

RIVERVIEW FARMS
CONTOUR TRAVERSE

W204

FIELD BOOK

No. 185F

W204

204

MICROFILMED
JAN 11 1965

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- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
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Stadia Traverse and
Topography to Locate
Surface Contours on
Riverview Farms, Lakeside
Farms and Surrounding
Basin.

Note - This survey was not
completed.

October, 1926.

Converse
Duermit
Butzine

B.M.# 55. 379.45
 0.76 380.21 11.46 368.75

Top Hub. S.W. Cor. El Monte Ranch Co.

B.S.	A.F.S.	L.R.	Vert. Δ	Rod	Hor. Dist.	Dif. Elev.	Elev.
E	165-21	-0-26	5.25	525	-4.0	369.1	
2	55-20	+10-47	2.10	203	+39	412	
D ₁	293-25	-7-22	0.75	74	-11	362	
C-D- H.I.=5.1							373.1
D	178-08	-0-09	5.55	555	-1.4	373.1	
2	179-05	-1-28	0.83	83	-2	372	
C ₁	297-45	-4-57	1.08	108	-9	365	
B-C- H.I.=5.0							374.5
C	51-30	+0-32	6.10	610	+5.7	374.5	
6	52-35	-0-12	5.30	530	-2	367	
5	47-40	+0-31	6.20	620	+6	375	
B ₄	33-50	+6-08	7.75	766	+82	451	
A	00	+8°43'	8.35	816	+125	493	
B ₃	00	+6°02'	6.20	613	+64.8	433.6	
B ₂	00	+2°04'	4.30	430	+15.5	384.3	
B ₁	0.0	+0°12'	2.21	221	+0.9	369.7	
A-B- H.I.=4.9							368.8

Note - "A" = N.E. Cor. Lot "O" Rancho
 El Cajon.
 "B" = S.W. Cor. El Monte Ranch
 Property.

⊥ of road.
 ⊥ of road.

Rod 6.9

N.W. Cor. F.A. Finer.
 S.W. Cor. E. Z. Hitt



(Note - Read from bottom, up.)

B.S. ΔFS	L R.	Vert L	Rod	Hor. Dist.	Dif. Elev.	Elev.
9	187-0	-0-32	4.37	437	-4.0	362
8	251-45	-0-53	3.13	313	-5.0	361
7	348-15	-0-29	2.95	295	-2.0	364
6	11-05	+0-20	4.45	445	+3.0	369
5	166-0	-0-22	8.48	848	-5	361
4	148-55	+4-34	10.55	1055	+89	450
3	110-35	+4-46	7.35	735	+61	427
2	124-10	+0-45	4.82	482	+6	372
F ₁	125-50	-1-06	1.47	147	-3	363

E-F H.I.=4.9

365.6

F	194-42	-0-13	9.18	918	-3.5	365.6
13	186-53	-0-16	8.15	815	-4	365
12	165-30	+0-13	9.55	955	+4	373
11	160-0	+2-03	10.90	1090	+39	408
10	145-40	+2-23	9.65	965	+40	409
9	145-15	+0-51	8.55	855	+13	382
8	131-50	+1-02	5.78	578	+10	379
7	116-40	+0-34	2.90	290	+3	372
6	110-10	+1-59	3.65	365	+10	379
5	92-05	+4-41	4.50	450	+37	406
4	26-25	+4-09	4.65	465	+34	403
3	14-35	+1-22	3.20	320	+8	377
2	272-45	-1-53	0.95	95	-3	366
E ₁	274-30	-1-56	1.55	155	-5	364

D-E H.I.=5.3

25' No. R.R. On Levee.

N.E. Cor. 10x12 Pump House + Well.

N. Cor. Barn

W. Cor. Farm House.

House over Well and Pump. N.W. Cor.

Bottom River Bed.

369.1 Note - "E" is 6" ft. No. Highway Pavement

B.S. ΔFS	LR	Vert L	Rod	Hor. Dist.	Dis. Elev.	Elev.	
7	8-55	+5-19	6.40	635	+59	424	
6	6-30	+0-02	3.68	368	0.0	365	Foot of Slope.
5	94-55	+0-20	5.80	580	+3.0	368	Foot of Slope
4	125-40	+0-14	6.63	663	+3.0	368	
3	169-55	+0-13	8.85	885	+3.0	368	
2	201-55	+0-24	5.65	565	+4.0	369.	Edge Willows.
I,	229-10	-0-22	3.55	355	-2.0	363.	Edge Willows.
H-I-	H.I.=5.0					365.2	
I	305-47	-2-48	7.75	775	-37.8	365.2	15' So. of S.W. Cor. Gilchrist Prop.
8	335-20	-4-49	5.10	510	-43	360	
7	48-15	-12-54	1.75	166	-38	365	
6	44-25	-8-36	2.97	290	-44	359	No. Bank
5	38-40	-5-11	5.17	508	-46	357	♀ River
4	42-35	-3-02	8.00	800	-42	361	So. Bank. River Channel 2' Lower.
3	94-30	-4-29	6.05	605	-47	356	♀ River Channel.
2	116-15	-4-04	5.50	550	-39	364	
H.I	138-25	+4-21	4.75	475	+36	439	
G-H-	H.I.=5.2					403.0	
H	192-11	+2-13	10.45	1045	+40.4	403.0	
3	216-45	-0-26	4.55	455	-3	360	No. Bank. River Channel 2' Lower
2	218-30	-0-53	2.60	260	-4	359	♀ River Channel.
G ₁	212-40	-1-24	0.99	99.	-2.4	360.	So. Bank. River Channel 2' Lower
F-G-	H.I.=4.7					362.6	
6	231-06	-0-23	4.48	448	-3.0	362.6	On Levee.
E-F-						365.6	

85.0 FS	L R	Vert L	Rod	Hor. Dist	Dif. Elev.	Elev.
L	220-54	+0-35	13.96	1396	+14.2	384.9
13	240-35	+0-07	10.60	1060	+2.0	373
14	235-55	+0-02	6.77	677	00	371
11	198-50	+0-11	3.25	325	+1.0	372
10	171-10	+0-27	7.05	705	+6.	377
9	139-05	+0-46	10.10	1010	+14	385.
8	150-20	+1-08	18.60	1860	+37	408
7	128-05	+0-56	17.90	1790	+29	400
6	107-0	+0-33	14.90	1490	+14	385
5	76-45	+1-50	13.00	1300	+42	413
4	62-15	+5-02	15.20	1508	+133	504
3	12-0	+4-11	6.55	655	+48	419
2	6-45	+0-37	4.80	480	+5.0	376.
K ₁	5-20	-0-24	3.65	365	-3.0	368
J-K-	H.I.=5.3					370.7
K	199-47	-2-11	7.68	768	-29.3	370.7
↓	227-30	-2-27	7.50	750	-32	368
3	252-20	-3-04	5.95	595	-32	368
2	305-10	-2-39	6.78	678	-31	369
J ₁	271-20	-15-04	1.42	133	-36	364
I-J-	H.I.=4.8					400.0
J	94-15	+1-54	10.50	1050	+34.8	4000
I ₈	84-55	+5-43	9.15	906	+91	456.0
H-I-	H.I.=5.0					365.2

Foot of Slope.

