
C.S.K.

U.S. G.S. B.M.

6-13-35  
Miller  
Walker  
Bliss.

4

San Diego at Naval Training  
Station at Cor. Rosecrans & Freeman  
100' S. of Main Entrance To a  
Lieutenant Commanders House at  
Cor. of Lawn. & Edge of side walk.  
Standard Disk stamped L. 57. 1926  
Top concrete Post. 16.987 Meters

55.732' above Mean Sea level

B.M. BP		41.75	S. W. Lyden & Rosecrans
B.M. BP		37.49	N. W. Brown & & Rosecrans.
B.M. B.P.		51.50	N. W. Homer & Rosecrans.
B.M. B.P.	5.60	54.42	N. W. Freeman & Rosecrans.
U.S. C+G.S. B.M.	4.67	49.75	City Datum
		<u>6.119</u>	
		55.869	
		<u>55.732</u>	
		.137	

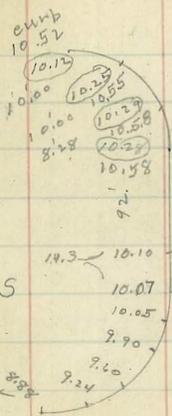
indexed  
C.S.K.

sect st 9/2 stakes.

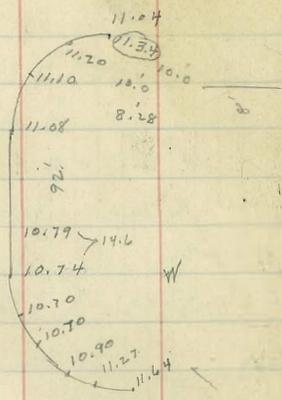
4.02  
10.18

3.75  
10.45

Cahan



ST



7.59 AM E. Cor Buret + Sect on star.

2.89								
10.47	W. 1.16	11.06	11.08	11.08	10.93	10.77	10.74	
7.59	11.04	3.14	3.12	1.12	1.27	1.41	1.46	
4.61		3.64						
12.20		-0.50						
3.41	E 3.68	10.55	10.58	10.58	10.35	10.13	10.07	
8.77	10.52	3.65	3.62	3.62	3.85	4.07	4.13	
5.41		4.15						
14.20		-0.50						

N. 10.70 10.70 10.90 11.27 11.64 Addison

E 10.02 9.90 9.60 9.24 8.88  
4.18 4.30 4.60

W. 11.00 10.60 10.25 10.00 9.75

	E.C.	
	9.60	9.00
	2.60	3.20

E 8.40 8.70 8.85 8.90 8.90

	8.80	8.20
	3.40	4.00

W 8.40 7.80 7.75 7.80 8.00

	P.C.	8.25	8.60
	4.40	4.45	4.40
	3.80	3.95	3.60

E 7.60 7.00 6.85 6.70 6.55

	4.60	5.20	5.35	5.50	5.65
--	------	------	------	------	------

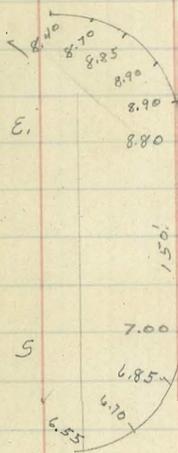
W 8.50 8.10 7.80 7.60 7.45

	1.97	2.37	2.67	2.87	3.02
					P.C.
					7.40
					3.07

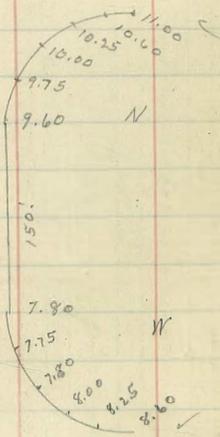
E 6.50 6.65 6.70 6.70

	3.97	3.82	3.77
--	------	------	------

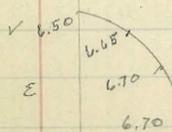
Addison



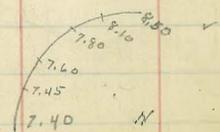
ST.



Byron

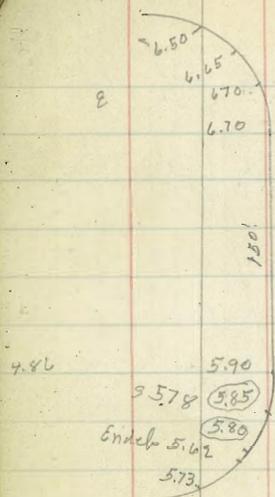


ST.



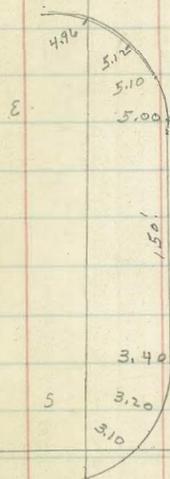
Byron

Scott St.



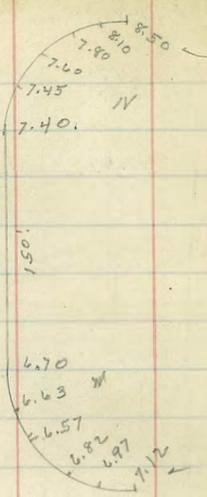
4.86

Carleton

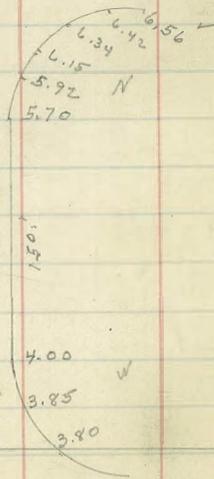


Diekens

St



St



St.

7.59 BM  
 2.88  
 10.47

N. Byron  
 E 6.70  
 3.78

W 7.40  
 3.08

W 4.32  
 6.16

E 5.34  
 5.14

P.C.  
 W 4.00  
 6.48

E 3.40  
 7.08

4.43  
 4.03

7.17  
 3.30

P.C.  
 5.92  
 4.55

5.10  
 5.38

3.85  
 6.62

3.20  
 7.28

P.C.  
 5.90  
 4.58

6.93  
 3.54

P.C.  
 5.70  
 4.78

5.00  
 5.48

3.80  
 6.67

3.10  
 7.38

5.78  
 4.70

6.63  
 3.85

5.13  
 5.34

4.46  
 6.02

3.93  
 6.55

3.10  
 7.38

4.86  
 5.02

5.90  
 6.38

4.54  
 5.91

3.93  
 6.55

3.10  
 7.38

3.10  
 7.38

Evergreen s/w stakes

indexed  
c. s. K.

ST.

Canon

L. 45.00  
45.11

1  
1  
1

46.60

96.57

S

42.50

42.15

41.75

41.30

40.80

43.20

42.95

42.60

43.10

44.00

45.50

W

Addison

ST

39.80

40.00

40.40

40.40

40.20

39.80

E

45.10

44.80

44.70

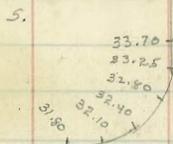
40.90

40.20

N.

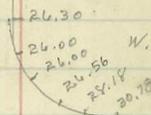
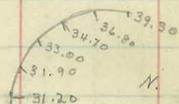
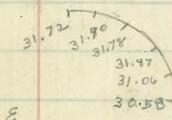
7

Evergreen.



Byron

ST.



Carlton

ST.

31.79 B.M. B.P. N.C. Byron + Evergreen

8.65  
40.47  
40.60  
29.97  
1.16  
32.03

8

P.C. E.C.  
W. 34.20 34.00 34.35 35.60 37.40 39.70

E 33.70 33.25 32.80 32.40 32.10 31.80

W 39.30 36.80 34.70 33.00 31.90 31.20  
1.17 3.47 5.77 7.47 8.57 9.27

E

5.68  
26.58  
End of.  
30.58  
6.97  
9.89  
9.920.41.  
25.06

W. 26.30 26.00 26.00 26.56 26.14 30.78.  
5.73 6.03 6.03

E 25.80 25.30 25.13 25.08 24.93 24.79  
6.23 6.73



Canon

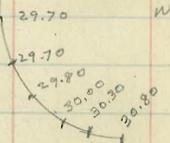
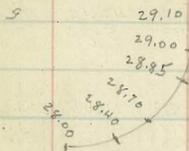
Locust St.

Indexed  
c.s.K.

39.80  
10.63  
40.30  
10.13

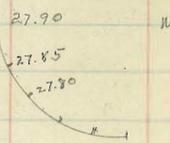
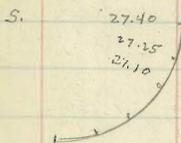
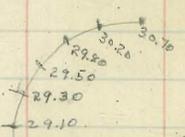
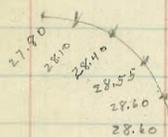
29.49

30.48

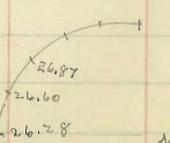
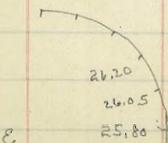


Addison

st



Byron



19.51 B.M. S.W. Evergreen @ Canon St.

0.42  
50.43  
12.87  
37.56  
0.25  
37.81

37.81  
1.81  
50.50 B.M. Top Hyd. Sac @ Locust & Addison

P.C.	30.30	30.00	29.80	29.70	29.70	29.70
W.	7.01	7.51	7.81	8.01	8.11	8.11

E	28.00	28.40	28.70	28.85	29.00	29.10
				8.96	8.81	8.71

W	Canon	ds.			
	30.48	7.59	7.85	8.11	
		7.33			

E	29.49	8.45	8.58	8.71
		8.32		

10

Indexed  
C.S.K.

College Way curb stakes

11-9-51  
Miller  
Walker  
B1.00

B.M. 440.80 B.P. E. side N. end Ex. Curb.

3.53  
16.47

	W. ch	C	E	S	C. d.
5+20 <sup>30</sup>	P.C. Ad 440.20				
7+20 B	444.20	43.53		43.53	444.20
6+80	441.39				441.39
6+40	438.58				438.58
6+33.5	P.C. Ret				438.12
6+00 B	435.77	35.10		35.10	435.77
5+80 B	434.42	33.72		33.95	434.59
5+60 B	433.25	32.52		32.95	433.57
5+40 B	432.24	31.48		32.14	432.74
5+25.53	J.O. Ret				432.18
5+20 B	431.40	30.61		31.49	432.07
5+03 <sup>53</sup>			1000 ft Rad		431.69
5+00	430.74	29.92		31.01	431.57
4+80	430.24	29.39		30.65	431.19
4+60	429.93	29.03		30.50	431.02
4+40	429.80	28.90		30.40	430.90
4+20	429.75	28.80		30.40	430.90
4+00	429.82	28.82		30.60	431.10
3+80	430.25	29.25		31.00	431.50
3+60	431.00	30.30		31.55	432.10
3+40	431.90	31.00		32.30	432.90
3+20	433.00	32.20		33.40	433.90
3+00	434.05	33.38		34.50	435.00
2+80	435.40	34.73		35.75	436.30

	W	E	S	C	P	PC
440.80						
3.73						
444.53						
0.33						
444.20						
35.34						
35.40						
440.80						
0.89						
441.69						
440.80						
0.04						
440.84						
4.05						
436.79						
7.46						
444.25						
0.52						
443.73						
12.64						
456.37						
35.34						
34.05						
7.64						
34.05						
4.79						
34.31						
6.53						
7.46						
-0.93						
29.82						
17.87						
12.32						
7.46						
-0.50						
29.75						
11.94						
29.85						
11.89						
29.93						
11.76						
30.24						
11.45						
30.74						
10.95						
37.64						
3.20						
3.75						
-0.55						
36.49						
4.35						
5.72						
-1.38						
35.34						
5.50						
6.93						
-1.43						
31.40						
12.95						
13.21						
-0.36						
32.24						
12.01						
11.00						
9.83						
10.33						
-0.50						
32.24						
32.74						
33.57						
34.59						
35.77						
38.12						
38.58						
0.8 up Hill						
71.39						
2.86						
2.80						
0.02						
0.52						
-0.50						
42.39						
3.14						
44.20						
0.93						
37.40						
36.68						
4.76						
36.12						
5.52						
4.30						
7.082						
7.139						
32.56						
9.08						
8.61						
8.03						
9.70						
-1.72						
33.83						
7.81						
9.28						
-1.47						

pc 11



	W. d.			C. d.
18710	443.30	42.63	42.63	443.30
PK. 17790	442.24	41.37	41.37	442.04
EV. 17780	441.34 X	40.67	40.67	441.34
17760	440.06	39.39	39.39	440.06
17740	439.02	38.35	38.35	439.02
17720	438.20	37.53	37.53	438.20
17700	437.61	36.81	36.81	437.61
16780	437.25	36.35	36.35	437.25
16760	437.12	36.12	36.12	437.12
16740	437.21	36.31	36.31	437.21
16720	437.54	36.74	36.74	437.54
16700	438.09	37.42	37.42	438.09
15780	438.87	38.20	38.20	438.87
15760	439.89	39.22	39.22	439.89
PK. 15740B	441.14	40.47	40.47	441.14
15700	443.85			443.85
EC. 14773.60	445.64			445.64
EV. 14760B	446.57	45.90	45.90	446.57
14740	447.86	47.09	47.09	447.86
14720	449.02	48.35	48.35	449.02
14700	450.12	49.45	49.45	450.12
13780	451.07	50.40	50.40	451.07
13771.20 EC. Ret East.	451.67			451.44
13765.60 PCN	451.91			451.91
13760		51.24	51.24	451.91
13740	452.60	51.93	51.93	452.60
13720	453.23	52.56	52.56	453.23
13700B	453.72	53.05	53.05	453.72
12750				

456.76 W	54.79	53.72	53.25	52.60	51.67	51.07	50.12
12.91	5.20	6.27	6.76	7.39	8.32	8.82	9.50
443.45							
4.64							
448.49 E	54.79	53.72	53.23	52.60	51.44	51.07	50.12
	3.59	4.66			5.32	5.69	6.47
459.99							
451.87 W	49.02	47.86	46.57	45.54	43.85	41.14	39.87
13.00				6.23	8.92	10.73	11.98
438.87							
8.67							
447.54 E	49.02	47.86	46.57	45.54	43.85	41.14	39.87
	7.74	8.90	10.19	12.91	15.35	18.20	21.62
457.09							
19.45							
37.54							
10.00							
10.33							
37.12							
10.92							
37.25							
10.79							
37.61							
9.93							
38.20							
9.34							
38.09							
10.40							
10.95							
11.28							
11.37							
11.24							
10.88							
10.27							
39.02							
8.52							
40.06							
7.48							
41.34							
6.20							
42.04							
5.50							
43.30							
4.24							
39.02							
9.47							
40.06							
8.43							
41.34							
7.15							
42.04							
6.45							
43.30							
5.19							

Returns COCOS

6.84	6.32	4	3	4	4.16
N 51.02	51.49	51.89	52.19	52.39	52.66
		5.97	5.67	5.27	5.20
					5.22
					42.74
					4
S 2.50	55.14	54.72	54.70	54.48	54.26
55.36	2.72	2.94	3.16	3.38	3.60
					1.12
					1.98

W. 26

E. 26

448.49 + H. 10 B. + 6.0 S. 7 + 1.0

51.05  
3.46  
3.83  
3.92

7.26

14

448.49 439.73	W	44.40 3.14	45.35 2.19	46.29 1.25	46.95 0.59	47.34 7.59	47.77 7.16	47.94 6.99
447.54 0.59					18.70 19.00 PER			PC 194.30
446.95 7.78	E	44.40 4.22	45.35 8.27	46.29 7.33	46.93 6.69	47.12 6.30	47.72 5.90	
452.93 1.65		40.41 +0.41	8.37 -0.10	7.61 -0.28	7.05 -0.36	6.81 -0.31	5.87 +0.03	
453.28 84. P. 10	W	48.74 6.27	49.10 5.91	49.45 5.56	49.80 5.21			
-453.32		2.3			4.71			
455.01					+0.50			
453.28 1.49	E	194.45 47.85	48.01	48.17				
454.97		5.77 5.77	5.61 5.22	5.45 5.57				
		0.00	+0.39	-0.12				
453.32 6.30	W							
453.62								

E 46.93	447.20	47.40	47.45	70	47.72
6.59	6.32		6.07	52	
6.13	6.69				
-0.34	-0.27				
453.52					47.62
					47.70
					6.36
					6.57
					-0.21
					5.87
					5.92
					+0.11

P.C.S. Mission

21 + 98.26	49.80
	49.45
	49.10

N.S. side, College Plate

20 + 58.626	48.74
20 + 29.42	48.47

20 + 17.4 pc. Walker 36.47

19 + 81.34

19 + 50.60 P.C. 4.4

ENC. 19 + 50.0 B

College Pl.

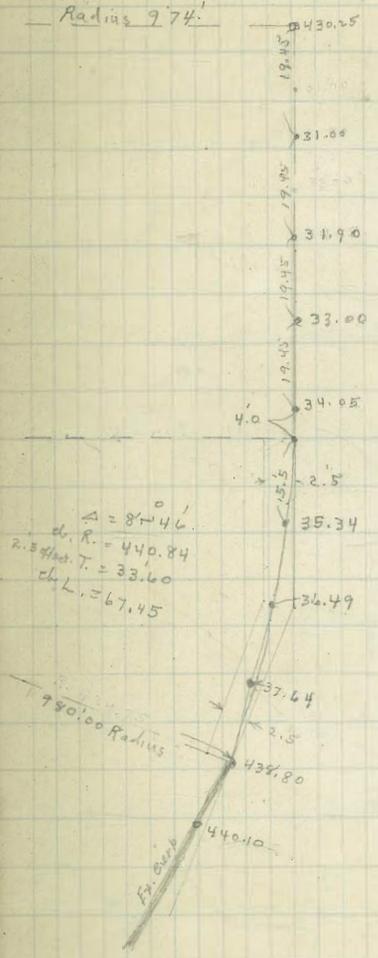
19 + 30	47.77	47.10	47.30	447.97
19 + 10	447.34	46.67	47.10	447.87
18 + 90	446.95	46.28	47.00	447.72
18 + 70	446.29	45.62	46.70	447.40
18 + 50	445.35	44.68	46.26	446.93
18 + 30	444.40	43.73	45.62	446.29
			44.68	445.35
			43.73	444.40

95  
25  
20

Transition from 52' to 40' Rdw.

Fire Hndt.  
S.E. Michigan

Radius 974'



456.37

S. End.

PC Ret

W	44.23	44.89	45.46	45.95	46.36	46.71	46.96	47.14	47.24
		11.49	10.91	10.42	10.01	9.66	9.41		

E	50.69	50.10	49.52	48.97	48.47	48.03	47.64	47.31	47.03
	5.48	6.27	6.85	7.40	7.90	8.34	8.73	9.09	9.38
		6.52	7.17	7.83	8.32	8.72	9.02	9.28	9.52
		-0.25	-0.52	-0.93	-0.82	-0.80	-1.24	+0.27	+0.28

W	47.26	47.21	46.99	46.69	46.48	46.27	46.06	45.86	
---	-------	-------	-------	-------	-------	-------	-------	-------	--

E	46.81	46.64	46.20	45.75	45.70	45.45	45.20	44.95	
	3.54	3.15	3.15	3.60	3.65	3.90	4.15	4.41	
	2.83	2.92	2.92	3.46	3.46	3.66	3.92	4.18	
	2.03	2.03	2.03	2.47	2.47	2.67	2.93	3.09	

43.27  
5.56  
48.83  
2.11  
46.65  
6.84  
53.49

W	45.65	45.45	45.21	44.97	44.73	44.49	44.25	44.01	43.77
		42.77	42.14						8.86
		5.96	5.43						43.77
		5.34	5.43						6.67

E	44.70	44.45	44.23	44.02	43.81	43.60	43.39	43.18	42.97
	6.55	6.00	5.77	5.54	5.32	5.10	4.88	4.67	4.45
	5.83	5.65	5.47	5.25	5.03	4.81	4.59	4.37	4.15
	5.03	5.15	5.29	5.45	5.62	5.79	5.96	6.13	6.30

W	43.52	43.27	43.05	42.89	42.80	42.76	42.72	42.65	42.59
	6.92	7.17	7.39	7.55	7.44	7.68	7.66	7.59	7.45

E	42.75	42.53	42.34	42.21	42.15	42.14	42.19	42.29	42.46
	6.08	6.30	6.49	6.62	6.68	6.69	6.64	6.54	6.37
								7.04	

W	43.19	43.45	43.71	43.97	44.22	44.48	44.74	45.00	45.26
	7.25	6.99	6.73	6.47	6.22	5.96	5.70	5.44	5.18
		5.38					4.74	4.09	

E	42.69	42.92	43.15	43.38	43.61	43.84	44.06	44.29	44.52
	6.14	5.91	5.68	5.45	5.22	4.99	4.77	4.54	4.31
						5.99	5.27	5.05	4.81
						-1.00	-0.50	-0.80	-0.50

W	45.52	45.72	46.04	46.21	46.58	46.85	47.12	47.38	
	4.92	4.67	4.40	4.13	3.86	3.59	3.32	3.06	
		5.67					1.71		
		-1.50							

E	44.75	44.97	45.20	45.43	45.66	45.89	46.13	46.37	
	4.08	3.86	3.63	3.43	3.17	2.94	2.70	2.46	
			4.13	4.43	4.73				
			-0.50	-1.00	-1.00				

W	48.20	47.96	47.64	47.25	46.77	46.22	45.64	
	3.67	3.91	4.23	4.62	5.10	5.65	6.23	

E	459.99	49.00	49.34	49.77	50.22	50.70	51.18	51.67
	457.06	10.99	10.63	10.22	9.77	9.29	8.81	

W	48.20	47.12	47.21	47.30	47.39	47.48	47.57	47.66
	50.44	350	380	389	395	401	407	413
		2.47	2.45	2.43	2.41	2.39	2.37	2.35
		2.68	2.66	2.64	2.62	2.60	2.58	2.56

E	46.81	46.64	46.20	45.75	45.70	45.45	45.20	44.95
	3.54	3.15	3.15	3.60	3.65	3.90	4.15	4.41
	2.83	2.92	2.92	3.46	3.46	3.66	3.92	4.18
	2.03	2.03	2.03	2.47	2.47	2.67	2.93	3.09