J.W. Cor. Wall + Pump House. 12' x 28'

Foot of Slope

B.S. & F.S.	L.R.	Vert. L	Rod	Hor. Dist.	Dif. Elev.	Elev.	
M	222-49	-0-11	11.10	1110	-3.6	387.3	
27	218-10	0-0	6.88	688	0.0	385	In Road
21	189-15	+3-56	7.90	790	+5.4	439	
20	196-55	+2-07	7.25	725	+2.7	417	Foot of Slope.
19	184-50	+3-02	6.50	650	+3.4	419	Windmill. Foot of Slope
18	151-55	+4-28	5.10	510	+4.0	425	385. Foot of Slope
17	158-10	+5-56	6.95	688	+7.1	456	
16	148-10	+5-36	8.60	852	+8.4	469	Foot of Slope Fe. Cor.
15	120-45	+4-08	9.45	945	+6.8	453	Foot of Slope.
14	102-35	+2-54	10.40	1040	+5.3	438	In Road
13	50-10	+0-49	5.65	565	+8.0	393	In Road
12	45-40	+0-17	2.93	293	+1.0	386	In Road.
11	350-15	-1-24	5.50	550	-1.3	372	
10	321-40	-2-25	3.05	305	-9	376	
9	260-30	-1-47	3.60	360	-11.	374	
8	231-25	-0-46	6.80	680	-9	376	
7	227-15	-0-28	10.10	1010	-8	377	
6	230-35	-0-30	14.80	1480	-13	372	Well + Pump House. 8x11. S.W. Cor. Concrete Tank. 40'x40'.
5	246-15	-0-24	15.40	1540	-11	374	
4	267-35	-0-37	12.50	1250	-14	371	
3	291-55	-0-46	11.70	1170	-16.	369	
2	322-50	-0-51	10.20	1020	-15.0	370	
L1	359-50	-0-44	10.25	1025	-13.0	372	Windmill + Tank. 30 ft West.
K-L-	HI-51					384.9	

B.S.A.F.S	LR	Vert L	Rad	Hor. Dist	Dif. Elev	Elev.	
8	189-05	-1-03	1.62	162	-3.0	371	
7	68-05	-0-12	2.33	233	-1.0	373	
6	66-10	+0-25	2.24	224	+2.0	376	Top Low Bank. Flood Channel.
5	214-05	-0-06	2.22	222	00	374	Top Low Bank. Flood Channel.
4	208-45	-0-48	2.30	230	-3.0	371	
3	202-45	-0-29	4.75	475	-4	370	
2	221-30	-0-05	8.10	810	-1.0	373	
0 ₁	266-40	-0-17	5.45	545	-3.0	371.	
N-0-	H.I. 54						374.2
0	271-33	0-00	11.40	1140	0.0	374.2	
10	271-33	-0-02	9.00	900	-1.0	373	
9	271-33	-0-04	7.80	780	-1.0	373	
8	271-33	-0-04	6.85	685	-1.0	373	
7	271-33	0-00	4.85	485	00	374	Intersection. Cottonwood Rd. + Riverside Drive
6	271-33	+0-09	2.75	275	+1.0	375	
5	91-33						Stone Mound on Hill.
4	41-50	+1-17	3.98	398	+9.	382	
3	50-55	+3-46	8.05	805	+53	427	
2	92-0	+2-55	2.05	205	+36	410	
N ₁	92-45	+0-56	3.30	330	+5.0	379.0	
M-N-	H.I. 54						374.2
N	190-57	-0-37	6.55	655	-7.1	374.2	"N" = N.E. Cor. Gilchrist Property.
2	216-10	-1-43	2.72	272	-8.	373	
M ₁	85-20	+4-06	2.87	287	+20	401.	
L-M-	H.I. 52						381.3

B.S. & F.S.	L.R.	Vert. L	Red	Hor. Dist	Dif. Elev.	Elev.	450
6	267-55	-7-37	5.65	560	-74	386	
5	298-05	-7-19	6.10	600	-77	383	
4	325-15	-8-51	5.05	495	-77	383	
3	296-40	-12-26	3.55	340	-74	386	
2	318-15	-15-47	1.80	165	-47	413	
5 ₁	21-45	+1-58	1.60		+6.0	466.0	

N-5- H.I. = 5.2 459.5

5	105-22	+3-37	13.90	1390	+87.5	459.5	
13	150-15	+0-22	7.75	775	+5.0	377	
12	149-40	+0-17	7.98	748	+4.0	376	
11	189-15	+0-14	7.40	740	+3.0	375	

M-N- H.I. = 5.3 372.0 Corrected.

C	146-11	+1-43	3.50	350	+10.5	376.8	374.5
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Q-R- H.I. = 4.7 366.3

R	156-24	-0-28	4.32	432	-3.5	366.3	
3	164-40	-2-50	0.46	46	-2.0	368	
2	245-25	+0-31	3.42	342	+3.0	373	
Q ₁	247-55	+0-12	3.28	328	+1.0	371	

P-Q- H.I. = 5.2 369.8

Q	182-48	-0-28	2.70	270	-2.2	369.8	
P ₁	181-50	-0-20	1.22	122	-1.0	371.0	

O-P- H.I. = 5.3 372.0

P	188-57	-0-13	5.72	572	-2.2	372.0	
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N-O- H.I. = 5.4 374.2

BS. Δ F.S.	L.R.	Vert. L	Rod	Hori. Dist	Dif. Elev.	Elev.
W	133-56	+1-11	9.00	900	+18.6	4122
12	134-10	+1-31	7.05	705	+19	413
11	134-10	+1-35	4.55	455	+13	407
10	273-10	-0-14	7.90	790	-6	388 Rod-8.2
9	237-05	+0-41	11-20	1120	+13	407
8	234-25	+1-56	12.80	1280	+43	437
7	200-20	+0-33	9.85	985	+9.0	403
6	182-15	+2-05	18.90	1890	+6.8	462
5	182-15	+1-19	15.60	1560	+3.6	430
4	182-15	+0-22	13.20	1320	+10	404
3	182-30	+1-04	10.65	1065	+20	396
2	184-20	-0-23	3.25	325	-2.0	392
V ₁	239-15	-1-16	2.95	295	-7.0	387
U-V-	H.I.:5.2					393.6
V	172-10	+0-26	5.36	536	+4.0	393.6
√	172-10	+0-32	2.65	265	+2.0	392.
U ₁	120-40	+0-59	5.32	532	+9.0	399.
T-U-	H.I.:5.4					389.6
U	118-57	-0-12	1.18	118	-0.4	389.6
S-T-						390.0
T	233-02	-3-43	10.75	1070	-69.5	390.0
8	244-35	-4-13	9.80	975	-72	388
S ₁	217-0	-11-43	3.28	315	-6.6	394
N-S-						459.5

B.S.A.F.S.	LR	Vert L	Rod	Hor. Dist	Dif. Elev.	Elev.
+	251-10	-0-08	10.10	1010	-2.0	384
3	220-05	0 0	15.00	1500	00	386
✓	218-40	-0-02	8.00	800	-1.0	385
X	275-10	-0-14	5.85	585	-2.0	384.

U-X- H.I.=5.3

385.6

X	264-09	-0-11	12.55	1255	-4.0	385.6
8	264-35	-0-23	7.05	705	-5.0	385
7	223-15	+0-01	4.40	440	00	390
6	265-05	-0-32	3.34	334	-3.0	387.
5	353-30	-0-32	14.80	1480	-14	376
4	353-35	-0-28	8.75	875	-7.0	383
4/3	354-05	-0-20	3.90	390	-2.0	388

T-U- H.I.=5.3

389.6

9	224-0	+1-46	4.20	420	+13	425
8	222-35	+4-54	6.35	635	+53	465
7	180-45	+1-31	6.24	624	+16	428
6	180-45	+1-22	11.70	1170	+28	440
5	125-35	+1-09	8.90	890	+18	430
4	123-25	+5-07	11.30	1120	+100	512
3	91-05	+3-11	11.10	1110	+62	474
✓	89-0	+0-10	8.20	820	+2	414
W1	88-0	-1-15	3.35	335	-7.	405.

V-W- H.I.=5.3

412.2

12.55
 .32
 2510
 3765
 40.160

B.S.A.F.S.	L.R.	Vert. L	Roof	Hor. Dist	Dif. Elev	Elev.
12	133-50	+0-53	5.85	585	+9	400
11	122-55	+0-26	3.48	348	+3.	394
10	116-35	+2-01	5.40	540	+19	410
9	80-15	+1-20	7.70	770	+18	409
8	55-15	+0-01	5.55	555	00	391
7	58-40	+0-39	7.80	780	+9	400
6	43-10	+0-03	8.90	890	+1.0	392
5	309-40	-0-12	8.65	865	-3.	388
4	287-0	-0-08	14.10	1410	-3.0	388
3	256-20	0-0	9.70	970	00	391
2	250-35	+0-01	5.70	570	00.	391
1	221-40	+0-07	5.98	598	+1.0	392

X-4- H.I.-5.3

390.6

4	180-49	+0-11	15.50	1550	+5.0	390.6
14	181-0	+0-09	11.05	1105	+3.0	389
13	181-00	+0-09	5.35	535	+1.0	387
12	159-05	+0-13	5.85	585	+2.0	388
11	142-50	+3-13	6.10	610	+34	470
10	123-65	+4-28	7.45	740	+58	444
9	88-25	+2-11	6.70	670	+25	411
8	88-25	+0-14	4.08	408	+2.0	388
7	45-20	+0-01	3.12	312	00	386.
6	308-40	-0-06	7.65	765	-1.0	385
X5	293-05	-0-13	15.20	1520	-6.0	380

U-X-

385.6

15.2
38
1216
456
5776

15.5
32
310
465
4960
141
23

423
288
3243

B.S. & F.S.	∠ R.	Vert. L	Rod	Hor. Dist	Dif. Elev	Elev.	
2	207-10	0.0	3.94	394	0.0	394	
IV 1	7-35	+0-24	1.14	114	+1.0	395	So Bank Main Channel.
II-IV-	H.I.=5.0					393.5	
Δ IV	198-07	-0-04	6.40	640	-0.8	393.5	
Δ III	202-49	-0-10	3.15	315	-1.0	393	∠ River Channel.
6	203-10	-1-19	0.92	92	-2.0	392	North Edge river channel.
5	276-35	+0-12	5.40	540	+2.0	396	Rod 7.9
4	277-30	+0-16	3.35	335	+2.0	396	
3	268-55	+1-09	2.34	234	0.0	394	Rod 10.4 N.E. Cor. Well + Pump House.
2	357-15	+1-53	0.70	70	+2.0	396	
II 1	337-55	+0-15	4.32	432	+2.0	396	N.E. Cor. Lakeside Farms Mut. Water Cos. Pump House.
Z-II-	H.I.=5.4					394.3	
Δ II	218-38	-1-12	5.76	576	-12.0	394.3	
3	174-55	+2-05	3.70	370	+13	419	
Z 2	186-45	-0-19	4.00	400	-2.0	404	
Z 1	185-05	+0-32	1.63	163	+2.0	408	
4-Z-	H.I.=5.3					406.3	
Z	183-08	+0-32	14.10	1410	+15.7	406.3	
18	181-10	+0-25	10.60	1060	+13	404	
17	179-10	+0-12	7.95	795	+3.0	394	
16	166-20	+1-42	11.75	1175	+35	426	
15	154-20	+2-47	13.40	1340	+65	456	
14	153-40	+2-08	10.50	1050	+39	430	
4/13	153-0	+0-31	6.45	645	+6.	397	
X-4-						390.6	

BS. Δ.F.S. L.R Vert L Rod Hor. Dist Dif. Elev. Elev.

BS. Δ.F.S.	L.R	Vert L	Rod	Hor. Dist	Dif. Elev.	Elev.
VI	176-50	+0-10	14.60			
V-VI	H.I. = 5.3					
VI	219-27	-0-10	13.90	1390	-4.0	392.7
14	212-40	-0-07	11.85	1185	-2.0	395
13	192-40	-0-04	8.90	890	-1.0	396
12	106-35	00	1.12	112	00	397
11	169-40	+0-02	6.85	685	00	397
10	168-20	-0-09	3.67	367	-1.0	396
9	195-40	-0-19	2.32	232	-1.0	396
8	208-40	-0-25	6.80	6.80	-5.0	392
7	229-30	-0-15	10.30	1030	-5.0	392
6	241-20	-0-13	14.80	1480	-6.0	391
5	252-50	-0-17	12.60	1260	-6.0	391.
4	257-0	-0-11	8.70	870	-3.0	394
3	260-50	-0-03	6.15	615	-1.0	396
2	272-45	-0-14	3.77	377	-1.0	396
I	291-20	-0-30	1.82	182	-1.0	396
IV-V	H.I. = 5.2					396.7
V	205-52	+0-17	6.56		+3.2	396.7
II-IV						393.5

N.W. Cor. Well + Pump House.

Top Bank

" "

Top Bank

12
12.6
5
6.3

38

44

14.8
34
59.2

10.3

44

412

412

11.85

2

2370

13.9

29

1251

278

4031

14.6

29

1314

292

4234

Prop. line survey in Miss. Res. Basin

35+65²⁰ P.I. 95°52'44"