W	45.65	45.45	45.21	44.97	44.73	44.49	44.25	44.01	43.77
		42.77	42.14						8.86
		5.96	5.43						43.77
		5.34	5.43						6.67

E	44.70	44.45	44.23	44.02	43.81	43.60	43.39	43.18	42.97
	6.55	6.00	5.77	5.54	5.32	5.10	4.88	4.67	4.45
	5.83	5.65	5.47	5.25	5.03	4.81	4.59	4.37	4.15
	5.03	5.15	5.29	5.45	5.62	5.79	5.96	6.13	6.30

W	43.52	43.27	43.05	42.89	42.80	42.76	42.72	42.65	42.59
	6.92	7.17	7.39	7.55	7.44	7.68	7.66	7.59	7.45

E	42.75	42.53	42.34	42.21	42.15	42.14	42.19	42.29	42.46
	6.08	6.30	6.49	6.62	6.68	6.69	6.64	6.54	6.37
								7.04	

W	43.19	43.45	43.71	43.97	44.22	44.48	44.74	45.00	45.26
	7.25	6.99	6.73	6.47	6.22	5.96	5.70	5.44	5.18
		5.38					4.74	4.09	

E	42.69	42.92	43.15	43.38	43.61	43.84	44.06	44.29	44.52
	6.14	5.91	5.68	5.45	5.22	4.99	4.77	4.54	4.31
						5.99	5.27	5.05	4.81
						-1.00	-0.50	-0.80	-0.50

W	45.52	45.72	46.04	46.21	46.58	46.85	47.12	47.38	
	4.92	4.67	4.40	4.13	3.86	3.59	3.32	3.06	
		5.67					1.71		
		-1.50							

E	44.75	44.97	45.20	45.43	45.66	45.89	46.13	46.37	
	4.08	3.86	3.63	3.43	3.17	2.94	2.70	2.46	
			4.13	4.43	4.73				
			-0.50	-1.00	-1.00				

47.45  
2.79  
47.92  
2.52  
48.19  
2.25  
48.46  
1.98  
48.65  
1.79  
48.67  
1.77  
48.52  
1.92  
48.52  
2.62  
48.52  
-0.50  
48.07  
5.42  
48.20  
5.29  
48.42  
5.07  
48.69  
4.80

46.65  
46.93  
47.21  
47.50  
47.79  
48.07  
48.20  
48.42  
48.69  
49.00  
4.49

453.28  
1.67

454.97	PC	1	2	3	4	5	6	7	8	9	10	11	12
47.94	48.00	48.05	48.10	48.15	48.20	48.25	48.30	48.35	48.40	48.45	48.50	48.55	48.60
7.03	6.97	6.92	6.87	6.82	6.77	6.72	6.67	6.62	6.57	6.52	6.47	6.42	6.37
					7.23	7.22	7.07						
					-0.50	-1.00	-0.50						

N	48.74	48.68	48.64	48.58	48.53	48.47	48.42	48.37	48.32	48.27	48.22	48.17	48.12
	6.23	6.28	6.33	6.37	6.44	6.50	6.55	6.60	6.65	6.70	6.75	6.80	6.85

Curve W. of Hwy

447.61	PC	1	2	3	4	5	6	7	8	9	10
48.42	48.40	48.36	48.32	48.28	48.24	48.20	48.16	48.12	48.08	48.04	48.00
6.55	6.57	6.61	6.65	6.69	6.73	6.77	6.81	6.85	6.89	6.93	6.97

453.32	PC	1	2	3	4	5	6	7	8	9	10
48.04	48.03	48.00	47.96	47.92	47.88	47.84	47.80	47.76	47.72	47.68	47.64
6.91	6.94	6.97	7.01	7.04	7.07	7.10	7.13	7.16	7.19	7.22	7.25

Mission Valley Rd. +-

50.3

N	51.05	50.8	50.3	49.6	48.9	48.2	47.5	46.8	46.1	45.4	44.7	44.0	43.3
	4.31	4.6	5.1	5.8	6.3	6.9	7.5	8.1	8.7	9.3	9.9	10.5	11.1

N	49.68	49.34	48.94	48.49	48.04	47.59	47.14	46.69	46.24	45.79	45.34	44.89	44.44
	5.6	6.0	6.4	6.8	7.2	7.6	8.0	8.4	8.8	9.2	9.6	10.0	10.4

49.87	PC	1	2	3	4	5	6	7	8	9	10
49.80	49.70	49.60	49.50	49.40	49.30	49.20	49.10	49.00	48.90	48.80	48.70
5.5	5.6	5.7	5.8	5.9	6.0	6.1	6.2	6.3	6.4	6.5	6.6
4.7											
10.8											

453.62

S	43.7	45.0	46.3	47.6	48.9	50.2	51.5	52.8	54.1	55.4	56.7	58.0	59.3
	11.7	10.4	9.0	7.7	6.3	5.0	3.7	2.4	1.1	-0.2	-1.5	-2.8	-4.1

PC	1	2	3	4	5	6	7	8	9	10
48.60	48.74	48.89	49.03	49.17	49.31	49.45	49.59	49.73	49.87	50.01
5.02	5.08	5.13	5.17	5.21	5.24	5.27	5.30	5.33	5.35	5.38
4.50										
10.52										

53.32  
4.63  
57.95

Mission Valley Rd. stakes

N	49.48	49.40	49.32	49.24	49.16	49.08	49.00	48.92	48.84	48.76	48.68	48.60	48.52
	8.27	8.35	8.43	8.51	8.59	8.67	8.75	8.83	8.91	8.99	9.07	9.15	9.23
	7.33	7.77	7.97	8.09	8.13	8.27	8.35	8.43	8.51	8.59	8.67	8.75	8.83
	10.34	10.38	10.36	10.41	10.43	10.34	10.37	10.26	10.14	10.02	9.90	9.78	9.66

S	48.60	48.68	48.77	48.86	48.95	49.04	49.13	49.22	49.31	49.40	49.49	49.58	49.67
	9.33	9.27	9.26	9.23	9.19	9.14	9.09	9.04	8.99	8.94	8.89	8.84	8.79
	8.83	9.13	9.22	9.26	9.24	9.23	9.23	9.23	9.23	9.23	9.23	9.23	9.23
	10.52	10.14	9.74	9.34	8.94	8.54	8.14	7.74	7.34	6.94	6.54	6.14	5.74

7.92 25.6

24

19.2

1137

48

35.44

50.65

35.44

51.39

51.50

51.59

51.68

51.77

51.86

51.95

52.04

52.13

52.22

52.31

52.40

52.49

52.58

52.67

52.76

52.85

52.94

53.03

53.12

53.21

53.30

53.39

53.48

53.57

53.66

53.75

53.84

53.93

54.02

54.11

54.20

54.29

54.38

54.47

54.56

54.65

54.74

54.83

54.92

55.01

55.10

55.19

55.28

55.37

55.46

55.55

55.64

55.73

55.82

55.91

56.00

56.09

56.18

56.27

56.36

56.45

56.54

56.63

56.72

56.81

56.90

56.99

57.08

57.17

57.26

57.35

57.44

57.53

57.62

57.71

57.80

57.89

57.98

58.07

58.16

58.25

58.34

58.43

58.52

58.61

58.70

58.79

58.88

58.97

59.06

59.15

59.24

59.33

59.42

59.51

59.60

59.69

59.78

59.87

59.96

60.05

60.14

60.23

60.32

60.41

60.50

60.59

60.68

60.77

60.86

60.95

61.04

61.13

61.22

61.31

61.40

61.49

61.58

61.67

61.76

61.85

61.94

62.03

62.12

62.21

62.30

62.39

62.48

62.57

62.66

62.75

62.84

62.93

63.02

63.11

63.20

63.29

63.38

63.47

63.56

63.65

63.74

63.83

63.92

64.01

64.10

64.19

64.28

64.37

64.46

64.55

64.64

BM.		100'	PC	EC	100'	PC	2	3	4	
453.32	N	49.63	49.65	49.65	49.78	50.22	50.36	50.44	50.55	50.66
2.29		4.79	4.82	4.87	4.94	4.10	4.16	3.98	3.87	3.76
455.61		4.29								
4.10		+0.50								
451.59										
1.83	S	5.70	49.13	49.22	49.27	50.22	50.45	50.66	50.93	51.21
454.42		5.39	5.29	5.20	4.65	4.10	3.97	3.76	3.49	3.21
3.06					4.15					3.20
451.36					10.50					
451.36	N	5	6-RT		50.91	50.90	51.00	51.17	51.24	51.32
5.69		3.69	3.67		6.24	6.15	6.05	5.93	5.81	5.73
457.05			3.65		6.21	6.13	6.04		5.31	
			ck		20.24	6.63	6.54		10.50	
					-0.50					
	S	51.44	51.55		51.32	51.33	51.34	51.35	51.36	51.36
2.98		2.98	2.87		5.73	5.72	5.71	5.70	5.69	5.69
2.98			2.87		5.72				5.19	
			ck						10.50	
	N	RT	100'	PC	RT	100'	PC	W End	W of W Alley	PC Prop
51.37		51.62	51.89	51.87	51.85	51.85	51.85	49.45	49.40	49.63
5.68		5.43	5.16	5.18	5.20			4.77	4.82	4.79
		4.93						4.67	4.32	4.27
		10.50						10.50	10.50	10.50
	S	51.37	51.60	51.83	51.87	51.88	51.88	49.11	49.08	49.03
5.68		5.45	5.22	5.18	5.07	5.07	5.30	5.34	5.24	5.29
					4.57			4.84	4.84	
					10.50			10.50	10.50	

College Ave Curve N. End.

		1	2	3	4	5	6	7	
451.36									
2.57									
453.93									
	E	PC 447.11	46.80	48.50	48.20	47.89	47.58	47.27	46.97
			5.13	5.43	5.73	6.04	6.35	6.66	6.96
			4.93	5.23	5.54	5.85	6.16	6.46	
			10.50	10.50	10.50	10.50	10.50	10.50	
	E	8-PC	EC	Prop					
		446.67	46.87	47.00					
		7.26	7.06	6.93					
		6.76	6.56	6.01					
		10.50	10.50	10.50					

indexed  
c.s.k.

LEVELS FOR STORM DRAIN  
Along lot line 9+10  
"CRENSITA DRIVE"

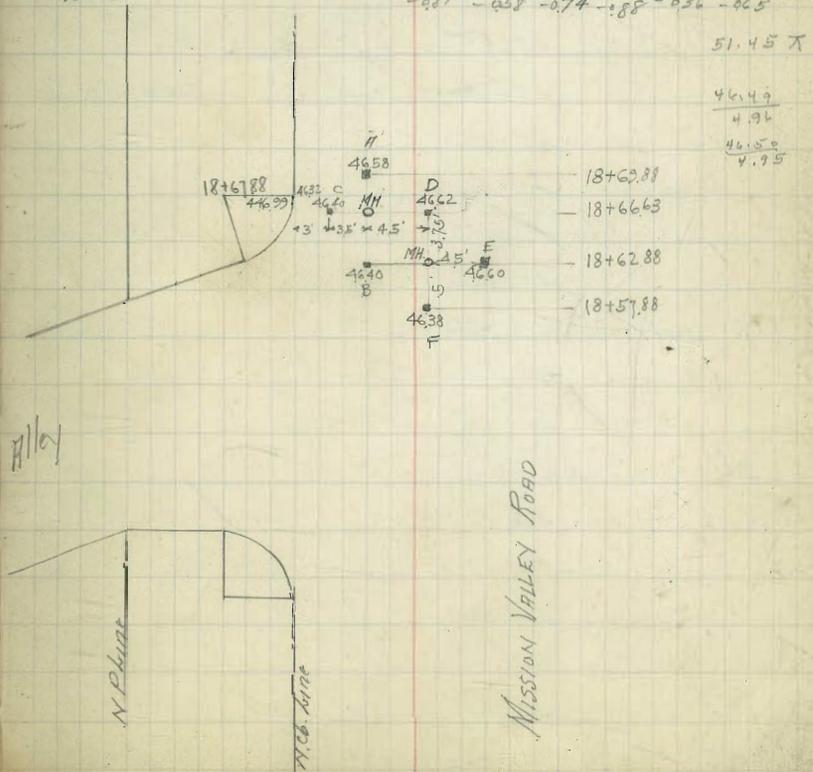
Station	+	PIZ	-	Elev. Stakes	Elev. Grade	Flowline
Start cb. line = 0+00		447.35	5.15	442.20	436.00	+6.20
+4.5			2.95	444.40	435.00	+9.40
+9.0 = Break.			7.44	439.91	434.00	+5.91
+14.0					425.50	
+19.0 = End line					417.00	
+1+00 = Temp End		8.52		438.83	432.30	+6.53

S.M. top of P. 16  
442.97  
438.7  
427.35 - 7  
482 -  
chk. 2nd stake North 242.53 v

indexed  
c.s.k.

LEVELS FOR M.H. in Mission Valley Rd.  
As Per Sketch. Grades are top of Finish Paving

Mission Valley Rd.	A	B	D	F	E
447.61 - S.M. in Pole 120' South	4658	4640	4662	4638	4640
297.7	395	413	391	415	393
450.53 - 7	471	421	465	523	448
	-981	-258	-074	-188	-936



51.45 X  
46.49  
4.96  
46.50  
4.95

18+69.88  
18+66.63  
18+62.88  
18+57.88



Mission Valley Road Cont. from P. 20

Nh. Sta.	Nh. Grade	Sh. Sta.	Sh. Grade
9	447.93	4	451.38
10 = 15 + 29.74 = P.T.	447.35	5	451.31
15 + 40	446.87	6 = PVC	451.24
+60	445.75	7	451.19
+80	444.66	8	451.17
16 + 00	443.70	9	451.17
+20	443.00 +	10 = P.R.C. <sup>2X Cor.</sup> <sub>hunch Paced</sub>	451.19
+40	442.58	P.R.C. <sup>S. Cor. hunch Paced</sup>	450.76
+60	442.40	1	450.61
+80	442.50	2 = PVC	450.46
17 + 00	442.85 +	3	450.28
+50	444.06	4	450.03
18 + 00	445.27	5	449.71
+35.91 = PC Alley Ret.	446.15	6	449.34
West side	446.30	7	448.90
West side	446.39	8 = PVC	448.39
West side	446.37	9	447.85
N.R. Abrog Alley	446.37	10 =	447.31
N.R. Alley East side	446.64	15 + 40	446.87
1/2 way from N.R. to P.C.	446.99	+60	445.75
P.C. Alley Ret. East side	448.02	+76.22 cb P.C. Ret.	444.78
18 + 67.88 = P.T. Alley Ret.	449.04	1	444.19
19 + 06.82	449.24	2	443.68
19 + 45.76 cb P.C.	449.46	3	443.27
1	449.72	4	442.94

Cont. P. 22

Station	Grade	Station	Grade
447.61	5.29	447.79	6.97
452.90		448.00	7.75
		448.20	8.53
		448.40	9.31
		448.60	10.09
		448.80	10.87
		449.00	11.65
		449.20	12.43
		449.40	13.21
		449.60	13.99
		449.80	14.77
		450.00	15.55
		450.20	16.33
		450.40	17.11
		450.60	17.89
		450.80	18.67
		451.00	19.45
		451.20	20.23
		451.40	21.01
		451.60	21.79
		451.80	22.57
		452.00	23.35
		452.20	24.13
		452.40	24.91
		452.60	25.69
		452.80	26.47
		453.00	27.25
		453.20	28.03
		453.40	28.81
		453.60	29.59
		453.80	30.37
		454.00	31.15
		454.20	31.93
		454.40	32.71
		454.60	33.49
		454.80	34.27
		455.00	35.05
		455.20	35.83
		455.40	36.61
		455.60	37.39
		455.80	38.17
		456.00	38.95
		456.20	39.73
		456.40	40.51
		456.60	41.29
		456.80	42.07
		457.00	42.85
		457.20	43.63
		457.40	44.41
		457.60	45.19
		457.80	45.97
		458.00	46.75
		458.20	47.53
		458.40	48.31
		458.60	49.09
		458.80	49.87
		459.00	50.65
		459.20	51.43
		459.40	52.21
		459.60	52.99
		459.80	53.77
		460.00	54.55
		460.20	55.33
		460.40	56.11
		460.60	56.89
		460.80	57.67
		461.00	58.45
		461.20	59.23
		461.40	60.01
		461.60	60.79
		461.80	61.57
		462.00	62.35
		462.20	63.13
		462.40	63.91
		462.60	64.69
		462.80	65.47
		463.00	66.25
		463.20	67.03
		463.40	67.81
		463.60	68.59
		463.80	69.37
		464.00	70.15
		464.20	70.93
		464.40	71.71
		464.60	72.49
		464.80	73.27
		465.00	74.05
		465.20	74.83
		465.40	75.61
		465.60	76.39
		465.80	77.17
		466.00	77.95
		466.20	78.73
		466.40	79.51
		466.60	80.29
		466.80	81.07
		467.00	81.85
		467.20	82.63
		467.40	83.41
		467.60	84.19
		467.80	84.97
		468.00	85.75
		468.20	86.53
		468.40	87.31
		468.60	88.09
		468.80	88.87
		469.00	89.65
		469.20	90.43
		469.40	91.21
		469.60	91.99
		469.80	92.77
		470.00	93.55
		470.20	94.33
		470.40	95.11
		470.60	95.89
		470.80	96.67
		471.00	97.45
		471.20	98.23
		471.40	99.01
		471.60	99.79
		471.80	100.57
		472.00	101.35
		472.20	102.13
		472.40	102.91
		472.60	103.69
		472.80	104.47
		473.00	105.25
		473.20	106.03
		473.40	106.81
		473.60	107.59
		473.80	108.37
		474.00	109.15
		474.20	109.93
		474.40	110.71
		474.60	111.49
		474.80	112.27
		475.00	113.05
		475.20	113.83
		475.40	114.61
		475.60	115.39
		475.80	116.17
		476.00	116.95
		476.20	117.73
		476.40	118.51
		476.60	119.29
		476.80	120.07
		477.00	120.85
		477.20	121.63
		477.40	122.41
		477.60	123.19
		477.80	123.97
		478.00	124.75
		478.20	125.53
		478.40	126.31
		478.60	127.09
		478.80	127.87
		479.00	128.65
		479.20	129.43
		479.40	130.21
		479.60	130.99
		479.80	131.77
		480.00	132.55
		480.20	133.33
		480.40	134.11
		480.60	134.89
		480.80	135.67
		481.00	136.45
		481.20	137.23
		481.40	138.01
		481.60	138.79
		481.80	139.57
		482.00	140.35
		482.20	141.13
		482.40	141.91
		482.60	142.69
		482.80	143.47
		483.00	144.25
		483.20	145.03
		483.40	145.81
		483.60	146.59
		483.80	147.37
		484.00	148.15
		484.20	148.93
		484.40	149.71
		484.60	150.49
		484.80	151.27
		485.00	152.05
		485.20	152.83
		485.40	153.61
		485.60	154.39
		485.80	155.17
		486.00	155.95
		486.20	156.73
		486.40	157.51
		486.60	158.29
		486.80	159.07
		487.00	159.85
		487.20	160.63
		487.40	161.41
		487.60	162.19
		487.80	162.97
		488.00	163.75
		488.20	164.53
		488.40	165.31
		488.60	166.09
		488.80	166.87
		489.00	167.65
		489.20	168.43
		489.40	169.21
		489.60	169.99
		489.80	170.77
		490.00	171.55
		490.20	172.33
		490.40	173.11
		490.60	173.89
		490.80	174.67
		491.00	175.45
		491.20	176.23
		491.40	177.01
		491.60	177.79
		491.80	178.57
		492.00	179.35
		492.20	180.13
		492.40	180.91
		492.60	181.69
		492.80	182.47
		493.00	183.25
		493.20	184.03
		493.40	184.81
		493.60	185.59
		493.80	186.37
		494.00	187.15
		494.20	187.93
		494.40	188.71
		494.60	189.49
		494.80	190.27
		495.00	191.05
		495.20	191.83
		495.40	192.61
		495.60	193.39
		495.80	194.17
		496.00	194.95
		496.20	195.73
		496.40	196.51
		496.60	197.29
		496.80	198.07
		497.00	198.85
		497.20	199.63
		497.40	200.41
		497.60	201.19
		497.80	201.97
		498.00	202.75
		498.20	203.53
		498.40	204.31
		498.60	205.09
		498.80	205.87
		499.00	206.65
		499.20	207.43
		499.40	208.21
		499.60	208.99
		499.80	209.77
		500.00	210.55

Mission Valley Road  
Cont. from P-21

N.L. Sta	N.L. Grade	S.L. Stu	S.L. Grade	
4	450.00	5	442.61	N 450.00 5030 5055 5074 5089 5100 5105 2.17 3.72 3.78 3.58 3.47 3.42 +0.90 +0.41 +0.18 +0.10 -0.04 +0.62 -0.51 -0.29 -0.12 +0.51
5	450.30	6	442.16	447.61 5 442.61 421.6 416.1 409.4 4017 392.9 398.7 405.5 411.8 417.5 3.55 8.0 10.3 11.9 11.5 451.16 -1.3 12.1 14.1 13.9 -1.3 -1.8 -2.2 -2.6
6	450.55	7	441.61	
7	450.74	8	440.94	N
8	450.89	9	440.17	453.92-877.10 Pk 115+
9	451.00	10=EC SW Cor Unpaired St.	439.29	454.47-x S 432.24 4270 4309 4392 4376 45.0 4634 4643 46.97 46.49 46.54 9.0 7.5 7.4 7.5 -3.7 +0.1
	451.05	SW Cor. " = P.C.	439.87	EC. P.C. E.C. S. Line P.L. W.P. 46.95 47.00 4.50 4.45 5.26 5.54 -0.76 -1.14
		1	440.55	447.61-877.10 Pk 423+ 457.84-x
		2	441.18	PT 446.77 4218 4830 4828 5.89 4.66 3.54 5.19 6.07 5.90 3.57 5.22 -1.00 -0.84 -0.13 +0.17
		3	441.75	447.61 4.43 4 51.45 5.46 -1.21
		4	442.24	
		5	442.70	
		6	443.09	
		7	443.42	
		8=17+4334-EC. +9334	443.70 445.02	
		SW Cor 18+43.19 - P.C. Alley Ref.	446.34	
		SW Cor. E.C. Alley	446.43	
		S.P.L. on West Side Alley	446.47	
		S.P.L. East "	446.49	
		1/2 Way to P.C. from RL	446.54	
		P.C. Alley Ref. on East.	446.77	
		18+75.12=PT Alley Ref	447.18	
		19+17.30 SW C. Alley Ref	448.30	
		19+54.44= P.C. cb Ref	449.28	

Mission Valley Road Cont from P. 22

Sta.	Sl. Grade
1	449.49
2	449.66
3	449.79
4	449.87
5	449.92
6	449.91
7	449.88
8 = E.C. College Hwy	449.80

AS. 97-K

5 449.49	4266	4279	4387	4222	4291	4288	4280
2.78	4.71	4.68	4.60	4.55	4.56	4.59	4.67
5.37	6.89	5.01	3.92	2.61	1.62	2.74	2.17
-0.89	-0.11	-0.33	-0.22	-0.12	-0.06	-0.15	+0.50

S.W. Gr. Machine Rd.

COLLEGE

A.E.

KATTA  
20'

cb P.T. = 15+23.24

POND  
+2.20

15+76.22

15+30.73

15+45.76

15+54.45

LINDO

DOSEO

cb PC = 12+61.34

12+61.15 = cb PC.

12+34.13 = cb AT

10+76.22 = of PC.

10+55.34

MISSION VALLEY

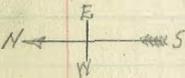
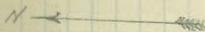
Alley

Road

Valley

17+43.34

447.61  
447.61 = 8 M.S  
in Pole



ALLEY

20'

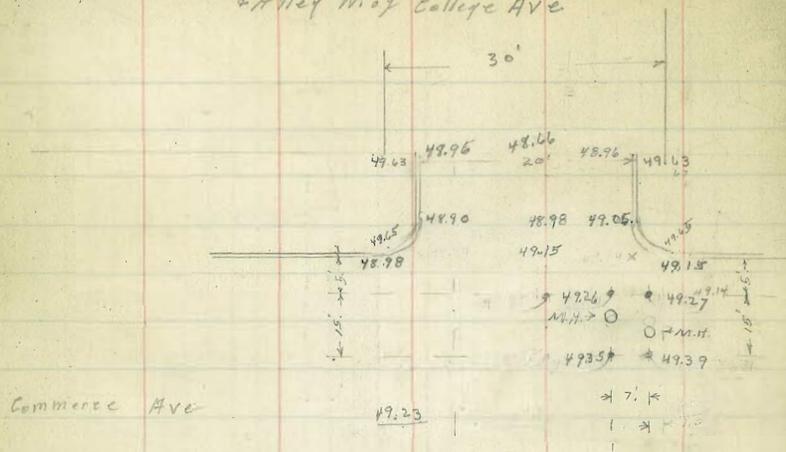
MISSION

15+29.34

15+76.22

15+30.73

Grades for M.H.s. in Commerce Ave.  
& Alley W of College Ave



Indexed  
e.s.R.

Commerce Ave elev. cuts

25

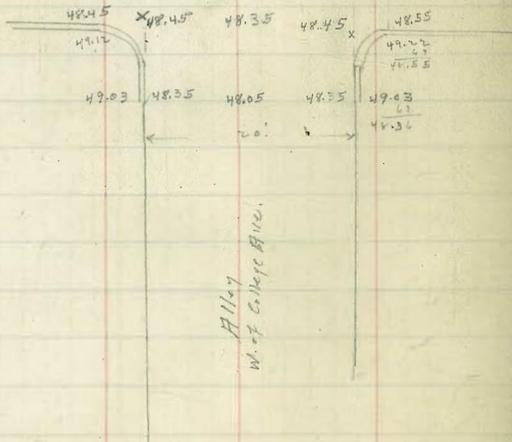
	Alley Ret.							
	N. Line	P.C.	E.C.	P.C.				
45447	$\frac{48.96}{5.51}$	$\frac{49.05}{5.42}$	$\frac{48.10}{5.37}$	$\frac{49.15}{5.32}$	$\frac{49.82}{4.65}$	$\frac{49.86}{4.61}$	$\frac{49.94}{4.53}$	$\frac{50.05}{4.42}$
	N 50.15	50.20	50.15		2.87	4.14		
	$\frac{4.32}{4.32}$	$\frac{4.27}{4.27}$	$\frac{4.32}{4.32}$		$\frac{51.60}{51.60}$	$\frac{50.33}{50.33}$		
	S 48.35	48.45	48.50	48.55	$\frac{49.65}{4.82}$	$\frac{49.78}{4.69}$	$\frac{50.00}{4.97}$	$\frac{50.26}{4.21}$
	$\frac{5.12}{5.12}$	$\frac{5.02}{5.02}$	$\frac{5.97}{5.97}$	$\frac{5.92}{5.92}$				
	S 50.55	50.80	50.93		49.45	48.48	48.39	48.35
	$\frac{3.92}{3.92}$	$\frac{3.67}{3.67}$	$\frac{3.34}{3.34}$		$\frac{6.02}{6.02}$	$\frac{6.05}{6.05}$	$\frac{6.04}{6.04}$	$\frac{6.17}{6.17}$

451.36  
3.11  
434.47

$\frac{49.65}{4.82}$

$\frac{49.26}{5.21}$      $\frac{49.27}{5.20}$

$\frac{49.35}{5.12}$      $\frac{49.39}{5.08}$



Alley  
W of College Ave.

54.58

Lindo Paeso Grades

	E.C.	3570 E.C. Alley Ret.	E.C. Alley Ret.	W. line	Indexod C.S.K.
W	50.41	50.72	50.90	51.03	51.00
	4.17	3.86	3.68	3.55	3.58
	4.49	3.98	4.00	4.11	3.88
	-0.32	-0.12	-0.32	-0.54	+0.20
E	50.41	50.72	50.92	50.80	50.77
	4.17	3.86	3.76	3.78	3.81
	4.33	3.96	3.82	3.92	3.55
	-0.16	-0.10	-0.06	0.64	+0.26

Indexod  
C.S.K.

indexod  
C.S.K.

M.H. in Mission Valley Rd. W of Lindo Paeso.

26

N. d.	52.98
	52.31
	52.55
	52.77
	52.82
57.89	
	52.55
	52.77
	5.34
	5.72
	-0.45

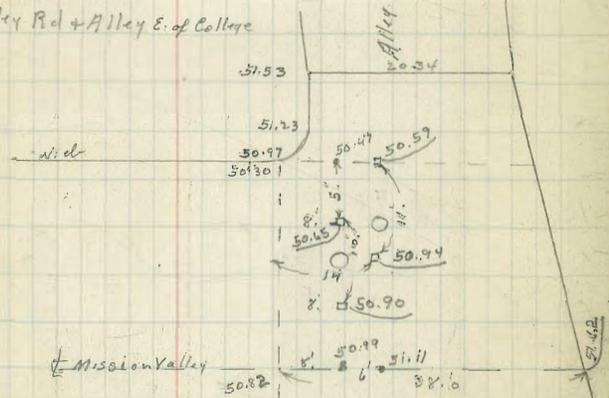
M.H. Stakes

Lindo Paeso & Mission Valley Road.

X 54.58

S.E.	1.51	N.W.	1.84	N.E.	2.69
2.96	3.07	52.70	51.89		
51.42	50.43	50.14	49.96		
50.21	50.43	50.14	49.96		
+0.41	+2.64	+2.56	+1.93		
50.14	50.96				
	50.21				
	50.43				
	50.47				

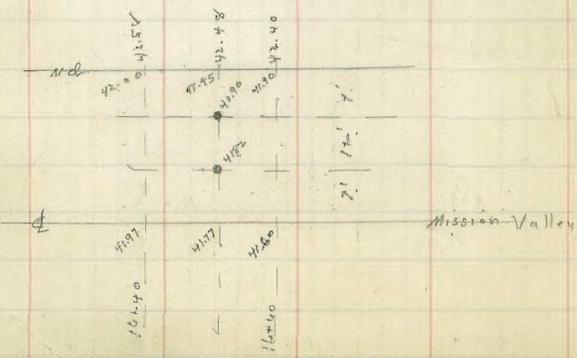
M.H. in Mission Valley Rd + Alley E. of College



Lindo	41.82	41.90
	12.76	12.68
S	12.24	11.51
	+6.52	+1.17

453.22  
1.97  
455.29

M.H. E. of Lindo Paeso









332.25

332.94

5.86

5.39 5.96 5.36

27.60

332.25

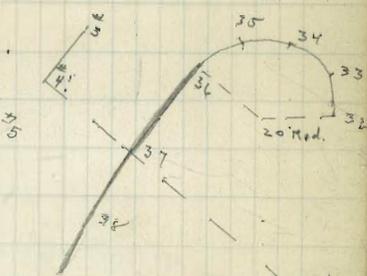
cl. grade gutter Edge Pav +8'

3

30

#14	23.45 85	22.80 25	9.23 23.02	9.14	10.01	10.16 22.80	22.60 25	(47) 23.25
#15	22.60 95	22.00 60	10.00 22.25	9.97	10.94	10.96 22.00	21.75 65	22.40
#16	21.65 80	21.05 60	10.95 21.30	10.93	11.74	11.82 21.14	20.90 65	(48) 21.55
#17 P.R.C.	21.35	20.75 60	11.24 21.01	11.21	12.10	12.13 20.83	20.60 65	(50) 21.25
#18	20.94							

#27	23.19	22.57 62	9.48 22.77	9.43				
#28	23.51	23.86 65	2.20 23.05	9.14				
#29	23.83	23.16 67	8.95 23.30	8.90				
#30	24.13		8.69 23.56	8.60				
#31	24.43	23.70 73	8.40 23.85	8.38				



332.25 H.I.

#19	20.52							
#20 E.C.	20.20 (20.10)	19.30 80	12.85 19.40	12.76				
#21	20.58		12.27 19.98	12.18				
#22	21.05		11.77 20.48	11.70				
#23	21.51		11.20 21.05	11.15				
#24	21.97		10.65 21.60	10.59				
#25	22.43		10.24 22.07	10.18				
#26	22.83		9.82 22.43	9.79				

31	24.43	24.70	25.65	26.60
	7.92	7.55	6.60	5.65
	8.20	8.07	6.50	4.49
	-0.14	-0.52	+0.10	+1.16
	27.80	27.30	26.75	26.15
	4.45	4.95	5.50	6.10
	5.00	5.53	6.40	7.20
	-0.55	-0.58	-0.90	-1.10
	20.94	20.52	20.20	
	11.31	11.73	12.05	
			12.20	
			-0.15	
	23.51	23.83	24.13	
	8.74	8.42	8.12	
	8.90	8.42	8.22	
	-0.06	0.01	-0.10	

2	27.55	28.30	28.55	28.80	28.70	28.50	28.20
	4.70	3.95	3.70	3.45	3.55	3.75	4.05
	3.76	2.64	3.62	3.52	3.96	3.90	4.52
	+0.94	+3.31	+0.08	-0.07	-0.41	-0.15	-0.47
	25.53	24.88	24.20	23.45	22.60	21.65	21.35
	6.72	7.37	8.05	8.80	9.65	10.60	10.90
	7.80	8.44	8.45	9.63	10.65	11.17	11.77
	-1.08	-1.07	-0.40	-0.83	-1.00	-0.57	-0.87
	20.58	21.05	21.51	21.97	22.43	22.83	23.19
	11.67	11.20	10.74	10.28	9.82	9.42	9.06
	11.90	11.20	10.80	10.49	9.82	9.20	8.26
	-0.23	6.0	-0.14	-0.21	0.01	+0.22	-0.20
32	27.30	27.70	28.10	28.50	28.60	28.60	28.80
	5.66	5.16	4.56	4.46	4.26	4.36	4.66
	5.53	5.05	4.86	4.67	4.46	4.46	4.48
	+0.13	+0.21	0.0	-0.21	-0.20	-0.10	+0.18
33	27.10	26.55	25.95	25.33	24.68	24.00	24.00
	5.86	6.41	7.01	7.63	8.28	8.96	8.96
	6.36	6.71	6.67	7.91	8.40	8.93	8.93
	-0.37	-0.30	-0.30	+0.34	-0.28	-0.12	+0.03
34	27.60	27.40	27.25				
	9.71	10.86	11.71				
	9.61	10.00	11.03				
	+0.10	+0.56	+0.68				



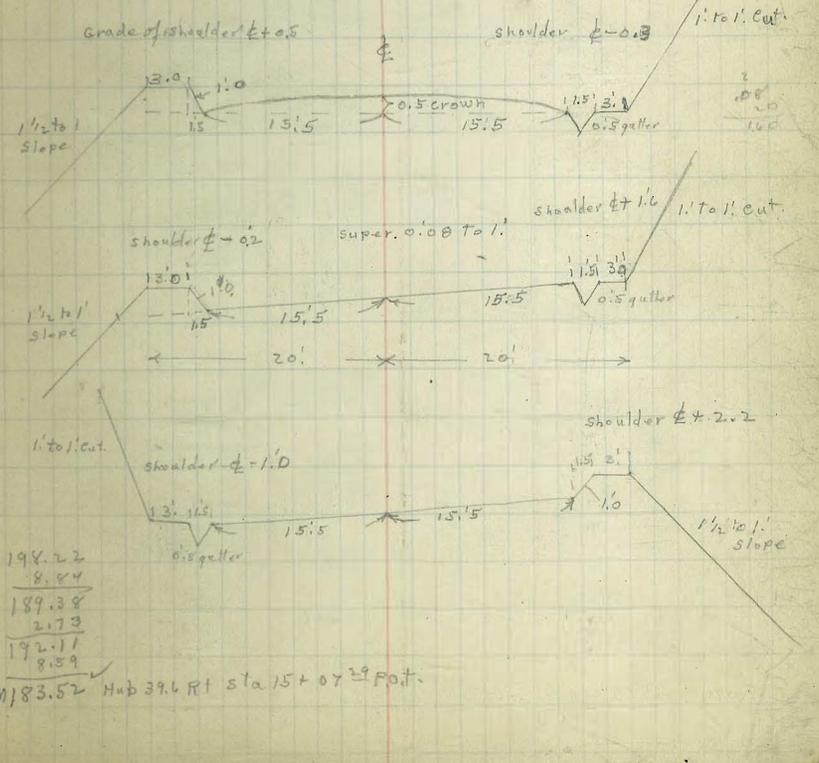
Home Ave. Grades		BM			
0+00	$\begin{array}{r} \pi 229.4 \\ W. Berm \\ 0, \\ \hline 229.6 \\ +0.2 \\ 13.6 \\ \hline -13.8 \end{array}$	229.13	$\begin{array}{r} \pi 229.13 \\ 0.31 \\ \hline 229.44 \\ 12.48 \\ \hline 216.96 \\ 1.04 \\ \hline 217.60 \\ 0.85 \\ \hline 217.05 \\ 13.29 \\ \hline 230.34 \\ 0.42 \\ \hline 229.92 \\ 12.64 \\ \hline \pi 242.60 \\ 0.32 \\ \hline 241.28 \\ 13.32 \\ \hline \pi 255.60 \\ BM 195.57 \\ 2.65 \\ \hline 198.22 \end{array}$	229.13	$\begin{array}{r} 229.13 \\ 0.31 \\ \hline 229.44 \\ 12.48 \\ \hline 216.96 \\ 1.04 \\ \hline 217.60 \\ 0.85 \\ \hline 217.05 \\ 13.29 \\ \hline 230.34 \\ 0.42 \\ \hline 229.92 \\ 12.64 \\ \hline \pi 242.60 \\ 0.32 \\ \hline 241.28 \\ 13.32 \\ \hline \pi 255.60 \\ BM 195.57 \\ 2.65 \\ \hline 198.22 \end{array}$
0+20	$\begin{array}{r} \pi 217.6 \\ \hline 217.6 \end{array}$	228.5			
0+40	$\begin{array}{r} \pi 228.6 \\ +17.0 \\ 3.4 \\ \hline -14.4 \end{array}$	228.1			
0+60	$\begin{array}{r} 227.7 \\ +10.1 \\ 2.3 \\ \hline -12.4 \end{array}$	227.2			
1+00		226.6			
1+20 E.V.C.	$\begin{array}{r} 226.3 \\ +8.7 \\ 2.3 \\ \hline -11.0 \end{array}$	225.8			
Normal Crown.					
1+50	$\begin{array}{r} 224.8 \\ +7.2 \\ 4.0 \\ \hline -13.2 \end{array}$	224.3	224.8		
2+00	$\begin{array}{r} 222.1 \\ +4.5 \\ 9.2 \\ \hline -14.2 \end{array}$	221.8	255.6 222.5 33.1 6.2 +26.9	46.9 out.	
2+50	$\begin{array}{r} 219.5 \\ +1.9 \\ 8.7 \\ \hline -10.6 \end{array}$	219.3	$\begin{array}{r} \pi 255.6 \\ 220.2 \\ 35.4 \\ 5.2 \\ \hline +30.2 \end{array}$	50.2 out.	
2+90 P.C.					
3+00	$\begin{array}{r} 216.9 \\ 0.7 \\ 5.4 \\ \hline -5.2 \end{array}$	216.8	$\begin{array}{r} \pi 242.6 \\ 217.9 \\ 27.7 \\ 6.2 \\ \hline +19.5 \end{array}$	38.5 out.	
3+50	$\begin{array}{r} 214.2 \\ 3.4 \\ 3.4 \\ \hline 0.0 \end{array}$	214.3	$\begin{array}{r} \pi 230.3 \\ 215.7 \\ 14.6 \\ 5.1 \\ \hline +9.5 \end{array}$	29.5 out.	

Rt.			Lt.	
4+00	$\begin{array}{r} 217.6 \\ 6.0 \\ 6.0 \\ 0.0 \end{array}$	211.8	$\begin{array}{r} \pi 230.3 \\ 213.4 \\ 16.9 \\ 14.9 \\ \hline +2.0 \end{array}$	221.0 out.
4+50	$\begin{array}{r} 209.1 \\ 2.5 \\ 9.7 \\ \hline -1.2 \end{array}$	209.3	$\begin{array}{r} \pi 217.6 \\ 211.5 \\ 4.1 \\ 15.1 \\ \hline -9.0 \end{array}$	33.5 out.
5+00	$\begin{array}{r} 206.6 \\ +4.4 \\ 3.1 \\ \hline -11.5 \\ -6.3 \end{array}$	201.4	$\begin{array}{r} 209.0 \\ +7.2 \\ 5.2 \\ \hline -12.4 \end{array}$	38.6 out.
5+50	$\begin{array}{r} 204.1 \\ +2.3 \\ 3.0 \\ \hline -5.3 \end{array}$	204.3	$\begin{array}{r} 206.5 \\ +4.7 \\ 4.4 \\ \hline -9.1 \end{array}$	33.5 out.
6+00	$\begin{array}{r} 201.6 \\ +3.4 \\ 2.4 \\ \hline -3.8 \end{array}$	201.8	$\begin{array}{r} 204.0 \\ +5.8 \\ 3.8 \\ \hline -9.6 \end{array}$	34.4 out.
6+40 P.V.C.	$\begin{array}{r} 199.6 \\ +1.4 \\ 1.6 \\ \hline +3.0 \end{array}$	199.8	$\begin{array}{r} 202.0 \\ +3.8 \\ 2.6 \\ \hline -6.4 \end{array}$	27.6 out.
6+60	$\begin{array}{r} 198.8 \\ 2.1 \\ \hline 198.8 \end{array}$	199.0	$\begin{array}{r} 201.2 \\ 2.2 \\ \hline 201.2 \end{array}$	
6+80	$\begin{array}{r} 198.0 \\ 0.2 \\ 2.2 \\ \hline -2.0 \end{array}$	198.2	$\begin{array}{r} 200.4 \\ +2.2 \\ 2.1 \\ \hline -5.3 \end{array}$	28.0 out.
7+00	$\begin{array}{r} 197.2 \\ 1.0 \\ \hline 197.2 \end{array}$	197.4	$\begin{array}{r} 199.6 \\ +1.4 \\ \hline 199.6 \end{array}$	
7+20	$\begin{array}{r} 196.4 \\ 1.8 \\ 2.6 \\ \hline -0.8 \end{array}$	196.6	$\begin{array}{r} 198.8 \\ +0.6 \\ 3.8 \\ \hline -4.4 \end{array}$	26.6 out.
7+40	$\begin{array}{r} 195.7 \\ -2.5 \\ \hline 195.7 \end{array}$	195.9	$\begin{array}{r} 198.1 \\ 2.2 \\ \hline 198.1 \end{array}$	
7+60	$\begin{array}{r} 195.1 \\ 3.1 \\ 4.9 \\ \hline -1.8 \end{array}$	195.3	$\begin{array}{r} 197.5 \\ 0.7 \\ 5.9 \\ \hline -5.2 \end{array}$	27.8
7+80	$\begin{array}{r} 194.5 \\ \hline 194.5 \end{array}$	194.7	$\begin{array}{r} 196.9 \\ \hline 196.9 \end{array}$	