34+04⁸² P.O.T

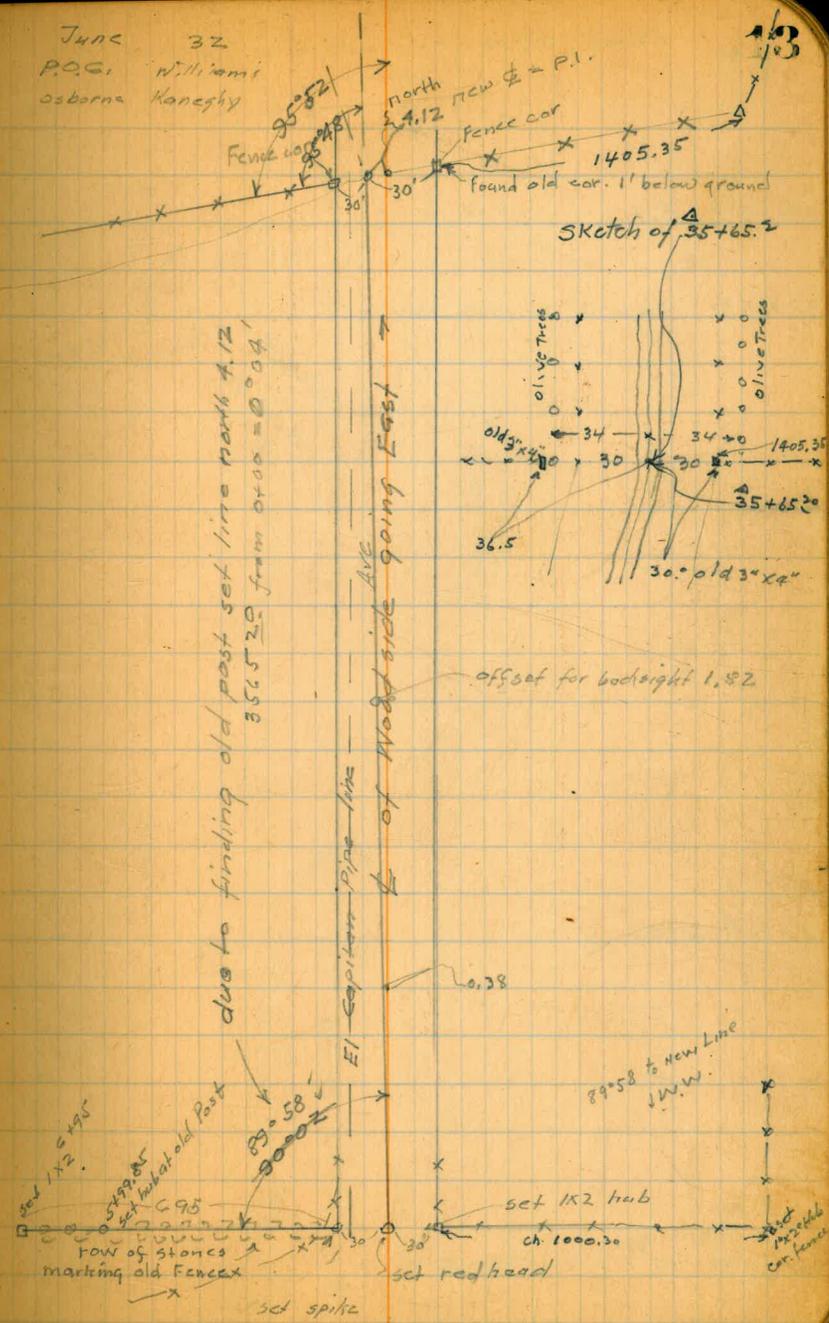
16+32⁸⁴ P.O.T

3+28⁹⁰ P.O.T

7+25⁰⁰ P.I. 89°58'44"
70+00 East on Woodside

this
 is
 the
 old
 fence
 line
 1000 ft
 long

June 32
P.O.G. Williams
Osborn Kaneghy



Prop. survey in Miss Res Bas.

61+34.25 P.I. 69°45L+

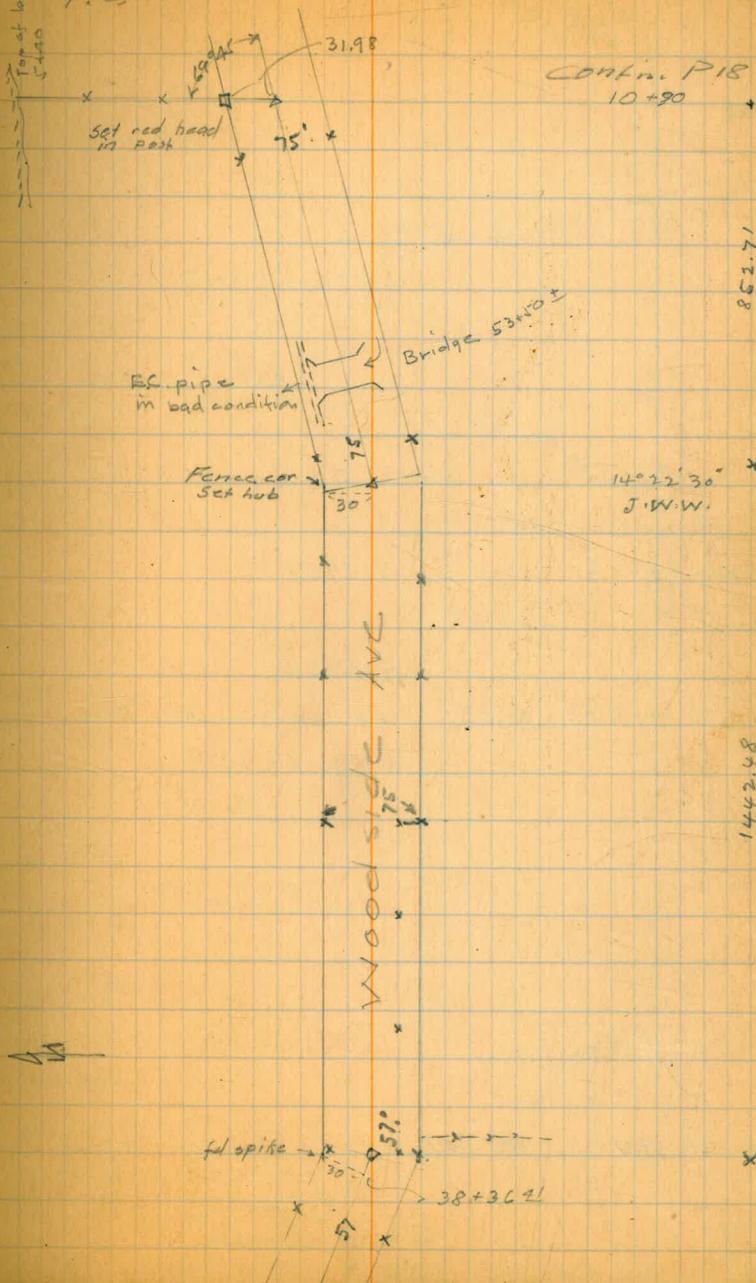
52+81.54 P.I. 14°22L+

52+77.75 oppos Fence cor.

38+39.06 P.I. 10°04L+

June N-32
P.O.G.

15



Mission Res. Prop line Survey

June 16-32
P.O.C

		47°34.5
		90°34.5
2448.6 =	3.388811	179.60
sin 48°51 =	9.824245	138.09.0
	3.213163	41.51
sin 47°34 1/2	9.868151	
	3.345012 =	2213.16
	49.81	
	31	
	196	
	114	