RL	W.	198.2	Lt.	192.11
		±	±	
8+00	194.0 4.2 5.5 -1.3	194.2	196.4 1.8 7.0 -5.2	
8+20	193.5	193.7	195.9	
8+40 EVC	193.2 5.0 7.1 -2.1	193.4	195.6 2.6 9.8 -6.7	
Normal super 9+00	192.2 6.0 8.7 -2.7	192.4 (+2.2)	194.6 3.6 10.7 -7.1	
9+50	191.6 0.5 2.9 -2.4	191.6 (+1.8)	193.5 1.4 5.2 6.6	
10+00	190.9 (+0.1)	190.8 (+1.5)	192.3 0.7 3.2 -3.4	
10+20 #EC	1.7 3.1 -1.4		1.7 2.0 -0.3	
10+50	190.2 (+0.2)	190.0 (+1.2)	191.2 0.9 4.2 -3.3	
11+00	189.6 (+0.4)	189.2 (+0.8)	190.0 2.1 5.9 -3.8	
Normal Crown	2.5 8.0 -5.5		1.9 2.0 -0.1	
11+50	188.9 (+0.5)	188.4 (+0.5)	188.9 3.2 7.8 -4.6	
12+00	188.1 (+0.6)	187.6	188.1 4.0 8.6 -4.6	
12+50	187.3 (+0.7)	186.8	187.3 4.8 6.9 -2.1	
13+00	186.5 (+0.8)	186.0	186.5 5.6 8.2 -2.6	
13+50	185.7 (+0.9)	185.2	185.7 6.4 9.9 -3.5	

16+00	181.2	192.11	183.5
Ro	±	±	Lt.
14+00	184.9 7.2 11.2 -4.0	184.4	184.9 7.2 9.7 -2.5
14+50	184.1 8.0 11.8 -3.8	183.6	184.1 8.0 10.4 -2.4
15+00	183.3 8.8 9.7 -0.9	182.8	183.3 8.8 11.6 -2.8
15+50	182.5 9.6 12.2 -2.6	182.0	182.5 9.6 14.6 -5.0
16+00	181.7 10.4 12.4 -2.0	181.2	181.7 10.4 14.6 -4.2

76.0 of 1.6 H<sub>2</sub>O Grade



183.77  
7.71  
174.06  
1.19  
177.27

	Rt.	E	Lt.
16400 Brk	181.7 2.7 4.1 -2.0	181.2	181.7
16450	180.8 3.0 5.0 -2.0	180.33	180.8 3.0 5.0 -2.0
17400	180.0 3.8 5.8 -2.0	179.46	180.0 3.8 7.8 -4.0
17450	179.1 4.7 9.4 -4.7	178.60	179.1 4.7 6.3 -1.6
New Brk 18400	178.2 5.4 9.6 -4.0	O.V.K. 177.73 change 177.1 <u>176.87</u>	178.2 5.6 6.6 -1.0
18450	177.4 4.0 2.7 -2.8	176.5 <u>176.0</u>	177.4 4.0 2.9 -3.0
19400 Brk	176.5 0.8 2.9 -2.1	176.5 <u>176.0</u>	176.5 0.8 2.6 -1.8
19450	175.9 1.4 4.8 -3.4	175.9 <u>175.4</u>	175.9 1.4 5.0 -3.6
20400	175.3 2.0 3.6 -1.6	174.8 <u>174.8</u>	175.3 2.0 4.1 -2.1
20450	174.7 2.6 4.7 -2.1	174.8 <u>174.2</u>	174.7 2.6 5.1 -2.5
21400	174.1 3.2 4.9 -1.7	174.3 <u>173.6</u>	174.1 3.2 6.5 -3.8
21450	173.5 3.8 6.2 -2.4	173.7 <u>173.0</u>	173.5 3.8 6.5 -2.7
22400	172.9 4.4 7.3 -2.9	173.2 <u>172.4</u>	172.9 4.4 5.9 -1.5

	Rt.	Lt.
22450	172.3 5.0 9.4 -4.4	172.3 5.0 9.4 -4.4
23400	171.7 5.6 7.1 -3.5	171.7 5.6 7.1 -3.5
23450	171.1 6.2 6.6 -0.4	171.1 6.2 6.6 -0.4
24400 Brk	170.5 6.8 7.1 -0.3	170.5 6.8 7.1 -0.3
24450	169.7 7.6 6.4 +1.2	169.7 7.6 6.4 +1.2
25400	168.9 8.4 6.4 +2.0	168.9 8.4 6.4 +2.0
25450	168.1 0.1 +8.5 above +8.4	168.1 0.1 +8.5 above +8.4
26400	167.3 0.9 1.9 -1.0	167.3 0.9 1.9 -1.0
26450	166.5 1.7 5.1 -3.4	166.5 1.7 5.1 -3.4
27400	165.7 2.5 5.1 -2.6	165.7 2.5 5.1 -2.6
27450	165.0 3.2 5.4 -2.2	165.0 3.2 5.4 -2.2
28400	164.2 4.0 5.9 -1.9	164.2 4.0 5.9 -1.9
28450	163.4 4.8 6.8 -2.0	163.4 4.8 6.8 -2.0

	Rt.	Lt.
172.6	<u>172.6</u>	172.6
172.3	<u>172.3</u>	172.3
172.1	<u>172.1</u>	172.1
171.7	<u>171.7</u>	171.7
171.5	<u>171.5</u>	171.5
170.6	<u>170.6</u>	170.6
change	171.00	171.00
170.00	<u>170.00</u>	170.00
change	170.1	170.1
169.2	<u>169.2</u>	169.2
169.2	<u>169.2</u>	169.2
168.3	<u>168.3</u>	168.3
167.63	<u>167.63</u>	167.63
167.5	<u>167.5</u>	167.5
166.84	<u>166.84</u>	166.84
166.6	<u>166.6</u>	166.6
166.05	<u>166.05</u>	166.05
165.7	<u>165.7</u>	165.7
165.26	<u>165.26</u>	165.26
164.9	<u>164.9</u>	164.9
164.47	<u>164.47</u>	164.47
164.0	<u>164.0</u>	164.0
163.68	<u>163.68</u>	163.68
163.1	<u>163.1</u>	163.1
162.89	<u>162.89</u>	162.89

1.733%

1.2%

33

AT	LT		
29+00	162.3	162.6	167.66
29+50	161.4	161.8	155.27
Normal Crown 30+00	160.52	161.0	159.10
30+50	159.73	160.6	
31+00	158.94	160.1	
31+50	158.15	159.7	
32+00	157.36	159.2	
Full Super 32+50	156.57	158.8	
33+00	155.78	156.7	
33+45 E.C.	155.00	156.5	
33+50			
34+00	154.20	155.3	
34+50	153.41	154.2	

Rt. Berm	Lt. Berm		
Normal Crown 35+00	152.62	53.1	159.10
35+50	151.83	52.3	147.02
36+00	151.04	51.5	146.50
P.V.C. 36+16 84	150.8	51.3	153.53
36+56 84	150.3	50.8	
36+96 84	149.9	50.4	
Equation 37+54.86 = 37+37.97	149.6	50.1	
37+60	149.45	50.0	
38+00	149.55	50.1	
38+40 E.V.C.	149.70	50.2	
75% 39+00	150.15	50.6	

1.57870

1.57870

75%

RT	5.04 152.00	£	LT	153.53
39+50	151.2 2.5 0.4 4.1 2.0 -1.6 2.0 out	150.52	151.0 2.5 2.4 7.6 2.0 -5.1 2.7 out	
40+60 P.V.C.	152.0 5.1 2.3 9.7 2.0 -4.6 2.6 out	150.90	151.6 6.7 2.0 12.1 2.0 -6.0 2.0 out	148.22 8.84 157.06
40+20	152.5	0 Lt 151.25	151.00	
40+40 50 RT 40+43 20 £ 40+45 15 Lt	152.98	2. Edge Pavmt. 151.95	151.00	
40+60 80 15 RT 40+63 20 £ 40+64 20 15 Lt	153.77	152.80	151.90	
40+80 B	154.0 3.1 1.2 5.5 2.0 -2.4 2.6 out	153.20	152.0 5.1 2.4 10.0 2.0 -4.9 2.3	
41+00 B	153.7 3.4 1.2 5.8 2.0 -2.4 2.6 out	153.20	152.7 4.4 2.7 9.9 2.0 -5.5 2.2 out	
41+20 B	153.2 3.9 1.0 5.8 2.0 -1.9 2.9 out	152.70	153.2 3.9 1.3 9.7 2.9 -5.8 2.7 out	
41+60	151.4 3.7 0.7 7.8 2.0 -1.3 2.0 out	150.9	151.4 5.7 1.7 9.0 2.0 -3.3 2.5 out	
42+00	149.5 7.6 0.4 8.4 2.0 -0.8 2.2 out	149.0	149.5 7.6 1.1 9.9 2.0 -2.3 2.3	

RT	£	LT	
42+40	147.7 7.9 0.4 10.2 2.0 -0.8 2.2 out	147.2	147.7 9.4 0.4 10.2 2.0 -0.8 2.2 out
PVC 42+80	145.9 11.2 0.2 11.7 2.0 -0.5 2.0 out	145.35	145.9 11.2 0.2 13.2 2.0 -2.0 2.0 out
43+00		144.50	
43+20	144.2 2.8 0.8 4.8 2.0 -1.6 2.2 out	143.70	144.2 2.8 1.4 5.6 2.0 -2.8 2.2 out
43+40		142.90	
43+60	142.7 4.3 1.4 7.0 2.0 -2.7 2.4 out	142.20	142.7 4.3 1.1 6.5 2.0 -2.2 2.3 out
43+80		141.55	
44+00	141.4 5.6 1.1 8.2 2.0 -2.4 2.4 out	140.90	141.4 5.6 0.9 7.4 2.0 -1.8 2.7 out
44+20		140.35	
44+40	140.3 6.7 1.3 9.3 2.0 -2.6 2.3 out	139.85	140.3 6.7 0.9 8.3 2.0 -1.6 2.4 out
44+60		139.45	
44+80	139.5 7.5 1.3 10.0 2.0 -2.5 2.3 out	139.05	139.5 7.5 0.9 7.5 2.0 0.0 2.0 out
45+00		138.65	

	RT.		Lt.
45+20 E.V.C.	138.7 8.3 6.1 +1.7	138.25	138.7 8.3 7.0 0.7
45+49	138.2 8.8 5.1 +3.7	137.70	138.2 8.8 7.9 -0.9
46+60	137.6 9.4 3.2 +6.3	137.14	137.6 9.4 8.2 -1.2
46+50	136.9 10.1 3.0 +7.1	136.44	136.9 10.1 8.4 +1.7
47+00	136.2 10.8 6.5 +4.3	135.74	136.2 10.8 11.7 -0.9
47+50	135.5 7.0 2.3 -2.5	135.05	135.5 7.0 2.0 -2.5
48+00	134.8 0.4 2.1 -1.7	134.35	134.8 0.4 2.4 -2.0
48+50	134.2 1.0 3.8 -2.8	133.66	134.2 1.0 3.0 -2.0
49+00	133.5 1.7 4.7 -3.0	132.96	133.5 1.7 3.8 -3.1
49+50	133.1 2.0 4.0 -1.9	132.27	132.6 2.6 4.2 -1.6
50+00	132.7 2.5 4.7 -2.2	131.57	131.8 3.4 5.0 -1.6
50+36 RC.			
50+50	132.4 4.2 7.0 -2.8	130.88	131.0 5.6 7.4 -1.8

	RT.		Lt.
51+00	132.0 4.6 7.0 -4.4	130.18	132.0 4.6 7.0 -4.4
51+50	131.7 5.0 2.0 -3.0	129.49	131.7 5.0 2.0 -3.0
52+00	130.7 6.0 7.4 -1.4	128.79	130.7 6.0 7.4 -1.4
52+50	129.6 7.0 6.5 +0.5	128.10	129.6 7.0 6.5 +0.5
53+00	124.6 8.0 7.0 +1.0	127.41	124.6 8.0 7.0 +1.0
53+50	127.5 9.1 3.7 +5.4	126.71	127.5 9.1 3.7 +5.4
54+00	126.5 10.1 0.9 +9.2	126.02	126.5 10.1 0.9 +9.2
54+50	125.6 11.0 0.4 +10.6	125.33	125.6 11.0 0.4 +10.6
55+00	124.7 12.0 5.8 +6.2	124.63	124.7 12.0 5.8 +6.2
55+60B	123.7 18.8 5.0 +13.8	123.80	123.7 18.8 5.0 +13.8
56+00B	123.0 19.4 1.0 +18.4	123.25	123.0 19.4 1.0 +18.4
56+40B	122.6 19.8 2.8 +17.0	122.75	122.6 19.8 2.8 +17.0
57+00	121.8 20.6 13.0 +7.6	122.04	121.8 20.6 13.0 +7.6

37

136.64
1.10
135.54
6.91
142.45
13.00
129.45
0.58
130.00

RT	LT		LT
57+50	121.3 8.7 2.1 +5.9	21.9 out 25.9 out	121.46 123.7 6.3 10.7 -4.4
58+00	120.8 9.2 6.0 +3.2	23.2 out 23.2 out	120.89 123.1 6.9 10.9 -4.0
Full Super +50	120.1 9.9 6.1 +3.1	23.1 out	120.32 122.5 7.5 11.8 -4.3
59+00	119.7 10.3 11.3 -1.0	21.5 out 21.5 out	119.74 121.6 8.4 12.1 -3.7
+50 +53 <sup>24</sup> PC	119.2 10.8 14.5 -3.7	25.5 out	119.16 120.6 9.4 13.1 -3.7
60+00	118.8 5.6 8.6 -3.0	24.5 out	118.58 119.7 7.7 8.4 -3.7
+50	118.3 6.1 7.1 -3.0	24.5 out	118.00 119.8 5.6 7.4 -3.8
Normal Crown 61+00	117.9 6.5 6.5 0.0	24.0 out	117.43 117.9 6.5 9.0 -2.5
+50	117.4 7.0 7.6 -0.6	20.5 out	116.86 117.4 7.0 9.6 -2.6
62+00	116.8 7.6 7.6 0.0	20.1 out	116.28 116.8 7.6 10.6 -3.0
+50	116.2 8.2 5.4 +2.8	22.4 out	115.70 116.2 8.2 11.6 -3.4
63+00	115.6 10.0 8.3 +7.7	21.7 out	115.12 115.6 10.0 10.4 -0.4
+50	115.0 10.6 5.6 +5.0	25.0 out	114.54 115.0 10.6 9.6 +1.0

RT	LT		LT
64+00	114.5 11.1 7.6 +3.5	23.5 out	114.5 11.1 7.6 +1.5
+50	113.9 11.7 4.2 +3.5	23.5 out	113.40 113.9 11.7 11.7 -0.2
65+00	113.3 12.3 11.8 +2.7	22.9 out	112.82 113.3 12.3 11.8 +0.8
+50	112.7 12.9 8.4 +4.5	24.5 out	112.24 112.7 12.9 11.1 +1.8
Normal Crown 66+00	112.1 13.5 8.1 +5.4	25.4 out	112.1 112.1 13.5 11.5 +2.0
+50	111.7 9.3 8.0 +7.3	27.3 out	112.10 111.7 9.3 9.6 -0.3
67+00	111.2 9.8 7.8 +8.0	28.0 out	111.63 111.2 9.8 7.8 0.0
+50	110.8 10.2 3.7 +7.1	27.1 out	111.17 110.8 10.2 9.2 +2.0
68+00	110.3 10.7 5.4 +5.3	25.3 out	110.70 110.3 10.7 11.0 -0.3
+50	109.8 11.2 7.8 +3.4	23.4 out	110.23 109.8 11.2 14.5 -3.3
Normal Crown 69+00	109.4 11.6 10.3 +1.3	21.3 out	109.76 109.4 11.6 14.0 -2.4
+50	109.1 11.9 11.6 +0.3	20.9 out	109.30 108.9 12.1 12.1 0.0
70+00	108.8 4.6 4.1 +0.5	20.5 out	108.82 108.5 4.6 5.4 -0.5

124.42  
8.93

2 Hub  
67+23.28  
P.E.

RT Chk Lt.  
112.1 112.5 112.1  
8.9 8.5 8.9  
3.5 9.3 6.9  
+5.4 0.8 1.0

Hub at PC 67+23.28  
125.56  
10.07  
115.49

67+23.28  
RM. 42 RT. 110  
119.87  
11.8  
121.00  
9.32  
T.P. 111.68  
Ho. RR Tr. out.  
69+85 26 P.C.

111.66  
112.56

RT

LT

RT

LT

113.41

70+50 108.5  
 4.9  
 4.1  
 +0.8  
 Full Super

108.35 108.0  
 5.4  
 5.6  
 -0.2  
 20.3 out

71+00 108.2  
 5.2  
 1.6  
 +3.6  
 23.6 out

107.88 107.6  
 5.8  
 9.4  
 -3.6  
 25.6 out

+50 107.7  
 5.7  
 2.4  
 +3.3  
 23.3 out

107.41 107.1  
 6.3  
 9.5  
 -3.2  
 24.8 out

72+00B 107.2  
 6.2  
 2.9  
 +3.3  
 23.3 out

106.94 106.6  
 6.8  
 8.8  
 -2.0  
 23.0 out

+50B 106.7  
 6.7  
 3.4  
 +3.3  
 23.3 out

106.42 106.1  
 7.3  
 7.7  
 -0.4  
 20.6 out

73+00B 106.1  
 7.3  
 5.4  
 +1.9  
 21.9 out

105.80 105.5  
 7.4  
 7.0  
 +0.9  
 20.9 out

+50B 105.4  
 8.0  
 5.9  
 +2.1  
 22.1 out

105.09 104.8  
 8.5  
 7.9  
 +0.7  
 20.7 out

74+00B 104.6  
 8.8  
 6.0  
 +2.8  
 22.8 out

104.27 104.0  
 9.4  
 9.9  
 -0.5  
 20.7 out

+50 103.7  
 9.7  
 7.3  
 +2.4  
 22.4 out

113.41  
 7.27  
 106.14  
 0.46  
 106.60

103.39 103.1  
 10.3  
 12.7  
 -2.4  
 23.6 out

75+00 102.8  
 3.8  
 2.0  
 +1.8  
 21.8 out

102.53 102.2  
 4.4  
 7.4  
 -2.7  
 21.3 out

+50 102.0  
 4.6  
 4.3  
 +0.3  
 20.3 out

101.66 101.4  
 5.2  
 8.5  
 -3.3  
 21.6 out

76+00 101.1  
 5.8  
 5.8  
 -0.3  
 20.5 out

100.80 100.5  
 6.1  
 9.9  
 -2.8  
 21.4 out

+50 100.2  
 6.4  
 6.2  
 +0.2  
 20.2 out

99.92 99.6  
 7.0  
 10.0  
 -3.0  
 24.5 out

77+00 97.4  
 7.0  
 7.0  
 -0.8  
 21.2 out

106.60  
 9.73  
 96.87  
 2.54  
 99.41

99.06 98.8  
 7.8  
 11.5  
 -3.7  
 25.5 out

+50 98.5  
 8.1  
 4.4  
 +3.7  
 22.7 out

98.20 97.9  
 8.7  
 8.1  
 +0.6  
 20.6 out

78+00 97.6  
 9.0  
 6.8  
 +2.2  
 22.2 out

97.34 97.0  
 9.6  
 11.9  
 -2.3  
 23.7 out

Full Super +50 96.8  
 9.8  
 9.0  
 +0.8  
 20.8 out

96.47 96.2  
 10.4  
 13.0  
 -2.6  
 23.0 out

79+00 95.7  
 3.7  
 3.7  
 0.0  
 20.0 out

99.41

95.61 95.30  
 4.1  
 5.7  
 -1.6  
 22.4 out

+50 94.7  
 4.7  
 7.9  
 +3.2  
 23.2 out

94.74

94.74 94.40  
 5.0  
 9.2  
 -4.2  
 26.5 out

80+00 93.6  
 5.8  
 5.6  
 +0.2  
 20.2 out

Normal Growth

93.44

93.44 93.50  
 5.9  
 10.9  
 -5.0  
 22.5 out

+50 92.60  
 6.8  
 12.2  
 -5.4  
 3.7  
 28.1

93.02

92.60 92.60  
 6.8  
 10.2  
 -3.4  
 25.1 out

Rt

±

Lt

π  
99.41

81+00  
 91.8  
 7.6  
 13.8  
 -6.2  
 29.8 out  
 3.1

+50  
 90.9  
 8.5  
 11.5  
 -3.0  
 4.5 out  
 2.1

11.46  
 2.54  
 90.49  
 5.84  
 84.65  
 1.26  
 85.91

92.16  
 91.30  
 POT. Hab.

91.8  
 7.6  
 10.2  
 -2.6  
 23.9 out  
 1.3

90.9  
 8.5  
 14.3  
 -5.8  
 2.9  
 28.7

82+00  
 90.0  
 0.5  
 4.1  
 -3.6  
 2.8 out  
 2.54 out

+50  
 89.2  
 7.3  
 5.4  
 -4.4  
 2.6 out  
 2.54 out

90.44  
 89.57

90.0  
 0.5  
 5.4  
 -4.9  
 2.4  
 27.3 out

89.2  
 7.3  
 5.4  
 -5.0  
 2.7 out  
 2.54 out

83+00  
 88.3  
 2  
 5.1  
 -2.8  
 2.8 out  
 2.42 out

+50  
 87.4  
 3.1  
 7.1  
 -4.0  
 2.4 out  
 2.4 out

88.71  
 87.85

88.3  
 2.2  
 6.4  
 -4.6  
 2.3  
 2.7 out

87.4  
 3.1  
 4.4  
 -1.3  
 0.7  
 2.0 out  
 2.4 out

84+00  
 84.6  
 3.9  
 6.2  
 -2.6  
 2.3  
 2.3 out  
 2.39 out

+50  
 85.7  
 0.2  
 1.4  
 -1.2  
 2.1 out  
 2.39 out

85.91

86.98  
 86.12

84.6  
 3.9  
 5.3  
 -1.4  
 2.1 out  
 2.1 out

85.7  
 0.2  
 1.6  
 -1.4  
 2.2 out  
 2.2 out

85+00  
 84.9  
 1.0  
 2.5  
 -1.5  
 0.7  
 2.2 out  
 2.2 out

+50  
 84.0  
 1.9  
 2.9  
 -1.0  
 2.15 out  
 2.2 out

85.26  
 84.39

84.9  
 1.0  
 2.5  
 -1.5  
 2.2 out  
 2.2 out

84.0  
 1.9  
 2.2  
 -1.3  
 2.10 out  
 2.2 out

Rt.

Lt.

85.91

86+00  
 83.1  
 2.8  
 3.6  
 -0.8  
 2.02 out  
 2.02 out

+50  
 82.3  
 3.6  
 7.6  
 -4.0  
 2.0 out  
 2.0 out

83.53

82.47

83.7  
 2.8  
 4.2  
 -1.4  
 2.1 out  
 2.1 out

82.3  
 3.6  
 4.6  
 -1.0  
 2.15 out  
 2.1 out

5.4  
 4.4  
 2.0

Change Page 42.

87+00  
 81.4  
 4.5  
 5.6  
 -1.1  
 2.6 out  
 2.6 out

+50  
 80.5  
 5.4  
 5.4  
 0.0  
 2.0 out  
 2.0 out

81.80

80.94

81.4  
 4.5  
 5.6  
 -4.1  
 2.6 out  
 2.6 out

80.5  
 5.4  
 7.3  
 -1.7  
 2.8 out  
 2.8 out

85.91

88+00 B  
 79.7  
 0.2  
 5.2  
 +1.0  
 2.1 out  
 2.1 out

+50 B  
 78.9  
 7.0  
 1.8  
 +5.2  
 2.52 out  
 2.52 out

80.08

79.28

79.7  
 0.2  
 7.8  
 -1.5  
 2.24 out  
 2.24 out

78.9  
 7.0  
 9.4  
 -2.4  
 2.52 out  
 2.52 out

	R+	£	L+
		85.91	
		9.95	
89+00 B	78.2	75.96	78.63
	7.7	4.04	7.7
	7.1	80.04	8.9
	10.6	9.74	-1.2
+50 B	77.7	70.30	77.7
	8.2	20.32	8.2
	8.2		10.2
	0.0		-2.0
90+00 B	77.3	77.73	77.3
	2.7		2.7
	3.1		5.9
	-0.4		-3.2
90+50	77.0	77.42	77.0
	3.0		3.0
	4.0		6.8
	-1.0		-3.3
91+00	76.7	77.11	76.7
	3.3		3.3
	4.7		5.3
	-1.4		-2.0
+50	76.4	76.80	76.4
	3.6		3.6
	5.5		5.2
	-1.9		-2.6
92+00	76.1	76.49	76.1
	3.9		3.9
	4.5		6.3
	-2.4		-2.4
+50	75.8	76.18	75.8
	4.7		4.7
	7.3		7.5
	-3.1		-3.3
93+00	75.5	75.87	75.5

Change Page 42

End Bndzort  
93+25 63

End Bridge  
93+40 £

End Bridgeort  
93+54 37

94+36<sup>75</sup> Medgeparnt. on £ 95.02

0.02%

94+36<sup>75</sup> Pav £ 75.02

94+56.42 Pav 73.90

24+75

New Channel Home Ave

1-7-33  
Walker  
Bless

	4.5	114 15+07 29.
	189.3	
7+50	187.3	183.52
	8.7	10.30
	6.3	193.82
	+2.4	
8+00	186.6	
	9.4	
	5.6	
	+3.8	
8+50	185.9	
	10.1	
	7.0	
	+3.1	
9+00	185.1	
	10.9	
	7.1	
	+3.8	187.89
		1.89
9+50	184.4	186.00
	11.6	10.03
	8.0	196.03
	+3.6	
10+00	183.7	
	12.3	
	8.0	
	+4.3	
10+50	183.0	
	13.0	
	9.8	
	+3.5	
11+00	182.2	
	13.8	
	10.0	
	+3.8	
x 100' 15' Rf		
11+50	181.4	
of Ditch 155'	6.5	
S. of Home	1.5	
	+5.0	

Grade

New Sta 25+37 25  
old Sta 25+12 17  
43

12+00	180.7		18+50	171.0	179.43
	7.2			8.9	0.43
	3.5			3.8	179.86
	+3.7			+5.1	1.51
12+50	180.0		19+00	170.2	178.35
	7.9			9.7	9.54
	4.4			5.8	187.89
	+3.5			+4.7	
13+00	179.2		19+50	169.4	
	8.7			10.5	
	5.7			5.7	
	+3.0			44.8	
13+50	178.5		20+00	170.7	
	9.4			16.7	
	5.3			11.2	
	+4.1			6.2	
14+00	177.7		20+50	167.9	
	10.2			12.0	
	5.9			6.8	
	+4.3			+5.2	
14+50	177.0		21+00	167.1	
	10.9			12.8	
	5.5			7.3	
	+5.4	15.8		+5.5	
15+00	176.3	178.3	21+50	166.3	
	11.6	17.3		13.6	
	6.0			7.3	
	+5.6			+6.3	
15+50	175.5		22+00	165.5	
	12.4			14.4	
	5.8			4.2	
	+6.6			+9.6	
16+00	174.6		22+50	164.7	
	13.3			15.2	
	5.3			4.8	
	+8.0			+10.4	
16+50	173.8		23+00	163.9	
	14.1			16.0	
	4.9			7.3	
	+9.2			+8.7	
17+00	173.1		23+50	163.1	
	14.8			16.8	
	6.7			8.6	
	+8.1			+8.2	
17+50	172.3		24+00	162.3	
	15.6			17.6	
	9.0			11.5	
	+6.6			+6.1	
18+00	171.7		24+25 Bank		
	9.2				
	2.1				
	+6.1		24+50 Wash.	161.4	
			of Ditch 155' E.	18.5	
			of Home.	15.5	
				+3.0	

163.91 Hub sta 30+85.27

4.47  
128.38  
2.07

p.c.

31+51.62

25+00 160.7  
6.8  
3.2  
+3.0

144.31  
1.21  
-167.52

151.6  
15.9  
11.7  
+4.2

25+50 160.6  
7.5  
2.0  
+4.9

11.24  
156.28  
3.25  
159.53

32+00

150.9  
16.6  
12.1  
+4.5

24+00 159.3  
8.2  
2.0  
+6.2

32+50 159.3  
8.2  
2.0  
+6.2

150.2  
9.3  
5.5  
+3.8

26+50 158.6  
8.9  
4.0  
+4.9

33+00 158.6  
8.9  
4.0  
+4.9

149.6  
9.9  
7.0  
+2.9

33+45 358.c.

27+00 157.9  
9.4  
4.9  
+4.7

33+50 157.9  
9.4  
4.9  
+4.7

148.8  
10.7  
5.5  
+5.2

27+60 157.2  
10.3  
5.2  
+5.1

34+00 157.2  
10.3  
5.2  
+5.1

148.0  
11.5  
7.0  
+4.5

28+00 156.5  
11.0  
6.4  
+3.4

34+50 156.5  
11.0  
6.4  
+3.4

147.2  
12.3  
6.9  
+5.4

28+50 155.8  
11.7  
8.4  
+3.1

35+00 155.8  
11.7  
8.4  
+3.1

146.4  
13.1  
6.8  
+6.3

29+00 155.1  
12.4  
6.8  
+5.6

35+50 155.1  
12.4  
6.8  
+5.6

145.6  
13.9  
9.0  
+4.9

29+50 154.4  
13.1  
7.6  
+5.5

36+00 154.4  
13.1  
7.6  
+5.5

144.8  
14.7  
11.0  
+3.7

30+00 153.7  
13.8  
8.1  
+5.7

36+50 153.7  
13.8  
8.1  
+5.7

144.0  
15.5  
10.3  
+5.2

30+50 153.0  
14.5  
9.4  
+5.1

37+00 153.0  
14.5  
9.4  
+5.1

143.2  
16.3  
12.2  
+4.1

31+00 152.3  
15.2  
9.3  
+5.9

37+50 152.3  
15.2  
9.3  
+5.9

142.4  
6.6  
0.0  
+6.6

149.6

B.M. 148.22 Rev Culvert

10.6 Fairmont

137.6

41

38+00 141.6  
7.4  
3.0  
+4.4

148.22  
0.90  
149.02

41+00 132.8  
7.3  
4.6  
+2.7

str Bed  
+50

132.2  
7.9  
6.6  
+1.3

148.22  
2.02  
150.24  
12.78  
137.46  
2.66  
140.12

38+50 140.8  
8.2  
3.0  
+4.5

39+00 140.0  
9.0  
6.6  
+2.4

45+00 131.6  
8.5  
5.9  
+2.6

39+50 139.2  
9.9  
8.3  
+1.5

+50 131.0  
9.1  
6.5  
+2.6

40+00 138.4  
10.6  
9.0  
+1.6

46+00 130.4  
9.7  
7.0  
+2.7

40+35 137.8  
11.2  
7.7  
+1.5

+50 129.7  
10.4  
8.3  
+2.1

E. Apron  
40+50 137.6  
11.4

47+00 129.0  
11.1  
8.7  
+2.4

Fairmont Ave Bridge 150.24

W. Apron  
41+12. 136.5  
13.7

+50 128.3  
11.8  
6.9  
+4.9

str Bed  
41+50 135.9  
14.3  
13.1  
+1.2

48+00 127.6  
12.5  
7.1  
+5.4

42+00 135.2  
15.0  
12.6  
+2.4

+50 126.9  
13.2  
10.6  
+2.6

5+B. 12.0

+50 134.6  
15.6  
6.3  
+9.3

49+00 126.2  
13.9  
10.9  
+3.0

43+00 134.0  
16.2  
10.1  
+5.7

+50 125.6  
14.5  
9.6  
+4.9

+50 133.4  
16.8  
13.8  
+3.0

140.12

50+00  $\frac{125.0}{15.0}$   $\frac{140.12}{10.37}$  56+00  $\frac{117.6}{10.5}$   $\frac{126.10}{2.02}$

$\frac{11.0}{+4.1}$  ✓  $\frac{129.75}{2.21}$   $\frac{8.3}{+2.2}$  ✓  $\frac{128.12}{12.35}$

+50  $\frac{124.4}{7.6}$  131.96 57+00  $\frac{116.9}{11.2}$  +50  $\frac{116.9}{11.2}$   $\frac{115.77}{3.50}$

$\frac{3.2}{+4.3}$  ✓  $\frac{123.8}{8.2}$  58+00  $\frac{116.2}{11.9}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{5.4}{+2.8}$  ✓  $\frac{123.2}{8.8}$  59+00  $\frac{116.2}{11.9}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{5.3}{+3.5}$  ✓  $\frac{122.6}{9.4}$  60+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

52+00  $\frac{122.6}{9.4}$  61+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{4.5}{+4.9}$  ✓  $\frac{122.0}{10.0}$  62+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

+50  $\frac{122.0}{10.0}$  63+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{5.0}{+5.0}$  ✓  $\frac{121.4}{10.6}$  64+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

53+60  $\frac{121.4}{10.6}$  65+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{5.5}{+5.1}$  ✓  $\frac{120.8}{11.2}$  66+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

+50  $\frac{120.8}{11.2}$  67+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{5.8}{+5.4}$  ✓  $\frac{120.8}{11.2}$  68+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

54+00  $\frac{120.8}{11.2}$  69+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{6.5}{+5.3}$  ✓  $\frac{119.6}{9.5}$  70+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

+50  $\frac{119.6}{9.5}$  71+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{3.8}{+5.7}$  ✓  $\frac{119.0}{9.1}$  72+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

55+00  $\frac{119.0}{9.1}$  73+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{2.0}{+2.1}$  ✓  $\frac{118.3}{9.8}$  74+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

+50  $\frac{118.3}{9.8}$  75+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

$\frac{7.4}{+2.4}$  ✓  $\frac{118.3}{9.8}$  76+00  $\frac{115.5}{12.6}$  +50  $\frac{115.5}{12.6}$   $\frac{119.27}{3.50}$

67+00  $\frac{109.0}{10.3}$   $\frac{119.27}{12.65}$  68+00  $\frac{100.4}{8.5}$

$\frac{5.6}{+4.7}$  ✓  $\frac{106.62}{2.25}$   $\frac{61}{+2.4}$  ✓

Δ 6-00 Rt. +50  $\frac{108.2}{11.1}$  Δ Rt +65  $\frac{99.5}{9.4}$  108.87

$\frac{5.9}{+5.2}$  ✓  $\frac{101.97}{3.95}$

63+00  $\frac{107.5}{11.8}$  69+00  $\frac{99.0}{6.9}$  105.92

$\frac{6.4}{+5.4}$  ✓  $\frac{98.6}{7.3}$

+50  $\frac{106.7}{12.6}$  +50  $\frac{98.6}{7.3}$

$\frac{8.2}{+4.4}$  ✓  $\frac{97.2}{2.2}$  ✓

64+00  $\frac{106.0}{13.3}$  70+00  $\frac{97.2}{7.7}$

$\frac{7.7}{+5.6}$  ✓  $\frac{97.2}{7.7}$

+50  $\frac{105.3}{14.0}$  +50  $\frac{97.2}{7.7}$

$\frac{9.0}{+5.0}$  ✓  $\frac{97.2}{7.7}$

65+00  $\frac{104.6}{14.7}$  71+05  $\frac{97.4}{8.5}$  7.1

$\frac{10.1}{+4.6}$  ✓  $\frac{97.4}{8.5}$  78.8

+50  $\frac{103.9}{15.4}$  +50  $\frac{97.0}{8.1}$

$\frac{16.2}{+5.2}$  ✓  $\frac{97.0}{8.1}$

66+00  $\frac{103.2}{16.1}$  72+00  $\frac{96.6}{9.3}$

$\frac{13.3}{+2.8}$  ✓  $\frac{96.6}{9.3}$

+50  $\frac{102.5}{16.8}$  +50  $\frac{96.2}{9.7}$

$\frac{12.9}{+4.0}$  ✓  $\frac{96.2}{9.7}$

67+00  $\frac{101.8}{17.1}$  73+00  $\frac{95.8}{10.1}$

$\frac{4.6}{+2.5}$  ✓  $\frac{95.8}{10.1}$

+50  $\frac{101.4}{17.8}$  +50  $\frac{95.4}{10.5}$

$\frac{5.7}{+2.6}$  ✓  $\frac{95.4}{10.5}$

6.4  
102.5

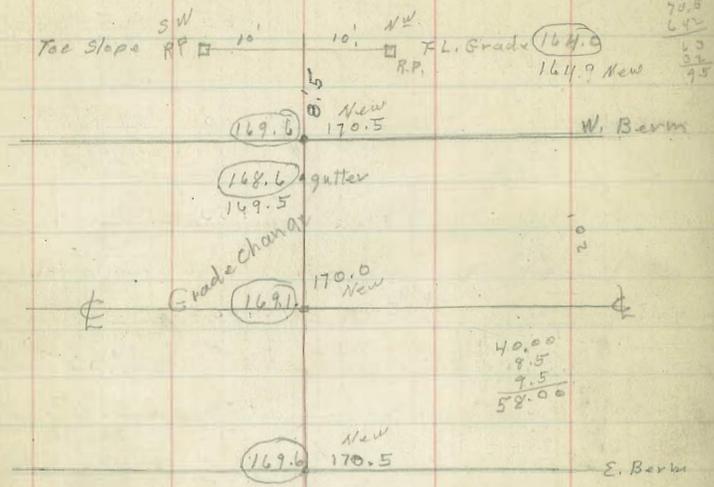
74+00  $\frac{95.4}{10.5}$  +85  $\frac{95.1}{10.8}$  10.3

$\frac{8.5}{+2.0}$  ✓  $\frac{95.1}{10.8}$  95.6

$\frac{7.5}{+2.6}$  ✓  $\frac{95.1}{10.8}$

+0.5

Culvert # 4 3x4 Box.  
 at 90° 00' at sta 24+55  
 B.M. P.O. H&P 0.22 179.65 179.43  
 T.P. 4.58 175.73 8.50 171.15

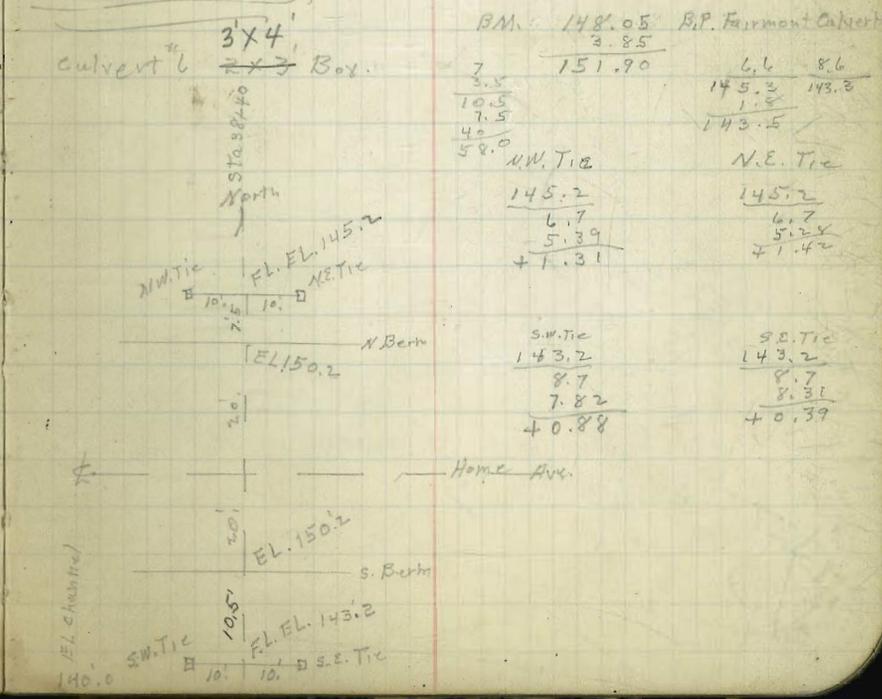


Toe Slope SW RP 10' 10' NW F.L. Grade 164.9 New  
 169.6 New 170.5 W. Berm  
 148.6 gutter  
 149.5  
 170.0 New  
 169.1 Grade Change  
 40.00  
 9.5  
 7.5  
 52.00  
 170.5 New E. Berm  
 9.5 N.E.  
 Toe Slope RP 10' 10' F.L. Grade 163.3  
 164.2 New  
 173.49  
 New Grade  
 SW RP. NW RP  
 164.90 164.90  
 8.59 10.39  
 2.34 7.06  
 6.20 +3.33  
 10.5 B. RP. 10. N.E. RP  
 163.3 163.3  
 12.00 164.20  
 6.56 11.10  
 5.44 +5.40 6.6 4.50  
 +4.54

Inlake  
 175.29  
 10' SW RP 10' NW RP  
 164.0 164.0  
 17.29 11.29  
 4.29 7.06  
 +7.00 +4.23  
 outlet  
 10.5 B. RP. 10. N.E. RP  
 163.3 163.3  
 12.00 164.20  
 6.56 11.10  
 5.44 +5.40 6.6 4.50  
 +4.54

164.20  
 9.29  
 4.29  
 4.54  
 164.90  
 3.33  
 169.23  
 5.21  
 173.49

Culverts. 3x4 BOX  
 # 13 sta 79+77 ~~13~~ Pipe  
 Culvert # 1 sta 5+82.5 4x4 Box staked 1/1/32 PAGE 31  
 # 2 15+50 24" Pipe staked 1/25/33 " 47  
 # 3 23+00 24" Pipe " 1/25/33 " 47  
 # 4 24+55 3x4 Box Restaked 1/24/33 " 46  
 # 5 29+00 24" Pipe staked 1/24/33 " 47  
 # 6 38+40 2x3 Box staked 1/24/33 " 46  
 # 7 44+50 24" Pipe staked 1-24-33 " 47  
 # 8 50+50 18" Pipe staked 2-24-33 " 48  
 # 9 55+00 18" Pipe " 2-33 " 48  
 # 10 64+20 3x4 Box staked 2-18-33 " 48  
 # 11 73+50 ~~24" Pipe~~ staked 5/24/33 " 53  
 # 12 77+15 18" Pipe " 73 77+77 3x4 Box " 53  
 # 14 86+76.5 18" Pipe " 53



BM. 148.05 R.P. Fairmont Culvert  
 3.85  
 151.90  
 3.5  
 10.5  
 7.5  
 4.0  
 59.0  
 NW Tie NE Tie  
 145.2 145.2  
 6.7 6.7  
 5.39 5.24  
 +1.31 +1.42  
 SW Tie SE Tie  
 143.2 143.2  
 8.7 8.7  
 7.82 8.31  
 +0.88 +0.39  
 Home Ave.  
 EL. 150.2 N. Berm  
 EL. 150.2 S. Berm  
 EL. 143.2 SW Tie SE Tie