Stadia line east from 22215 point east

Sec. Cor 29-19
25-30

Stadia east 375

from 22215 2596.5

Point 2020

4616.5

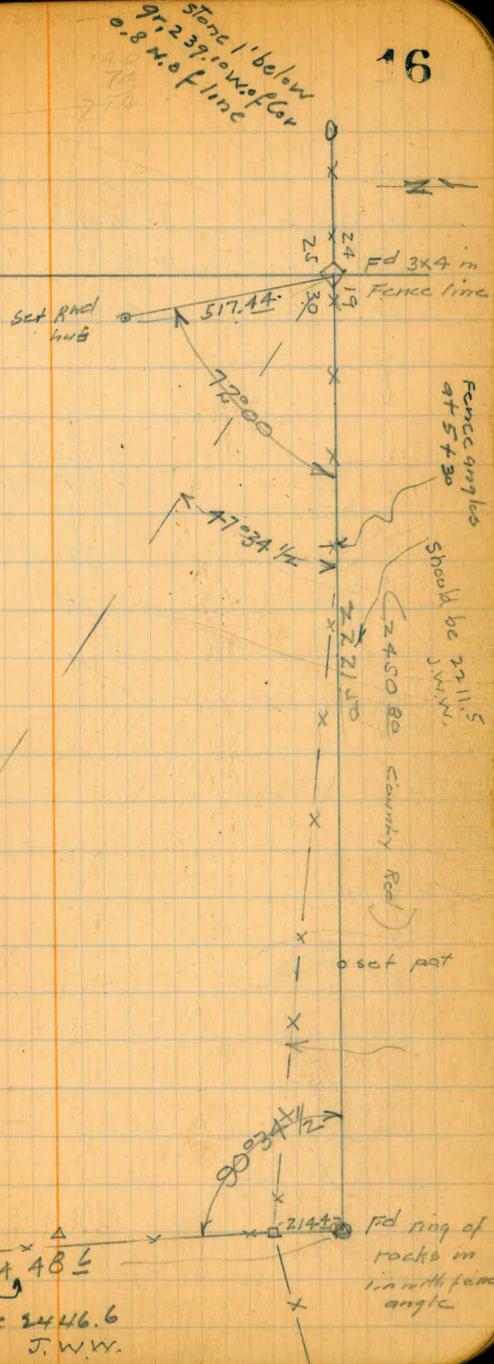
at 46+16 S C° 14 L⁺ 4 55

to sec. cor 3x4 stake in rock mound

5071.5

0+00 P.I. 90°34 1/2 ft from Sec. Cor

24-19
25-30



Set Rod hub

Should be 2446.6
J.W.W.

Miss. Res. Survey of Prop. line

$$\begin{array}{r} 83 \\ 3156.5 = 3.499137 \\ \sin 35^{\circ}50'20'' \quad 9.767533 \\ \hline 3.266753 \\ \sin 89^{\circ}40'10'' \quad 9.999993 \\ \hline 3.266760 = 1848.24 \\ \begin{array}{r} 02 \\ 58 \\ 47 \\ 11 \end{array} \end{array}$$

$$\begin{array}{r} 83 \\ 3156.5 = 3.499137 \\ \sin 54^{\circ}29'30'' = 9.910641 \\ \hline 3.409861 \\ 89-40-10 \quad 9.999993 \\ \hline 3.409868 = 2569.62 \\ \begin{array}{r} 9764 \\ 104 \\ 101. \\ 34. \end{array} \end{array}$$