1-24-33

Culvert #5 24" Pipe

Sta 29+00

± Grade 162.3

Berm " 162.8

25.7  
27.2  
52.9

24.5  
23.9  
48.4  
4.3

B.M. 163.91 P.O.T. Hub Sta 30+70.2

165.83

NW.Tie

159.0  
6.83  
5.96  
+0.87

SW.Tie

158.0  
7.83  
6.04  
+1.75

NE.Tie

159.0  
6.23  
4.42  
+2.41

SE.Tie

158.0  
7.83  
5.30  
+2.53

Culvert #2

Sta. 15+50

24" pipe  
18" X 30" BOX

47

B.M. 183.46 P.O.T. High V. Line 15+07.29

186.42

channel  
4.6  
78.0

182.5 Berm

182.5

SW.Tie

NW.Tie

181.5 gutter

178.7

3.8

178.70

182.0 ±

1.9

5.7

8.12

182.5 Berm

182.5

4.21

7.18

182.5

177.7

+1.91

+0.94

182.5

4.8

5.7

SE.Tie

182.5

7.2

40

NE.Tie

182.5

5.7

178.00

178.00

182.5

40

8.82

8.82

182.5

52.9

8.64

7.37

182.5

39.6

+0.14

+1.45

182.5

25.7

13.9

178.00

182.5

32.9

66.8

8.82

182.5

66.8

178.00

7.37

182.5

175.5

178.00

+1.45

182.5

175.5

178.00

178.00

182.5

175.5

178.00

178.00

182.5

175.5

178.00

178.00

182.5

175.5

178.00

178.00

182.5

175.5

178.00

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182.5

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178.00

178.00

182.5

175.5

178.00

178.00

182.5

175.5

178.00

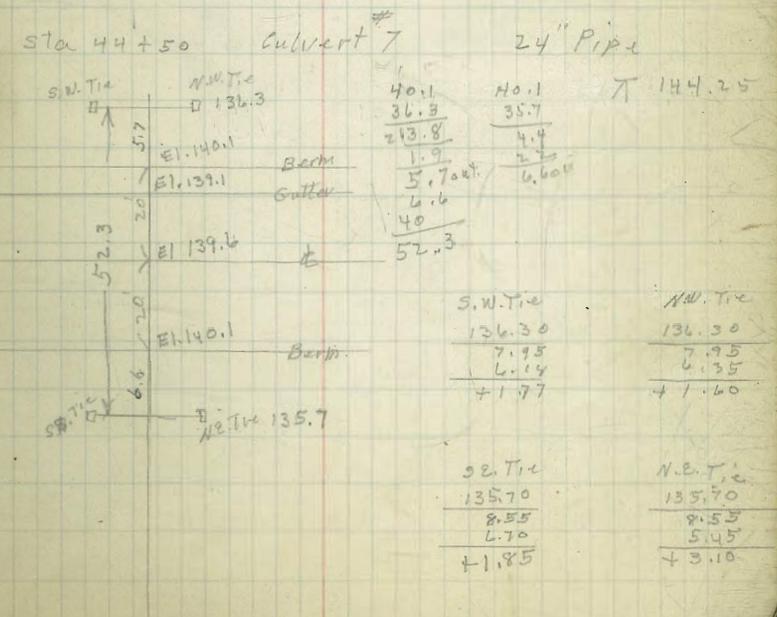
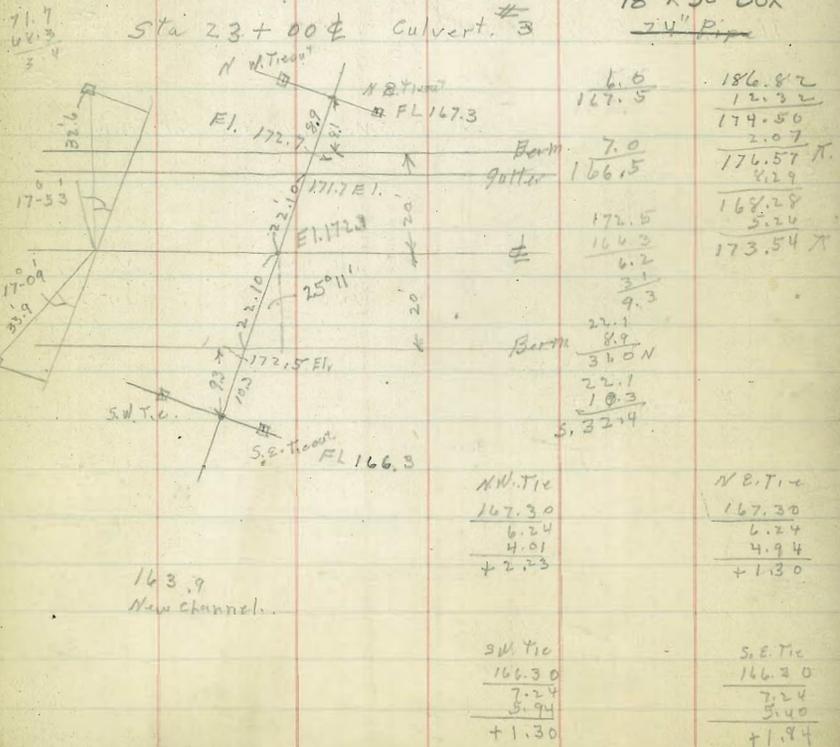
178.00

182.5

175.5

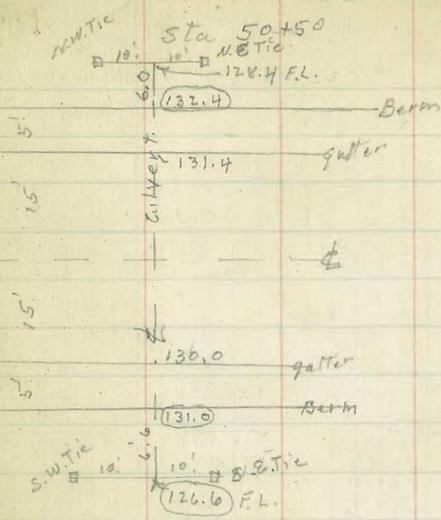
178.00

178.00



Culvert #8

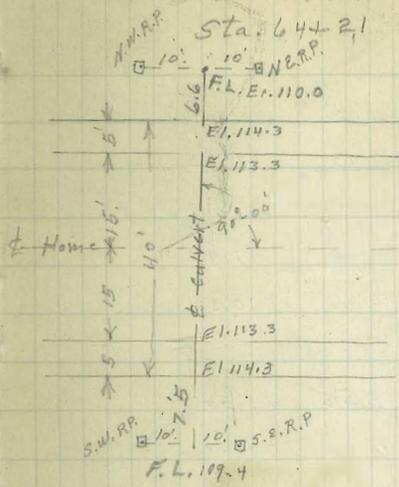
4.5 1286  
 29.7  
 131.4  
 130.4  
 128.4



1.8" Pipe	128.28	4.82	133.10
N.W. Tie	128.40	4.70	133.10
S.W. Tie	126.60	6.50	133.10
Berm	130.0	3.87	133.87
S.E. Tie	126.60	3.61	130.21

Culvert #10 3'x4' BOX

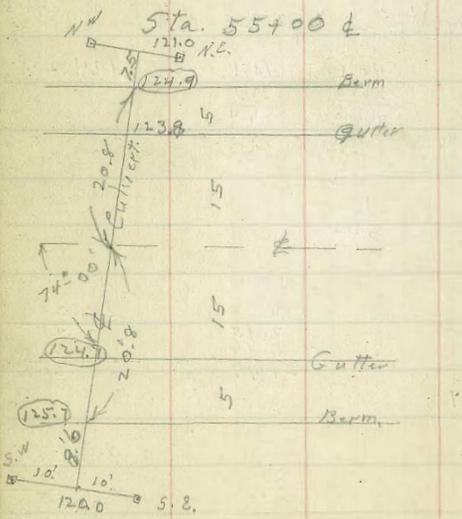
48



N.W. Tie	110.00	1.49	111.49
N.E. Tie	110.00	3.85	113.85
S.W. Tie	109.40	12.09	121.49
S.E. Tie	109.40	8.45	117.85

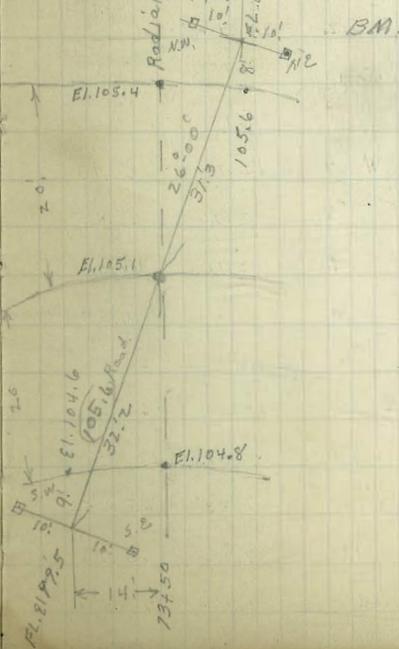
Culvert #9

18" Pipe



18" Pipe	123.8	2.08	125.88
N.W. Tie	121.00	13.31	134.31
S.W. Tie	120.00	14.31	134.31
Berm	120.00	12.13	132.13
S.E. Tie	120.00	11.61	131.61

Culvert #11 24" PIPE 3'x4' BOX



N.W. Tie	100.50	10.66	111.16
N.E. Tie	100.50	4.46	104.96
S.W. Tie	99.50	11.66	111.16
S.E. Tie	99.50	6.93	106.43

con Page 53



6<sup>th</sup> Ave Pavmt Grades Indexed  
 Upas. To 21st c.s.k.

289.07 B.M. S.W. 6<sup>th</sup> & Upas.

5.97  
 295.04  
 6.29  
 288.75  
 2.98  
 291.73  
 11.35  
 280.38  
 1.28  
 281.66

Brooks

272.0

75.  
 ↓ N. End Curb  
 74.36 74.15 74.00 74.02

6

55.01

IVY Lane.

50'

86.45 86.51 86.50 87.30 0.93 G  
 86.82 86.79 86.79 87.66 287.5  
 86.93 86.93 86.93 87.73

15.11-4

0.86 G

289.5

88.67

.73

88.83

Upas St

286.86 B.M. N.W. Penn & 6<sup>th</sup>

3.06  
 289.92

286.86  
 5.62  
 292.48

285.51 B.M. 6<sup>th</sup> & Robinson

3.22  
 288.73

78.54	5.84	Gutter	75.90	75.06
4.07			6.76	7.55
82.61			7.35	7.35
			-0.64	40.20

Anderson

85.31 85.31 86.27  
 85.23 85.30 86.15 86.0  
 85.82 85.72

77.81 77.75 78.54 S. End curb  
 gutter 75.06 75.90

Robinson

83.86 83.72  
 84.04 83.72 84.64

50

87.00 87.00 87.67 82.5  
 0.5  
 87.08 87.10 87.00 86.90  
 Penn  
 87.00 87.00 86.95 87.42  
 87.00 87.00 87.00 87.42  
 46.89 46.90 87.62 87.5



3-3-33  
Miller  
Walker  
Blair

Grades.  
Alley BIK 96. City Hts.  
Myrtle to Dwight bet. Central + 41st

Indexed  
C.S.K.

	W. line	±	E. line
0+00 S. Line Dwight.	330.00		329.90
0+20 Brk	330.30		330.10
0+40 "	330.20		330.00

AM. BT. N.W. Myrtle + 41st 321.52  
6.03  
327.55  
1.97

3+50	326.60 4.95 4.70 +0.25	326.65 4.90 4.65 +0.25	325.68 5.87 331.55 10.15 321.40
------	---------------------------------	---------------------------------	---

4+00	326.01 5.54 4.89 +0.65	326.10 5.45 5.56 -0.11	
------	---------------------------------	---------------------------------	--

4+50	325.43 6.12 5.73 +0.39	325.56 1.99 1.91 +0.08	1.082%
------	---------------------------------	---------------------------------	--------

5+00	324.85 2.70 2.51 +0.19	325.02 2.53 2.58 -0.05	1.161%
------	---------------------------------	---------------------------------	--------

5+30 Brk	324.50 3.08 2.99 +0.06	324.70 2.85 2.89 +0.46	
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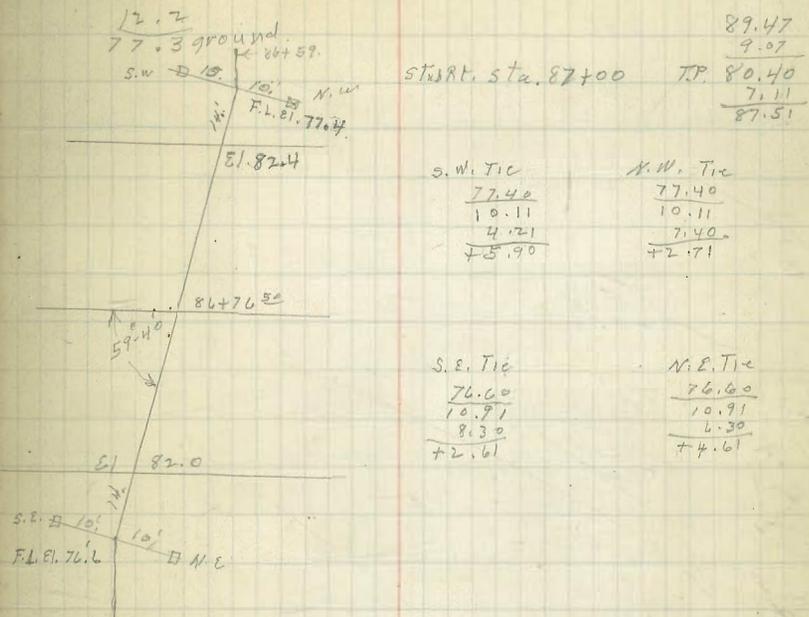
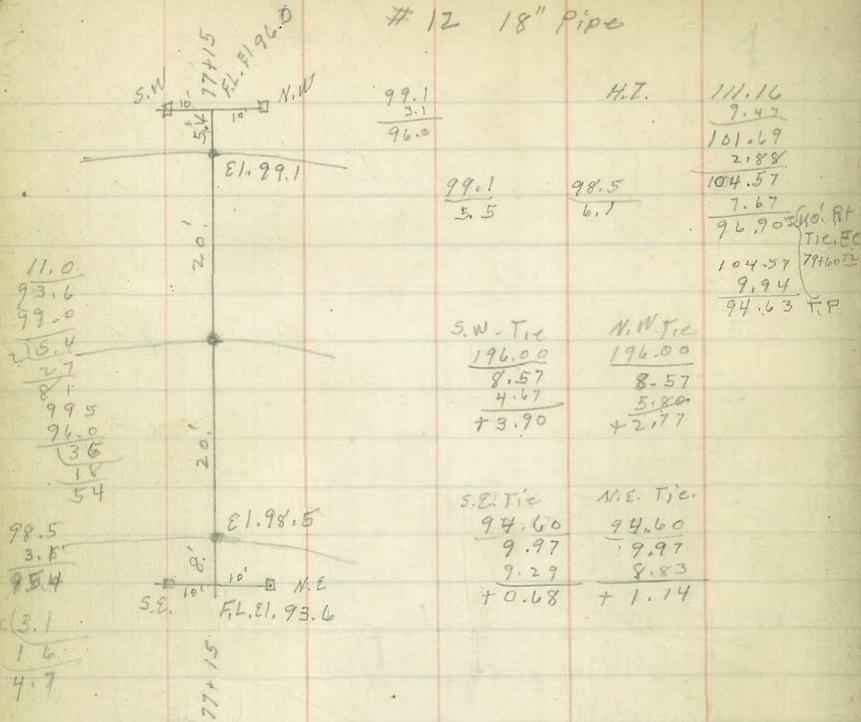
5+50 Brk	323.90 3.65 3.38 +0.27	324.20 3.35 2.95 +0.40	
----------	---------------------------------	---------------------------------	--

5+70 Brk.	323.00 4.55 3.70 +0.85	323.20 4.35 3.65 +0.70	
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6+00 = N. Line Myrtle.	321.40 6.15	321.30 6.25	
------------------------	----------------	----------------	--

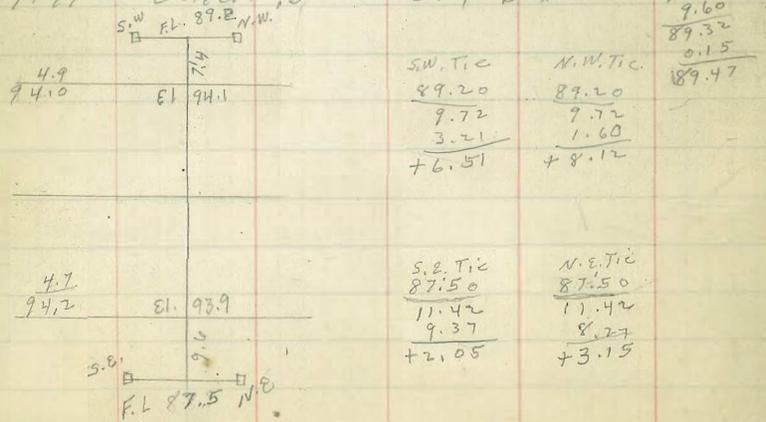
#12 18" Pipe

#14 18" PIPE



79+77 Culvert #13

3x4 Box



Indexed Alley BK 6. Blairs Highlands. 5-29-33  
c.s.K. bet. Granada + R 9<sup>th</sup>. S. of Palm.

54

BM. B.P. 6.96 317.87 310.91 N.E. Palm  
+ Granada.

W  
0 to 100 S. of Palm 312.86 312.74 312.47  
5.51 5.53 5.40  
5.51 5.40  
0.0 Paymt. 0.0 Paymt.

6 + 10 312.61 312.41 312.76  
5.26 5.11  
4.51 4.04  
+ 0.75 + 1.07

0 + 30 313.00 312.80 313.17  
4.87 4.70  
4.66 4.11  
+ 0.21 + 0.59

0 + 50 313.17 312.97 313.44  
4.70 4.43  
4.82 4.22  
- 0.12 + 0.21

0 + 70 313.13 312.93 313.43  
4.74 4.44  
4.92 4.65  
- 0.18 - 0.21

0 + 75 313.07 312.87 313.37  
4.80 4.50  
5.29 4.73  
- 0.49 - 0.23

5-31-34 Fire Hydt. S. E. Cor.  
 Miller  
 Walker  
 Bliss.

Indexed  
 C.S.K.

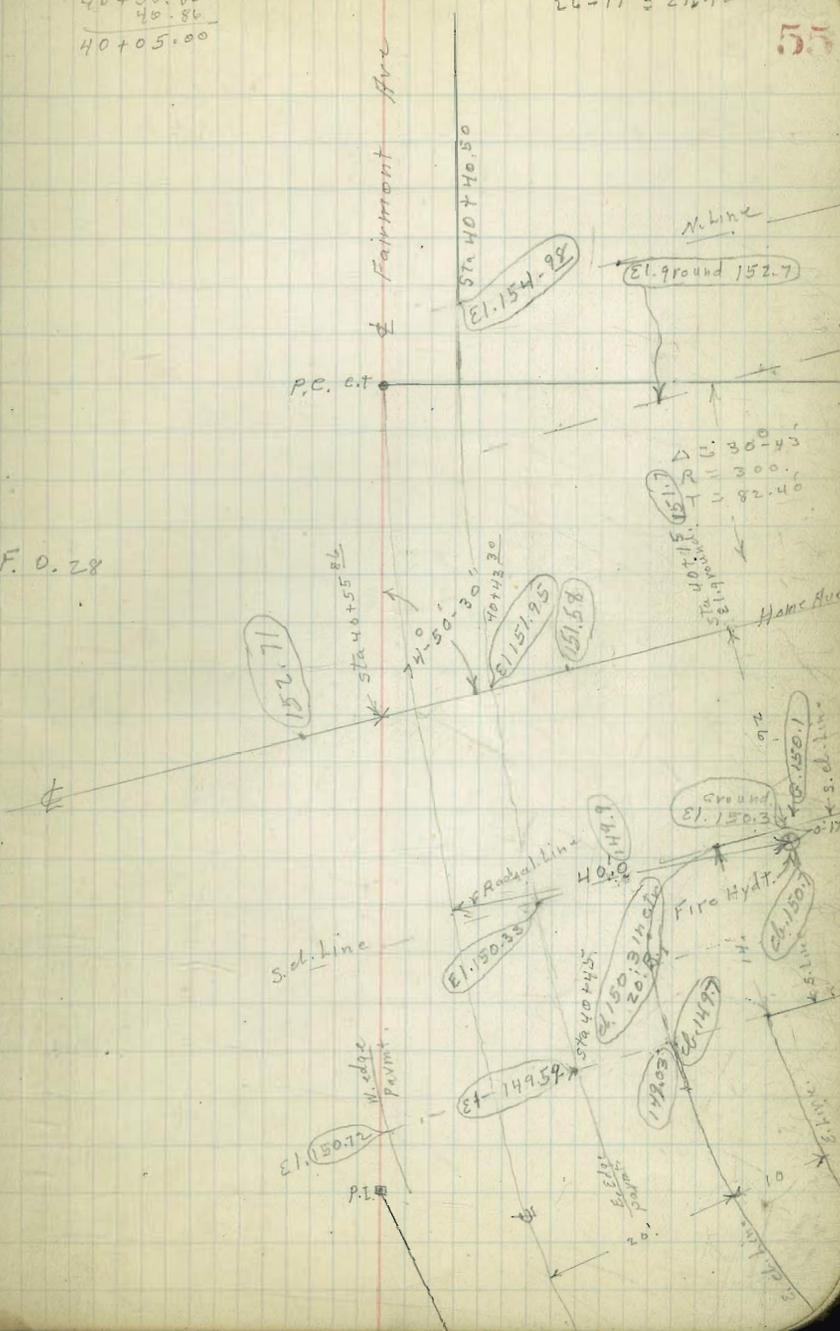
Fairmont. + Home Aves.