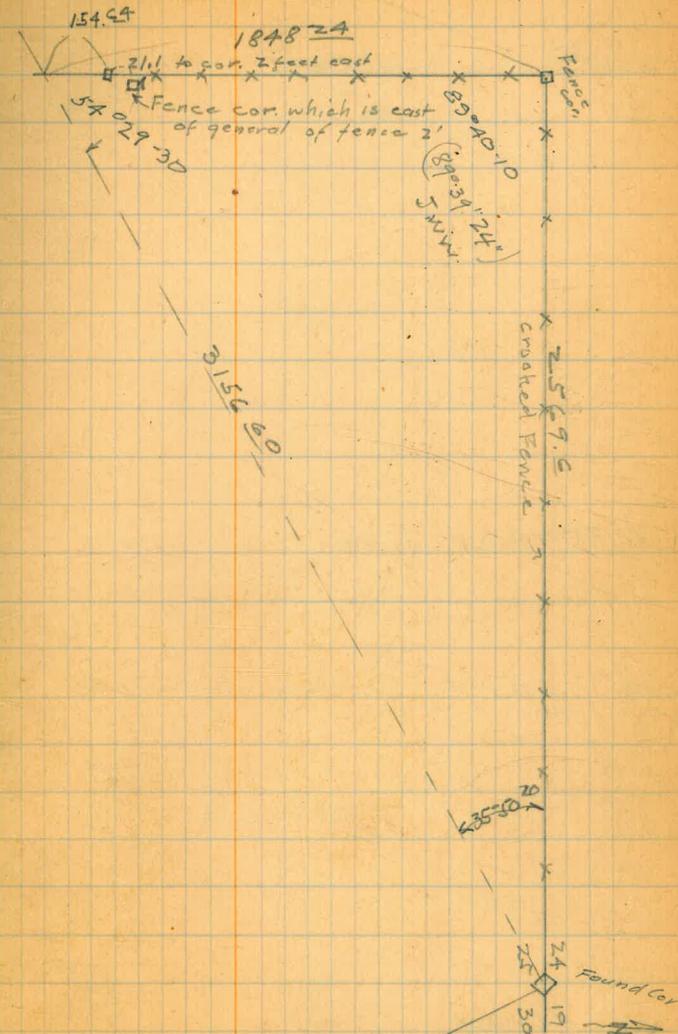
June 17-32
P.O.C

2910596
45
641

767475
50
767533

17

Set hub back toward Fence to make red. dist. = 1993.6



Prop line Survey in Misc. Res continue
from P 15

27+64⁸⁸ P.I. 90°00Rt. trying with stadia
to find sea cor. east

13+64⁸⁸ P.O.T

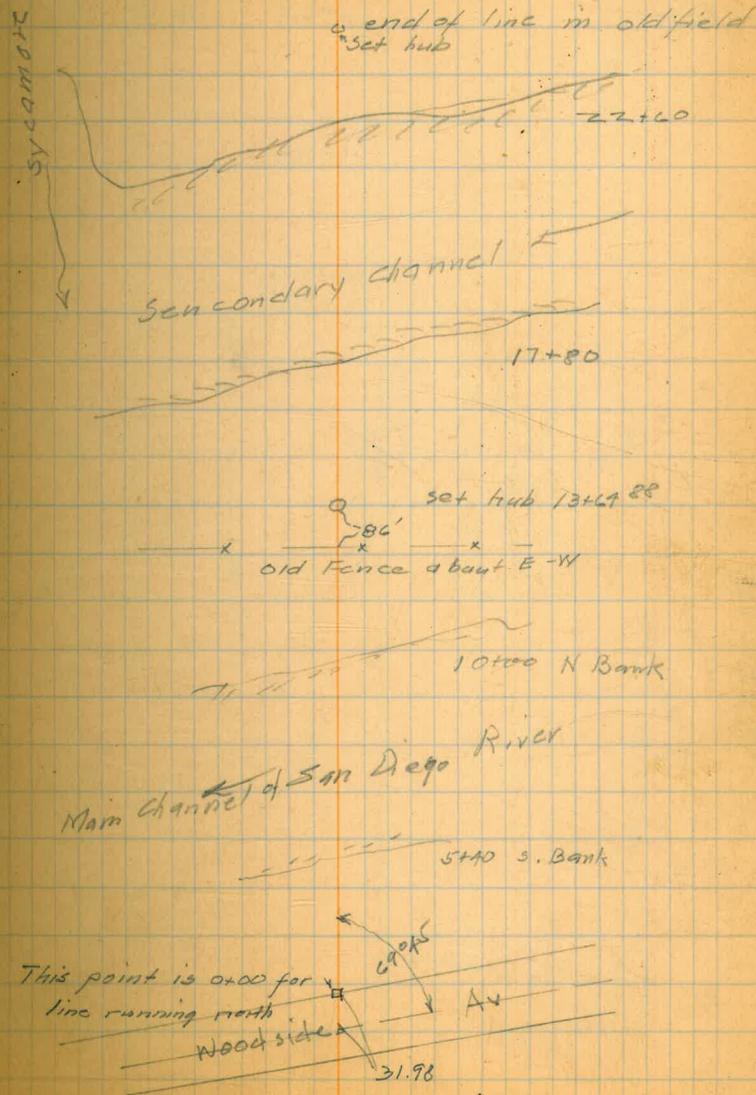
10+90 P.O.T

0+00 = 31.98 north

61+34³⁵ P.I. 69°45L*

June 17-32
P.O.G

18



Lat 19+0087

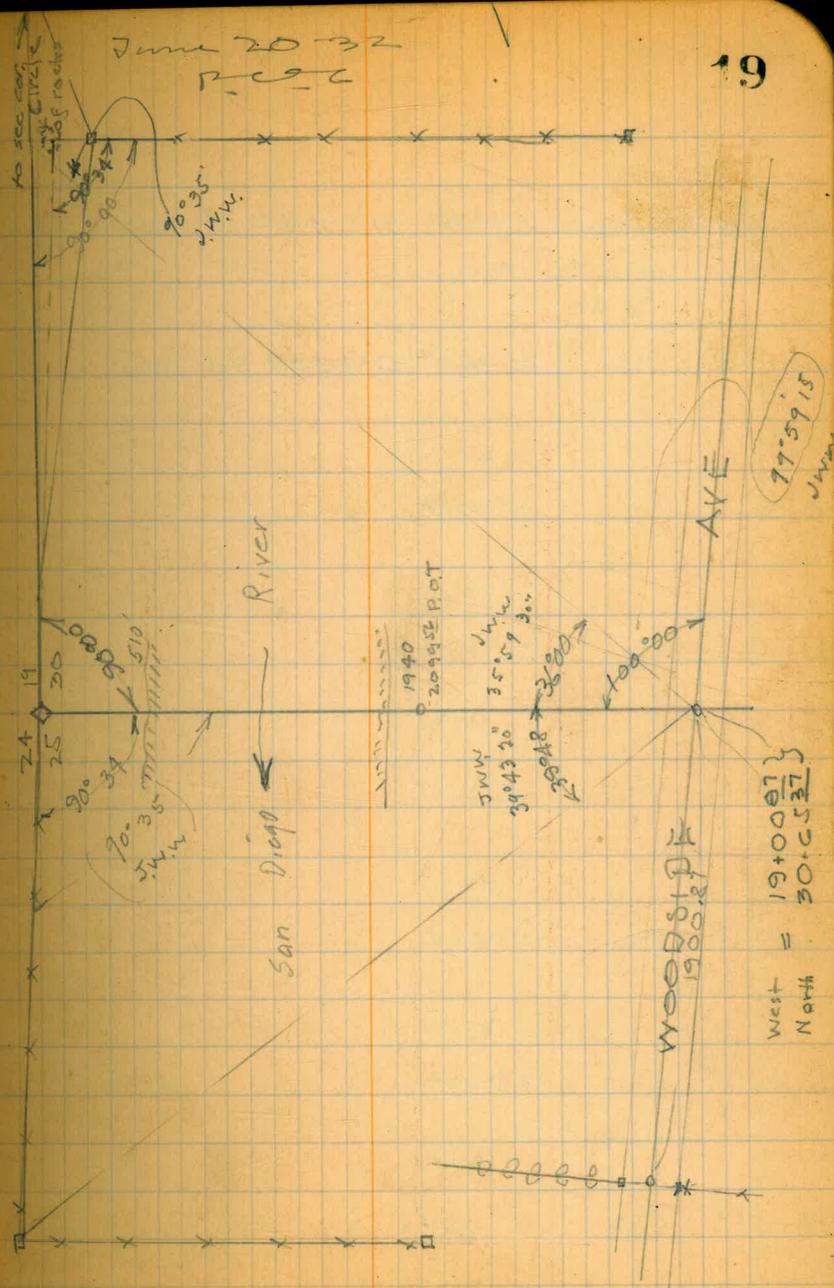
39°44'
79°28'

30°00'
73°00'

100°00'
200°00'

20+99.56 P.O.T

520.68



Prop. line. Contin.

56+71.02 P.I. 107°04'
 = 440 south of 24°08' 107°04' Lt to E Woodside
 Woodside 44+36.70

50+62.75 P.I. 2°45'RT 0°47'RT to hub

45+71.95 P.I. 35°00'RT

37+95.55 P.I. 31°00'RT

27+39.55 P.I. 35°00'Lt

14+85.55 P.I. 1°00'Lt

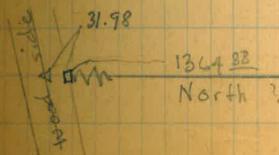
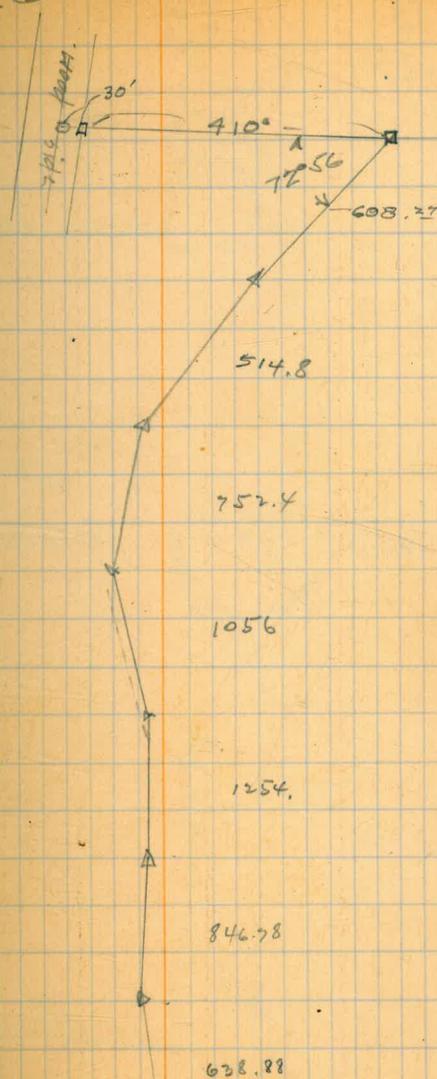
6+38.88 P.I. 16°00'RT

13+64.88 P.I. 115°30'Lt
 = 0+00

June 20-32
 P.O.C

20

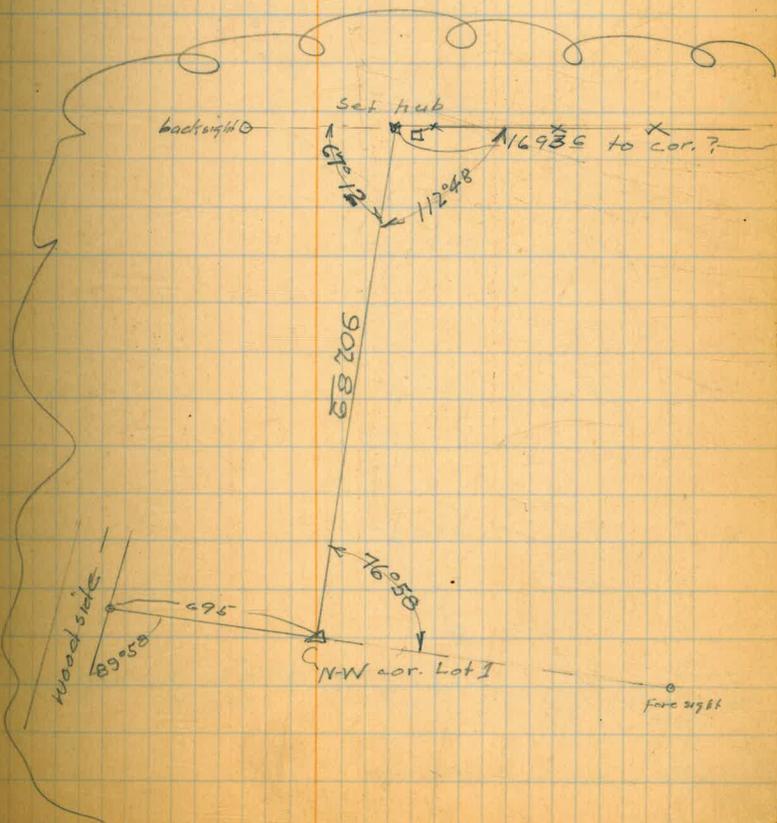
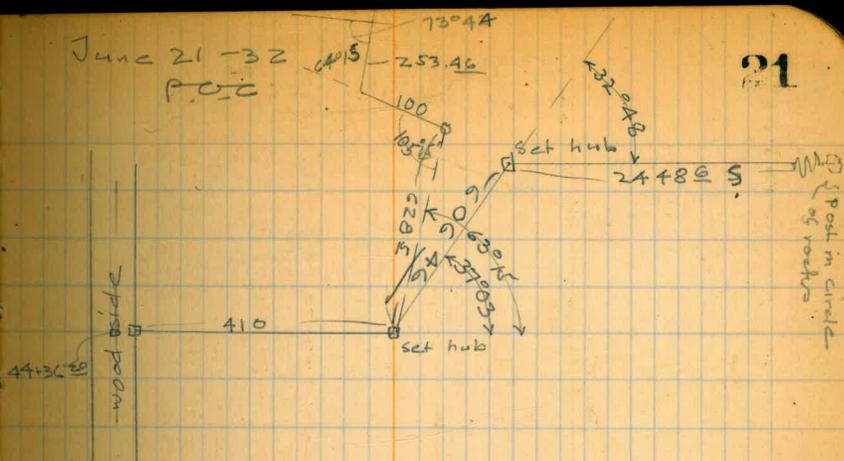
Sta. 8+71



Prop. lme. Survey contin.

June 21 - 32
P.O.C.

21

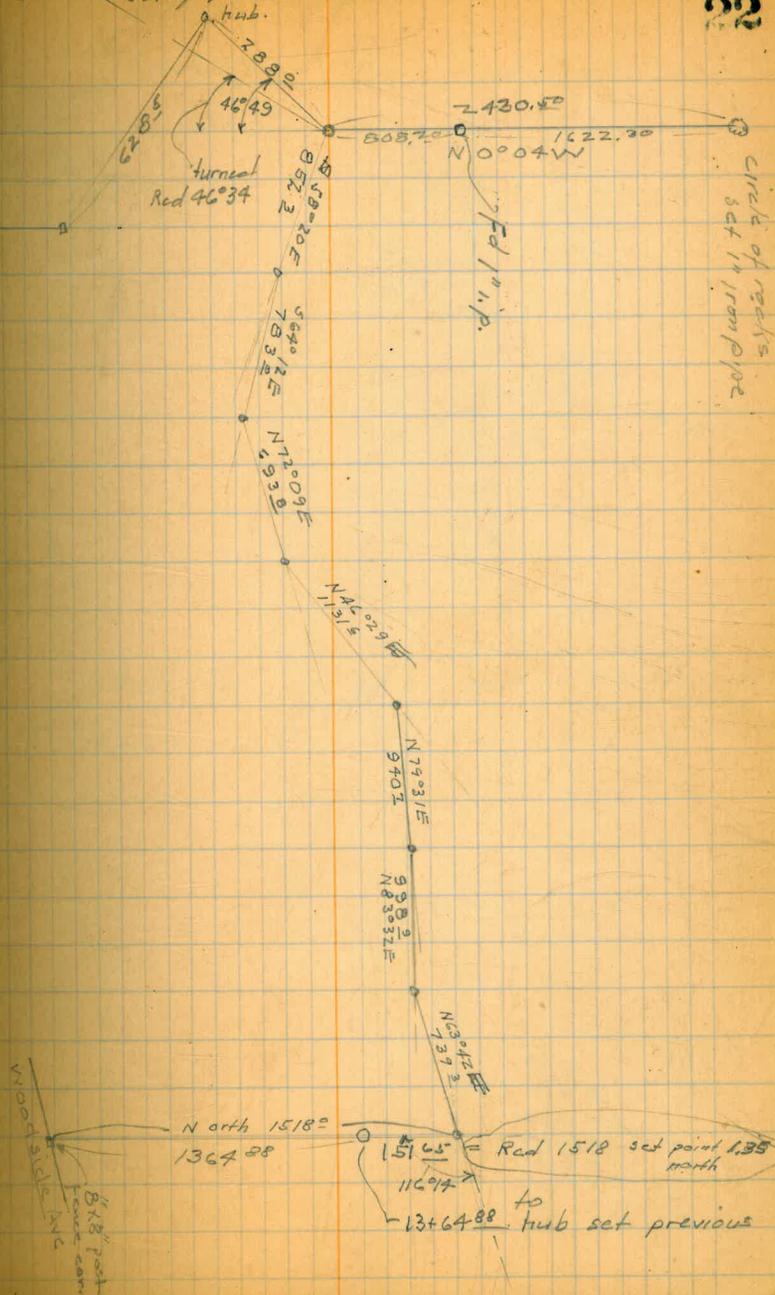


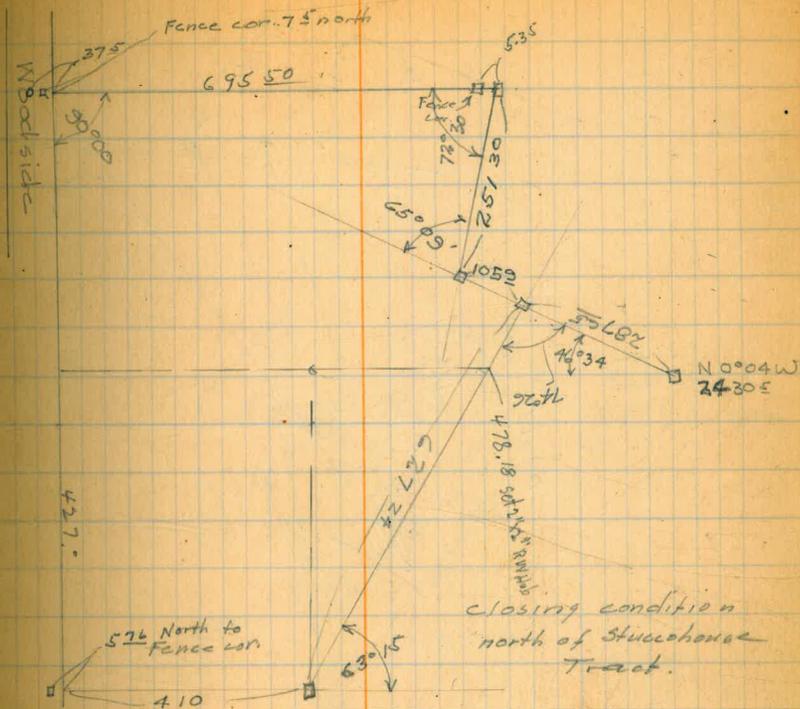
Resurvey of Rumsey line
(same as p-20)