Sta Cor.				S. of Home
R.M. B.P. Box Culvert	8.00	156.22	14.8.22	+ Fairmont Ave
4. Home E. Edge Fairmont Pavmt	4.27	151.95		
S. d. line Ex ground	5.9	150.3	151.0	
4 " "	4.5	151.7	150.9	
N. d. Line " "	3.5	152.7	152.0	
S. d. Home E. Edge Pav.	5.89	150.33		
S. line " " " "	6.63	149.59		
S " " W " "	5.50	150.72		
5' Tie out. stub Fire Hydt.	5.80	150.42	150.7	F. O. 28

40+55.86  
 40.86  
 40+05.00

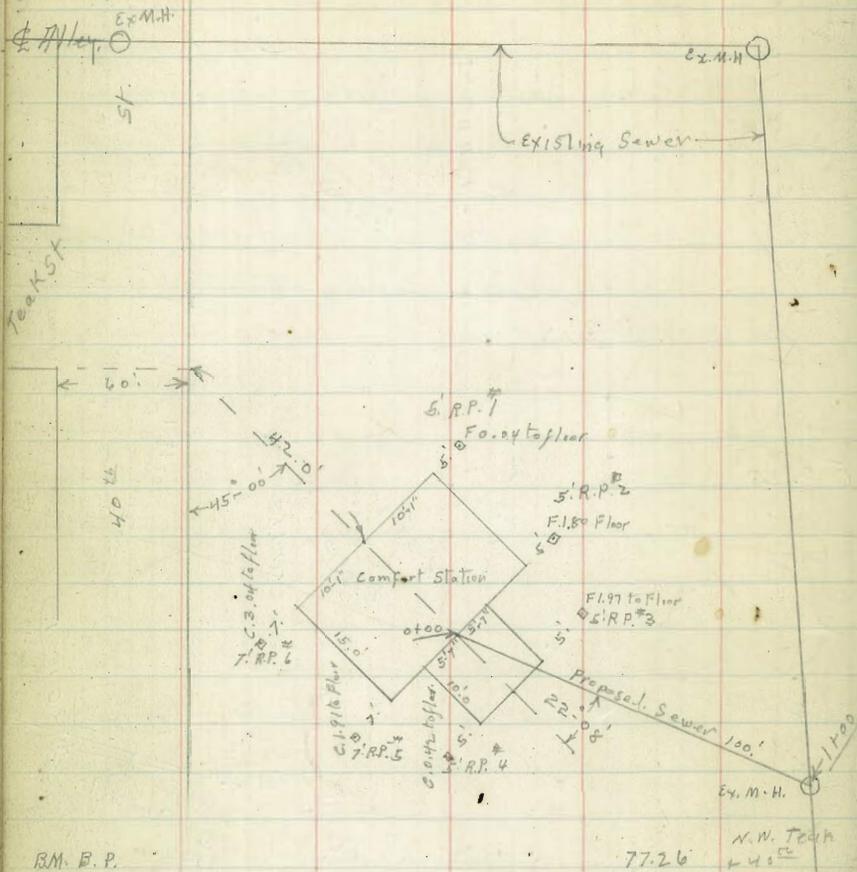
26'-17" = 27.42

55



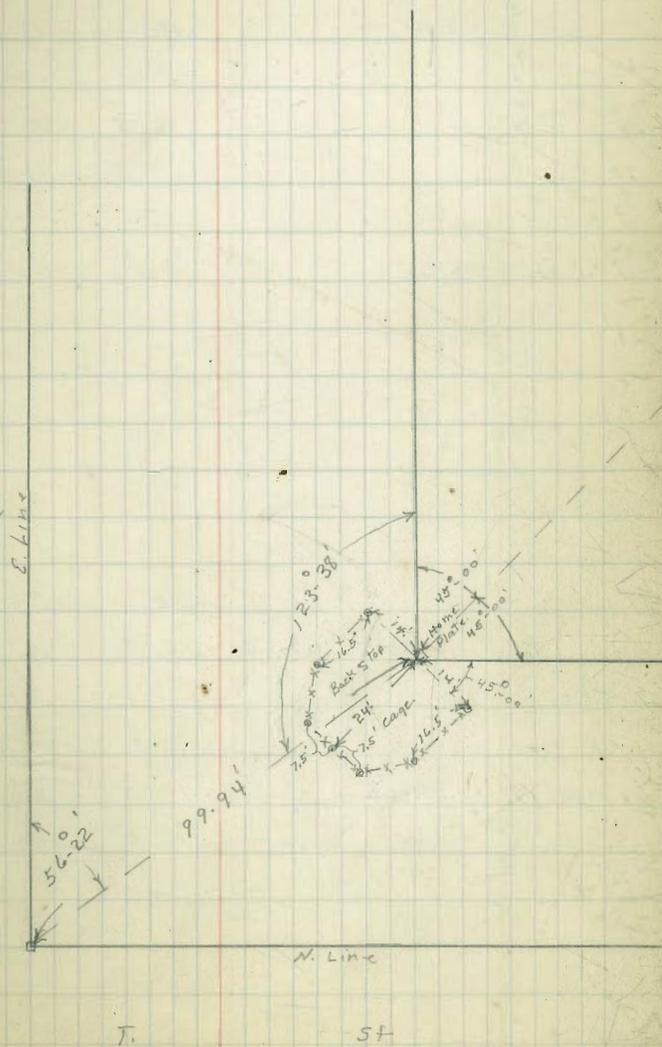
1-21-37  
Miller  
Walker  
Bliss

# Mt. View Park Comfort Station



# Ball Diamond Mt. View Park

56



Floor Grades. Comfort Station

BM. B.P. 1.52 78.78 77.26 N.W. Cor. 40' + Teak St.

Finish Floor Grade

5' R.P. #1	N.E. Cor	10.12	68.66	68.70	F. 0.04
5' R.P. #2		11.88	66.90	68.70	F. 1.80
5' R.P. #3		12.05	66.73	68.70	F. 1.97
5' R.P. #4		9.66	69.12	68.70	C. 0.42
7' R.P. #5		8.17	70.61	68.70	C. 1.91
7' R.P. #6	N.W. Cor.	7.04	71.74	68.70	C. 3.04

78.78

Sewer Connection Grades.

T.P.	2.86	69.59	12.05	66.73	
0+00			1.19	68.40	66.59 C. 1.81
0+50			7.24	62.35	59.99 C. 2.36
1+00. Ex. M.H. Rim.			11.93	57.66	53.39 C. 4.27 Rim To F.L.
1+00.7 F.L. Main.			16.71	52.88	= 52.88 Profile

## T. St. Grades

58

B.M. B.P.	8.27	58.89	50.62	N.W. 40 <sup>th</sup> + T. Sts. N. Line Grade		
0+00 = E. Line 40 <sup>th</sup> St			6.0	52.9	50.5	+ 2.4
0+50			6.4	52.5	49.8	+ 2.7
1+00			7.8	51.1	49.4	+ 1.7
1+35			9.6	49.3	49.1	+ 0.2
1+70 B.			9.9	49.0	48.8	+ 0.2
2+00 B.			10.4	48.5	48.9	- 0.4
2+30 B.			10.0	48.9	49.5	- 0.6
2+60 B.			9.5	49.4	50.7	- 1.3
2+90 B.			8.3	50.6	52.5	- 1.9
3+35			5.0	53.9	55.7	- 1.8
3+80			1.9	57.0	58.9	- 1.9
T.P. 14.71	71.76		1.84	57.05		
4+25			11.2	60.6	62.0	- 1.4
4+70 B.			7.4	64.4	65.2	- 0.8
4+90 B.			5.7	66.1	66.4	- 0.3
5+10 B.			4.6	67.2	67.3	- 0.1
5+22 = W. Line Boundary			3.8	68.0	68.0	00

40<sup>th</sup> St. Grades

59

BM. B.P.	8.27	58.89	50.62	N.W. 40 <sup>th</sup> + T. 5/6	E. Line Grades	
0+00 = N. Line T. St			6.0	52.9	50.5	+2.4
0+50			4.2	54.7	53.7	+1.0
1+00			1.3	57.6	56.8	+0.8
T.P. 12.79	70.42		1.26	57.63		
1+50			10.2	60.2	59.8	+0.4
2+13 S. Line S. St.			4.9	63.5	63.7	-0.2
2+63 N " " "			4.7	65.7	65.7	0.0
3+13			2.9	67.5	67.7	-0.2
3+63 T.P. 8.75	78.78		0.39	70.03	69.8	+0.2
4+13			5.9	72.9	71.8	+1.1
4+76 S. Line Teak. St			4.0	74.8	74.4	+0.4
5+39 N " " "	" "		3.4	75.4	75.7	-0.3
T.P.M. 3.26	80.52		1.52	77.26	N. Line Teak + 40 <sup>th</sup>	
5+89			5.0	75.5	76.2	-0.7
6+39			5.8	74.7	76.7	-2.0
6+89			6.1	74.4	77.2	-2.8
7+39			3.6	76.9	77.7	-0.8
7+89			2.9	77.6	78.3	-0.7
8+24 S. End. Ex. ent. cl. Return.			2.5	78.0	78.6	-0.6
T.P.			8.74	71.78		

π 80.52

S. End. Ex. cl. S. E. Cor. Ocean View + 40<sup>th</sup>  
2.10 78.42 = 78.42 ✓

## Boundary St. Grades.

71.76 Page 58

60

0+00 = K Line T. St.	3.8	68.0	68.0	0.0
0+34 KB	3.4	68.4	68.9	-0.5
+74 B	3.0	68.8	69.7	-0.9
1+14 B	3.5	68.3	70.0	-1.7
+54 B	2.2	69.6	70.0	-0.4
+9.4 B	2.2	69.6	69.6	0.0
2+34 B Exe.	2.0	69.8	69.0	+0.8
2+94 B B.V.e.	2.6	69.2	67.7	+1.5
3+34	4.6	67.2	66.9	+0.3
3+74	5.2	66.6	66.5	+0.1
4+14	5.1	66.7	66.3	+0.4
4+54	5.2	66.6	66.5	+0.1
4+94	4.9	66.9	66.9	0.0
5+34	4.8	67.0	67.6	-0.6
5+74			68.6	
5+85	3.3	68.5	68.9	-0.4
T.P.	+0.02	71.78	=71.78 T.P. Page	59

INDEXED

WK  
DEC 27 1948

2-4-37

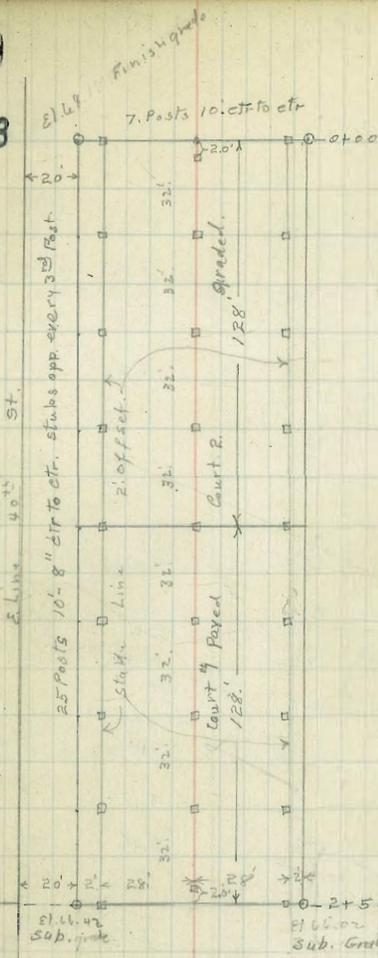
Tennis Courts Mt. View Park.

INDEXED  
WK  
DEC 27 1948

61

BM. B.P.	0.51	77.77	77.26	N.W. Cor. 40' x Tenk.
Stab W. Line		Stab 4	E. Ground	E. Gr.
0+00 = N. End	8.22	8.61	9.15	
N. End Grad. in 7	68.58	69.16	69.62	
+11 N. End 5	68.51 Finish G	69.31 Finish G	69.71	
	+1.04	+0.85	+0.51 Finish	
0+32	9.73	9.72	9.64	
	68.04	68.05	68.13	
	68.29 Finish G	68.09	68.89	
	-0.25	-0.04	+0.24 Finish	
0+64	9.83	10.20	10.20	
	67.74	67.57	67.57	
	68.07 Finish G	67.87	67.67	
	-0.13	+0.39	-0.10 Finish	
0+96	10.45	10.42	12.28	
	67.32	67.35	65.49	
	67.85	67.65 Finish G	67.45	
	-0.53 Finish G	-0.35	1.96 Finish	
1+28 X	0.42 10' N Finish G	0.33 Finish G to N	0.20 Finish	
	10.56	10.67	10.74	
	67.21	67.10	67.03	
	67.30	67.10 Sub. G	66.90 Sub. G	
	-0.09 10' S Sub. grade	0.00	+0.13	
1+60	10.69	10.54	10.70	
	67.08	67.23	67.07	
	67.08 Sub. grade	66.88 Sub. G	66.68 Sub. G	
	0.00	+0.35	+0.39	
1+92	10.61	10.96	10.92	
	67.16	66.81	66.85	
	66.86 Sub. grade	66.66 Sub. G	66.46 Sub. G	
	+0.30	+0.15	+0.39	
2+24	10.56	11.21	11.29	
	67.27	66.56	66.48	
	66.64 Sub. G	66.44	66.24 Sub. G	
	+0.57	+0.12 Sub. G	+0.24	
2+56 S. 2nd	10.11	11.43	11.79	
	67.66	66.34	65.98	
	66.42 Sub. G	66.22 Sub. G	66.02 Sub. G	
	+1.24	+0.12	-0.04	

6. Line Tenk. 5'



66.64 68.58  
 0.57 0.12  
 3.98 4.85  
 71.19 = 71.19

4.03  
 67.16  
 66.42 sub. G  
 +0.74 Rest.

3-1-37

University Hts. Storm Drain  
 Alley BIK 147 U.H.  
 stubs 14. offset RT  
 Restake See Page 64

315.58

5239 L.

63

INDEXED

WK

DEC 27 1948

8+03 <sup>45</sup> End. Ex 30" Culvert	FL	7.25	308.33 =	308.33			
+50		4.76	310.82	307.90	+2.92 ✓		
9		5.82	309.76	307.47	+2.29 ✓		
+50		5.28	310.30	307.04	+3.26 ✓		
10		5.40	310.18	306.60	+3.58 ✓		
+50		5.41	310.17	306.17	+4.00 ✓		
11		4.75	310.83	305.73	+5.10 ✓		
+50		4.90	310.68	305.30	+5.38 ✓		
+88 = N. Line Polk Ave	No grade pt.						
T.P. 0.95	311.81	4.72	310.86	T.P.			
+99 = 14" N. of Polk St. Culvert	Polk St.	0.95	310.86	304.86	+6.00 ✓		
12 +13. Cleanout. Δ 90° RT							
25 S. of N. Line Polk.		0.95	310.86	304.75	+6.11 ✓	Ex. M.H. & Alley	
+27.		0.95	310.86	304.05	+6.81 ✓	+ & Polk Ave	8.71 = 303.10 F.L.
+67.25		3.46	308.35	302.03	+6.32 ✓		
13 + 07.50		6.55	305.26	300.01	+5.25 ✓		
+47.75		8.63	303.18	298.00	+5.18 ✓		
+68 E. Line Louisiana St		9.41	302.40	297.00	+5.40 ✓	Pay & 10.15	301.66 +4.66
+88 Cleanout		10.08	301.73	296.00	+5.73 ✓	" " 10.08	301.73 +5.73
14 + 42 Cleanout		9.72	302.09	295.06	+7.03 ✓	" " 10.41	301.40 +6.34
+97.5		7.26	304.55	294.12	+10.43 ✓		
15 + 53		4.44	307.37	293.18	+14.19 ✓		
T.P. stub 4.46	311.83	4.44	307.37	292.50	+16.02 ✓		
14" N. of Cleanout		3.26	308.57	292.50	+16.02 ✓		
Cleanout - bet Louisiana & Miss.							
15 + 93 Δ 90° Lt. 5" E & Alley 14" N.		3.09	308.74	292.50	+16.24 ✓		
16 + 48 = S. Line Polk		4.32	307.51	291.57	+15.94 ✓		

8+88.5 E. Alley - MH 10.98 304.60 F.L.

Nail in garage 14.9 offset RT

Ex. M.H. & Alley  
+ & Polk Ave 8.71 = 303.10 F.L.

Pay &amp; 10.15 301.66 +4.66

" " 10.08 301.73 +5.73

" " 10.41 301.40 +6.34

New Location Cleanouts Louisiana + Polk

13 + 93.5 Cleanout. 4.37 301.84 295.90 + 5.94

14 + 45.5 Cleanout. 4.65 301.56 295.00 + 6.56

17+0.0		4.38	307.45	290.70	+16.75 ✓	
+50		6.47	305.36	289.85	+15.51 ✓	
18		7.32	304.51	289.00	+15.51 ✓	
+50		8.22	303.61	288.15	+15.46 ✓	
19		10.02	301.81	287.30	+14.51 ✓	
+58		11.47	300.36	286.32	+14.04 ✓	
20		13.17	298.66	285.60	+13.06 ✓	
T.P.	1.51	300.31	13.03	298.80		
+50		2.84	297.47	284.75	+12.72 ✓	
21		5.31	295.00	283.90	+11.10 ✓	
+50		8.31	292.00	283.05	+8.95 ✓	
22		9.46	290.85	282.20	+8.65 ✓	
+48 = N Line Lincoln		9.58	290.73	281.40	+9.33 ✓	
T.P.	2.63	293.36	9.58	290.73		
T.P. B.M.	8.94	294.82	7.48	285.88	= 285.88	
chk. New stub 22+48			2.75	292.07	281.40	+10.67
B.M.	7.58	293.46		285.88		
22+88 = $\phi$ Lincoln		1.76	291.70	280.70	+11.00	
22+98 = $\phi$ Cleanout $\Delta$ 90°-00' RT		2.46	291.00	280.55	+10.45	
23+48		4.84	288.62	279.70	+8.92 ✓	
24+0.0		6.95	286.51	279.21	+7.30 ✓	
24+50		7.49	285.97	278.80	+7.17 ✓	
24+58 E. Line Mississippi						
24+84		7.83	285.63	278.50	+7.13 ✓	
25+18 = Cleanout		9.30	284.16	278.20	+5.96	

2.70 coverage

Restake Univ Hts Storm Drain

See Page 62

B.M. Stub	4.48	311.85	307.37	Sta 15+53 Fin. Grade	
14+97 <sup>50</sup> <sub>7</sub>	chk. stub	7.30	307.55	294.12	+10.43 chk
15+04.5		7.50	304.35	294.00	+10.35 ✓
15+53	chk. stub	4.48	307.37	293.18	+14.19 chk
15+93	chk x 14' N. of cleanout	3.28	308.57	292.50	+16.07 chk.
15+93	grade ctr cleanout	3.63	308.22	292.50	+15.72
16+48	N. End shaft				
16+59	S. End shaft				
17+41 <sup>20</sup>	(# spk. sta 17+39 <sup>20</sup> )	6.82	305.03	290.00	+15.03
17+40	N. End. shaft				
17+51	S " "				
18+11	N " "				
18+11.2	(# spk. at sta 18+09 <sup>2</sup> )	8.33	303.52	288.88	+14.64
18+21	S End. shaft				
18+90	N " "				
18+91	(# spk. at sta 18+89)	10.34	301.51	287.46	+14.05
19+00	T.P. stub	2.05	303.86	287.30	+14.51 chk
19+10				14' W. of 19+00	
19+26					
19+48					
19+58					
19+75					
19+90					
20+10					
20+28					
20+35					

303.86

65

<sup>20</sup> 20+55	7.24	296.62	84.67	+111.95 ✓
<sup>21</sup> 20+76	8.22	295.64	84.31	+111.33 ✓
<sup>11</sup> 20+87	7.93	295.93	84.12	+111.81 ✓
<sup>13</sup> 21+00	8.90	294.96	283.90	+111.06 ✓
<sup>20</sup> 21+20	9.67	294.19	283.56	+110.63 ✓

X See at 10<sup>th</sup> + Univ. <sup>Indexed</sup>  
Continued from F.B. 1520 - Page 80  
E.S.K.

- T 287.35  
287.40

~~287.35~~  
287.40

66

1+81 = E. Line 10 <sup>th</sup> St.			
N. Line from W. - 18.5 - N. d. Cleveland.	4.07	283.33	cl + paving Flush on Return
" " " "	4.14	283.26	
" " " " + 12 = N. d. from W	4.22	283.18	
14.5 S. of N. d. = Rail.	4.25	283.15	
0+00 = P.C. S. Rad. Return N.E. 10 <sup>th</sup> + Cleveland.			
at 90 <sup>o</sup> from N. d. See FB 1520 - P. 77.			
N. d. of Cleveland N.W. Cor. E.B.	4.07	283.33	
" " + 2.5 = S.W. " " "	4.09	283.31	
" " + 10	4.13	283.27	
" " + 20	4.13	283.27	
" " + 20	4.15	283.25	
0+4.5 = E. End. Catch Basin			
N. d.	4.03	283.37	
Gutter = N.E. Cor. E.B.	5.24	282.16	
+ 2.5 = S.E. " " "	5.25	282.15	
+ 7	4.53	282.87	
+ 10	4.40	283.0	
+ 20	4.19	283.21	
+ 30	4.09	283.31	
0+20			
N. d.	4.84	282.56	283.56
Gutter	4.69	282.71	
+ 10 S.	4.33	283.07	
+ 20 S.	4.12	283.28	
+ 30	3.89	283.51	

0+40

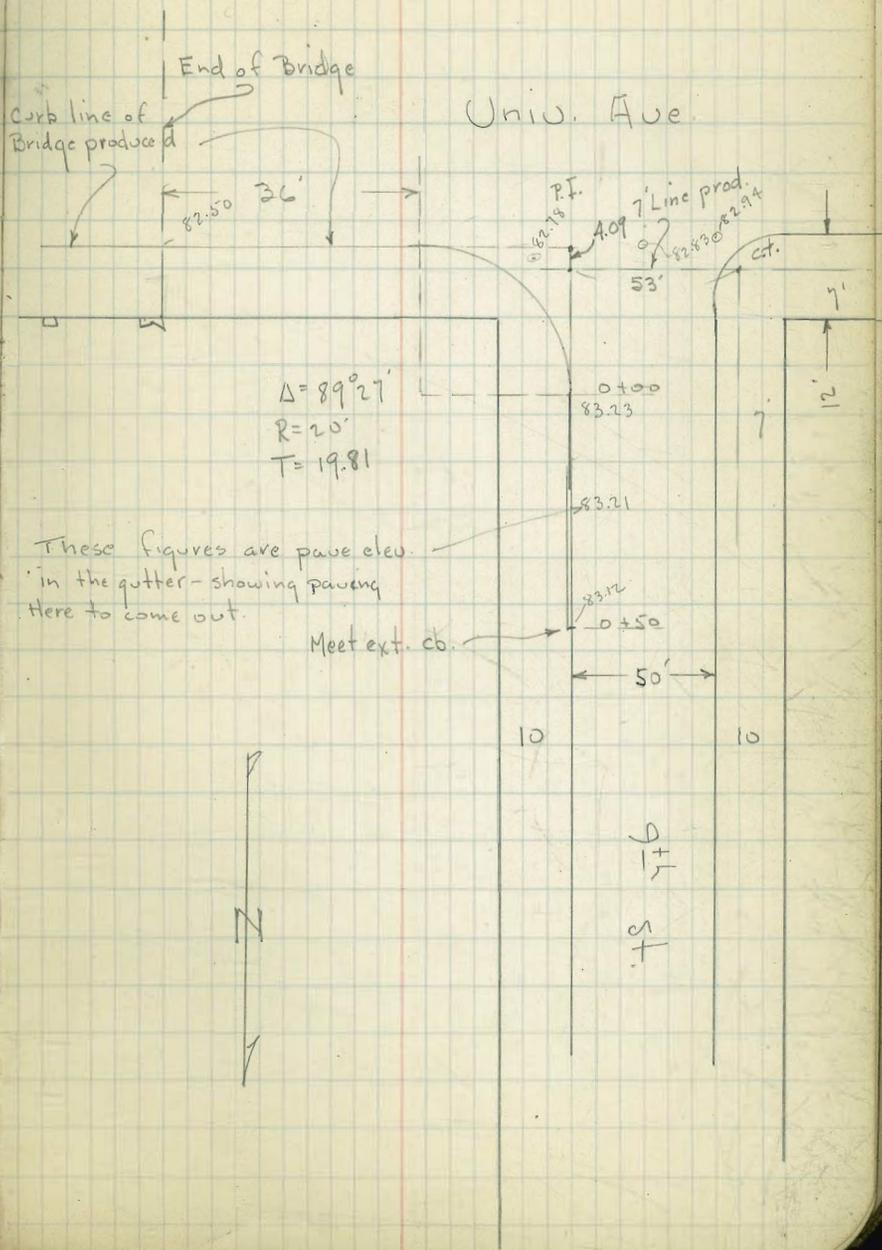
N. d.			3.64	283.76
Gutter			4.49	282.91
+ 10			4.11	283.29
+ 20			3.87	283.53
+ 30			3.61	283.79
T.P.	5.53	292.09	0.84	286.56
		292.04		286.51
BM B.P. S.W. Vermont + Univ	2.36			289.68 = 289.73
" " " " " "	2.36			289.73 OK BM Book
chk. Levels				
BM B.P.	2.36	292.09		289.73 S.W. Univ + Vermont.
T.P.	0.84	287.40	5.53	286.56
New BM. Old. Location			5.39	282.01 = 282.02 BM
				282.01
				282.01

↑ This H.I. should be used FB. 1520 - P. 77



4-30-47  
7.0.

B.M.	4.42	288.18	283.76	NE. 9 <sup>th</sup> Univ.
				Est. grade
End. cb. on Bridge	4.68	83.50	283.36	stakes 3' out
36' W. = P.C. on Univ.	6.39	81.79	83.47	F 1.68
± Ref.	5.40	82.78	83.50	F 0.72
0+00 = P.C. on 9 <sup>th</sup>	4.95	83.23	83.53	F 0.30
0+25 = U.	4.97	83.21	83.60	F 0.39
0+50 = Ext. cb.	4.52	83.66	83.66	













indexed  
C.S.K.

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Sewer Grades  
Alley BIK 28'9". S. D. L+T.

SpK B.M.  
0+00=W  
Line Rigel

S.W. Rigel  
↓ Birch  
Flow Line  
Grade

1+10  
1+10=End  
Existing Sewer

6.61

1+60 T.P. 3.61 17.28 12.20 13.67 6.86 + 6.81

2x F.L.

1+95 end diagonal to N. E. Cor Lot. 90' to Main 7.50 7.03

2+10 5.92 11.36 7.11 + 4.25

Ex. F.L.

2+38 square out. to Main 70' 7.50 7.25

2+60 7.12 10.16 7.36 + 2.80

2+80 opp. Plumbing House on S. 7.46

3+10 8.17 9.17 7.61 + 1.56

T.P. 4.78 14.57 7.49 9.79

2+38 100' S. of Alley 6.72 7.85 Top Pipe at House  
35  
7.50

2+38 104' S. of Alley Floor House 4.41 10.16

B.M. 5.17 14.34 9.17

2+80 Ex plumbing 16'S 7.07  
6.07

2+80 F.L. 6.44 7.90 7.46

40<sup>th</sup> St. Grades  
Ocean View Blvd to T. sls

Indexed  
C.S.K.

E. Curb Grades

75

W. d. 18 1/2 ft. of 40<sup>th</sup>  
S. Side Ocean View  
E. Side Curb

E. Curb Grades.

8+24	5.49 El. 78.42 3.87	Excl. S. End Return 78.42 5.70 ✓	82.18 1.94 84.12
35	82.18 0.13		
7+89	82.31 7.05 75.26 1.47 76.73	78.12 4.2 5.0 -0.8	78.12 6.00 6.7 F 0.7 F 0-4 78.06 6.00 6.7 F 0.7
7+39	77.69 4.6 7.7 -3.1	77.7 6.4 8.8 F 2.4 F 2-5	77.54 ✓ 6.4 8.8 F 2.2 F 2.3
6+89	77.27 5.0 9.6 -4.6	77.3 6.8 9.5 F 2.7 F 2-8	77.83 ✓ 7.1 9.5 -2.4 F 2.5
6+39	76.85 5.5 8.6 -3.1	76.8 7.3 8.9 F 2.6 F 2-7	76.52 ✓ 7.6 8.9 -2.3 F 2.4
5+89	76.42 5.9 7.6 -1.7	76.4 7.7 9.3 F 1.6 F 1-7	76.01 ✓ 8.1 9.3 F 1.2 1.1
N. Line Teak 5+39	76.5	76.0	75.5 ✓
63	77.16 76.15	6.3 7.0 0.7	8.6 8.1 C. 0.5 Cal
S. Line Teak 4+76	75.2	74.2	
63	2.5 1.5 +1.0	9.9 8.9 C. 1.0	
4+13	71.62 5.1 3.2 +1.9	71.6 ✓ 12.5 10.7 C. 1.8 C. 1-10"	
3+63	69.58 7.1 6.2 +0.9	69.6 ✓ 1.2 +0.05 C. 1.25 C. 1-3"	
3+13	67.54 9.2 9.2 0.0	67.5 ✓ 3.3 2.6 C. 0.7 C. 0-8"	

Changed

changed

N. Line S.

2+63	66.50	76.73 12.62	65.50	65.5 ✓	70.77 X
50	66.54	64.11	11.2	5.3 5.3	12.75
	Hemlock	1.65	11.2	0.0	58.02
S. Line S	65.60	65.16	0.0		1.55
2+13	64.50	11.85	63.50	63.5 ✓	59.57
		53.31	13.2	7.3 6.8	9.95
63			12.6	0.5	50.62 BM
			+0.6		C. 0-6" 40-27"
1+50			59.65	59.6 ✓	
			5.5	11.2	
			4.4	7.9	
			+1.1		C. 1-4"
1+00	M		56.60	56.60 ✓	
	0		8.6	8.10	
	0		7.5	2.1	
	0		+1.1		C. 0-9" C. 0-11"
0+50			53.55	53.5 ✓	
			11.6	6.3	
			10.1	6.3	
			+1.5		C. 0-8" C. 0-10"
N. Line T.			50.50	50.5	N. End Ret.
0+00	51.10		15.2	9.1	
			14.7	9.9	
			11.8		
			+2.9		C. 1-2" C. 1-3"
					50.0 E. End. Ret.
					7.6

T. St Grades		Indexed c.s. etc.	
N. Line	N. d	Boundary	S. Line
4+25	62.0 ✓ 6.2 10.2 -4.0	68.17	61.7 6.5 3.6 +2.9
3+80	58.9 ✓ +2.9 2.4 -5.3	H.I. 55.97	58.4 9.8 9.8 0.0
3+35	55.7 ✓ 0.3 6.1 -5.4		55.1 0.9 5.0 -4.1
2+90B	52.5 ✓ 3.5 9.3 -5.4	52.30	51.60 51.8 4.2 8.7 -4.5
2+60B	50.7 ✓ 5.3 7.9 -3.6	50.50	49.65 49.8 6.2 11.6 -5.4
2+30B	49.5 ✓ 6.5 10.2 -3.7	49.35	48.40 48.6 4.9 8.6 3.7 5.5 out
2+00B	48.9 ✓ 7.1 10.4 -3.3	48.75	47.75 47.9 8.1 12.1 -4.0
1+70 Brk	48.8 ✓ 7.2 7.8 -0.6	48.65	47.65 47.8 5.7 7.3 -1.6 2.4 out
1+35	49.1 ✓ 6.9 4.7 +2.0		48.1 48.1 5.4 7.9 6.9 +1.1
1+00	49.4 ✓ 6.6 5.3 +1.3		48.4 48.4 7.6 7.6 0.0
0+50	49.4 ✓ 6.2 3.5 +2.7		48.8 48.8 7.2 7.2 0.0
S. Line 40 <sup>th</sup> 0+00	50.2 5.8 2.8 +3.0	50.00	49.00 49.2 6.8 5.5 +1.3
W. Line 40 <sup>th</sup>		50.60	49.60

50.62 AM. B.P. NW. 40 <sup>th</sup> St.		53.31	
N. Line	N. d	S. d.	S. Line
		2.66	
55.97 0.26 55.71 12.46 68.17 0.91 67.36 7.53 74.89 7.1 67.8			
Curb Inlet T. St. E. of 40 <sup>th</sup> Stakes 3' from Face Curb			
N. d.		2+06	S. d.
			47.87 5.63 6.63 -1.00
2+03	48.80 4.70 5.70 -1.00		
		1+96	47.74 5.76 6.76 -1.00
1+93	48.73 4.77 5.77 -1.00		
E. Line 40 <sup>th</sup> = 0+00			
BM 50.62			
2.88			
53.50			
	11.3 4.5 6.8 3.4 10.2		
W. Line Book			
	67.7 7.2 7.1 +0.1	67.50	68.00 68.2 6.7 6.6 +0.1
5+10B	67.2 7.7 7.6 +0.1	67.05	67.05 67.2 7.7 5.6 +2.1
4+90B	66.4 8.8 8.8 -0.3	66.20	66.20 66.4 8.5 6.1 +2.4
4+70B	65.2 3.0 4.0 +1.0	65.00	64.85 65.0 9.9 7.9 +2.9

Culvert Mt. View Park.

index  
c/sk

12.85  
3.55  
15.40

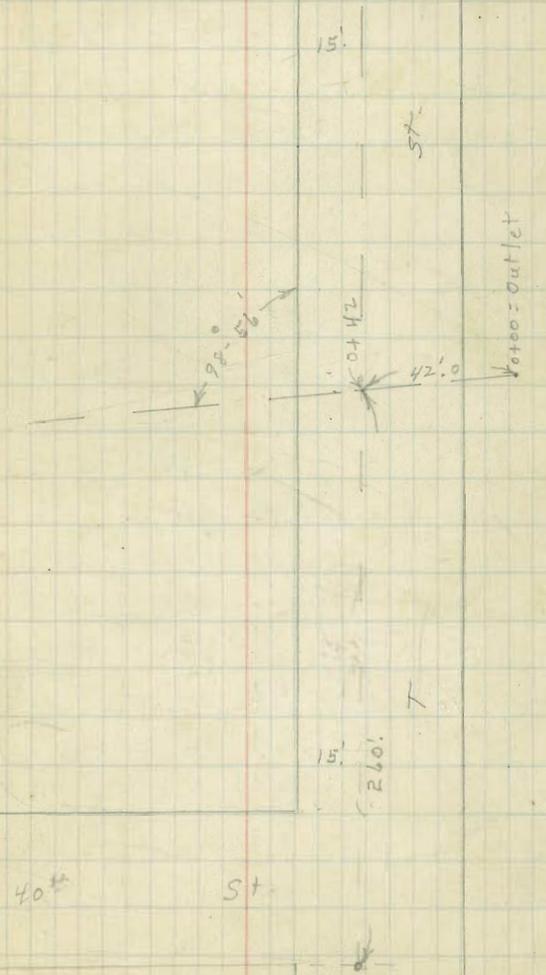
15.1  
44.3

11.6  
3.5  
15.1

77

BM	883	59.45 Restake	50.62	BM.N.W. 40 <sup>th</sup> + T.	
BM	879	58.81	50.62		
				Grade	
5+00			0.6	52.8	56.90 C 1.7
4+50			1.5 0.9	57.9 57.9	55.65 C 2.25
4+00			2.5 1.8	57.0 57.0	54.4 C 2.6
3+50		Restake	4.5 3.0	55.0 55.8	53.15 C 1.85 + 2.7
3+00		Restake	5.0 3.5	54.4 55.3	51.90 C - 2.5 + 3.4
2+50		Restake	4.9 4.1	54.5 54.7	50.65 C 3.85 + 4.0
2+00		Restake	4.8 4.6	54.6 54.2	49.40 C 5.2 + 4.8
1+50			5.7	53.7	48.15 C 5.55
1+00			7.3	52.1	46.90 C 5.20
0+70			7.5	52.0	46.15 C 5.85
0+42			12.0	47.4	45.45 C 7.95
0+00 outlet			15.4	44.0	44.3 44.9 ground outlet F.0.4

57.8 5+00  
ground  
in ditch



Grades Ball field  
Mt. View Park

Indexed  
c.s.K.

BM/BP	8.11	58.73	50.62	N.W. 40 <sup>th</sup> 4 <sup>th</sup> St. Grades Book 1398	54.0	
Home Plate		5.55	53.18	54.0	-0.8	✓
3 <sup>rd</sup> Base line						
100'		3.98	54.75	55.00	-0.2	✓
200'		3.84	54.89	56.0	-1.1	✓
300'		1.64	57.09	57.5	-0.4	✓
22°-30' Rt						
100'		4.41	54.32	54.5	-0.2	✓
200'		4.26	54.47	55.25	-0.8	✓
250'		2.10	56.63	56.0	+0.6	✓
45°-00' Rt						
100'		4.15	54.58	54.0	+0.6	✓
195'		4.32	54.41	54.5	-0.1	✓
230'		2.88	55.85	55.0	+0.8	✓
67°-30' Rt						
100'		5.07	53.66	53.75	-0.1	✓
200'		4.66	54.05	54.5	-0.5	✓
240'		2.83	55.90	55.1	+0.8	✓
90°-00' Rt = 1 <sup>st</sup> Base Line						
100'		6.01	52.72	53.5	-0.8	✓
200'		6.29	52.44	54.5	-2.1	✓
290'		4.22	54.51	55.8	-1.3	✓

Restake

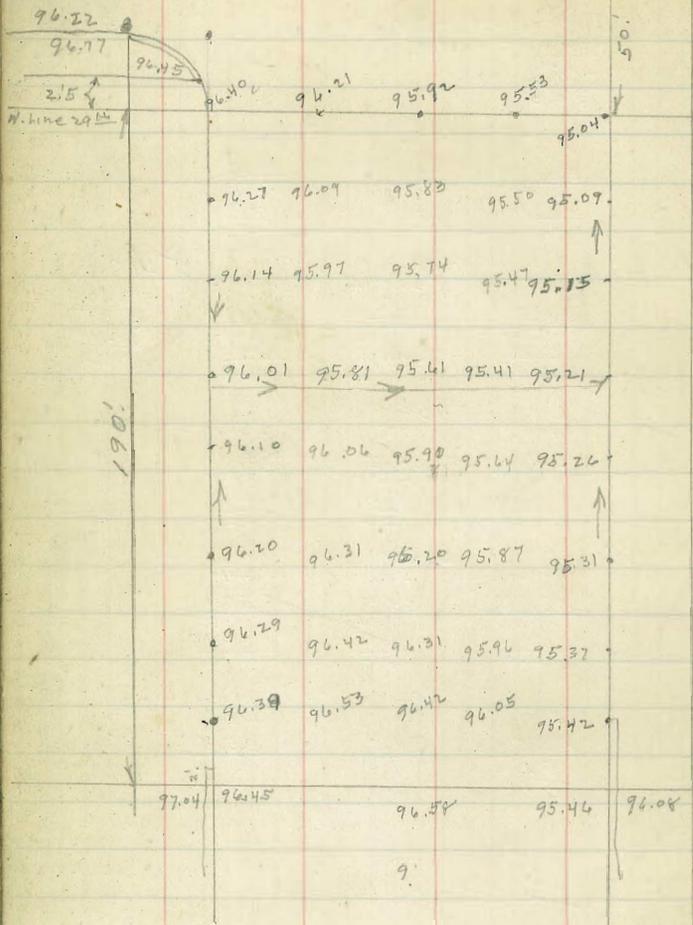
BM	8.19	58.81	50.62	54.0 Home Plate		
		4.81	54.0	54.0		
		11.421				
		0.0				
3 <sup>rd</sup> Base line						
100'		55.0	56.0	57.5		
		3.81	2.81	1.31		
		3.81	2.191	1.31		
		0.0	0.0	0.0		
22°-30'						
100'		54.5	55.25	56.0		
		4.31	3.56	2.81		
		4.31	Change	2.41		
		0.0		0.0		
45°-00'						
100'		54.0	54.5	55.0		
		4.81	4.31	3.81		
		4.81	4.31	3.81		
		0.0	0.0	0.0		
67°-30'						
100'		53.75	54.5	55.1		
		5.06	4.31	3.71		
		5.06	4.31	3.71		
		0.0	0.0	0.0		
90°-00'						
100'		53.5	54.5	55.8		
		5.31	4.31	3.01		
		5.31	4.31	3.01		
		0.0	0.0			

78

96.88  
96.97

B. St Pavmt. Grades  
28<sup>th</sup> to 29<sup>th</sup>

ch. inlet  
3-11-33  
Miller  
Walker  
Bliss.



220.14 N.C. 30<sup>th</sup> + B. Sts  
 0.20  
 220.34  
 11.74  
 208.60  
 0.37  
 208.97  
 10.09  
 198.88  
 1.80  
 200.68

Indexed  
C.S.K.

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Ray St Paving Grades  
Dwight to Myrtle

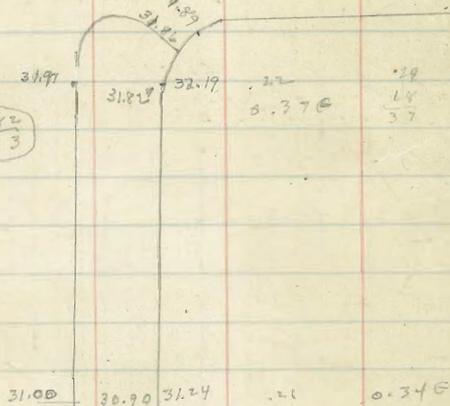
R.M. 331.90 N.E. Myrtle + 30<sup>th</sup> 332.46 N.E. Dwight + Ray  
 $\frac{337.95}{7.02}$   $\frac{337.95}{3.49}$   
 $\frac{337.95}{7.02}$   $\frac{337.95}{3.49}$

TP 336.93  
 $\frac{5.13}{336.06}$

d	Pav	
6.06	6.09	5.76
30.89	30.86	32.19
		34.97
		31.82
		6.13

d	Pav	
6.71	6.95	30.90
31.24	31.00	7.05

d	Pav	
7.17	7.30	30.53
30.88	30.65	7.42

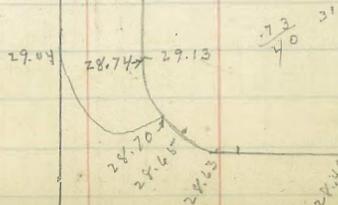


336.06

d		
6.93	7.02	6.70
29.13	29.04	

7.36	7.41	7.43	7.58
28.70	28.65	3	48

$\frac{28.74}{7.32}$



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not

IMPROVED TABLES

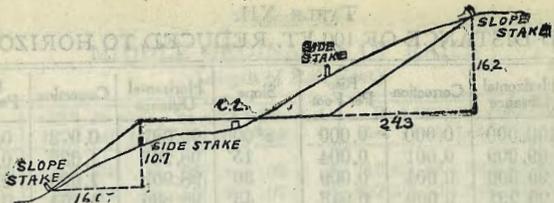
AND

INFORMATION

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections.

Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

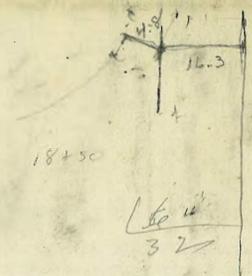
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

82.40  
44.68  
37.72

8.5  
7.8  
16.3

11-15  
12-15  
22-30  
11-15  
33-45  
11-25  
48-60  
11-15  
56-15  
67-30  
11-15  
74-45  
11-15  
90



7.8  
3  
4.8  
4  
2  
1.4  
24.

25.3  
24.2  
69.  
  
12.98  
69  
13.77

313.80  
756.90  
9  
165.90

11+90.44

48  
+54

308.57  
2.27  
311.84  
307.37  
4.47  
311.84

310.2

602.71  
22

293.4  
1.9  
291.5

30  
7.4

10.4  
2.4  
40.2  
13.2  
25.4  
26.68  
14.19  
40.87  
26.68  
67.55

35  
41.  
3.5  
37.5  
4  
41.5



13.5  
27.02

51.90  
18

10.00  
54.27  
35.33  
38  
26

1.90

47.72  
47.30  
42

38  
23  
47  
44

6.32  
54  
68.6

1.5

195.03  
45.

30.88  
95.91  
503.53

1460.44

55.86  
33.72  
109.58

57.54  
50.70  
48.7  
21

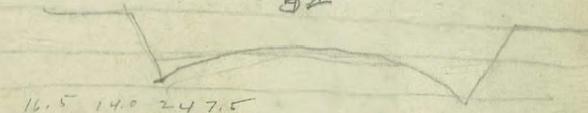
54.79

7.2

24  
10.5  
7.5

2182.11  
2184.79  
47.32

7.5  
4.5  
4.8  
3.2



1.2  
95  
100  
100  
10.7

18  
7.3  
10.7

8.000  
344  
560  
996  
640

91.5  
2.5  
94.0

31.6  
53

0.610

31.7  
56

532.0

47.72  
46.97  
294.65  
47.22

47.80  
46.30  
46.15  
46.85

48.04  
5.7  
42.20

46.93  
45.25  
42.24  
46.11

20+17.61

47.40  
46.30  
43.70  
46.85

192.137

7+20.30  
1+98  
8+28.20

16.47  
42.24  
5.73

11.70  
20  
31.70

179.60  
58-14  
121-46

47.20  
41.4  
42.8

17.97  
35.94

22.0187  
21.31

170.87  
35.44

9920.80  
9784.47  
154.33