0	P.I.	$58^{\circ}16' L$
1	P.I.	$5^{\circ}52' L$
2	P.I.	$43^{\circ}39' L$
3	P.I.	$25^{\circ}40' L$
4	P.I.	$33^{\circ}02' R$
5	P.I.	$4^{\circ}01' R$
6	P.I.	$19^{\circ}50' L$
7	P.I.	$116^{\circ}12' R = 116^{\circ}14'$ turned angle

Aug July 7 -32

22





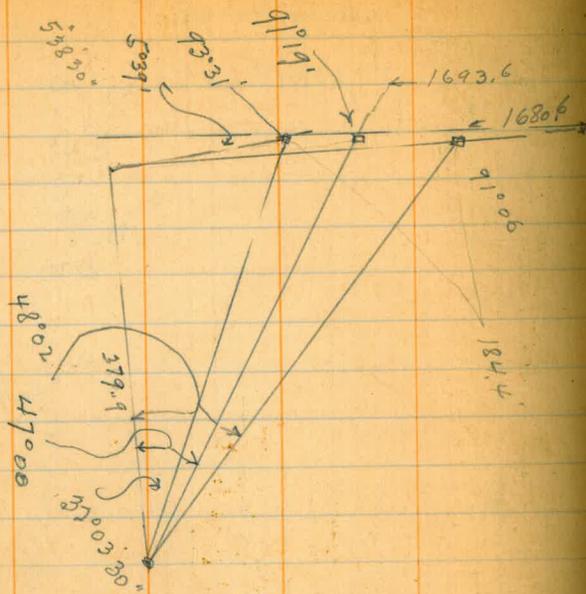
89°60	
63°15	
26°45	
111985	7
427	4
783895	
223970	
447945	
47817595	

Prop line Survey contin.

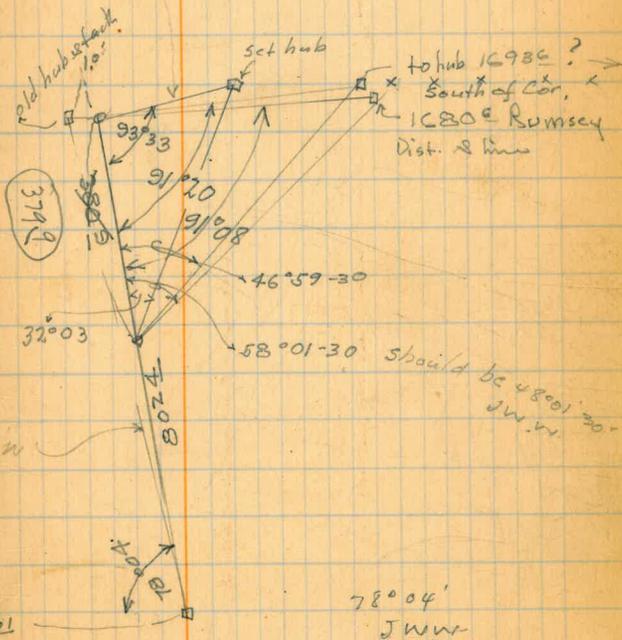
P. O. G.
July 2-9-32

24

2.
9004
1117

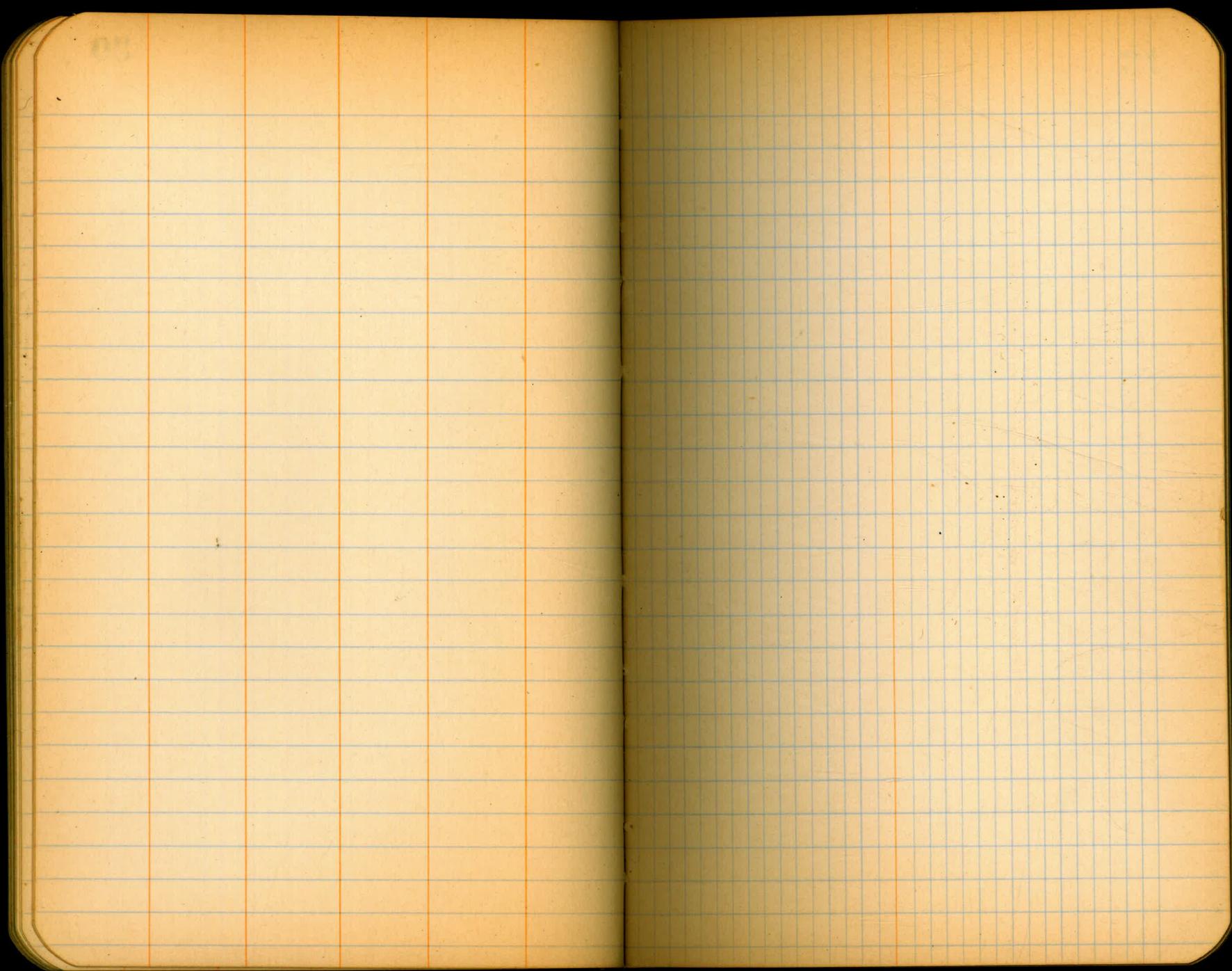


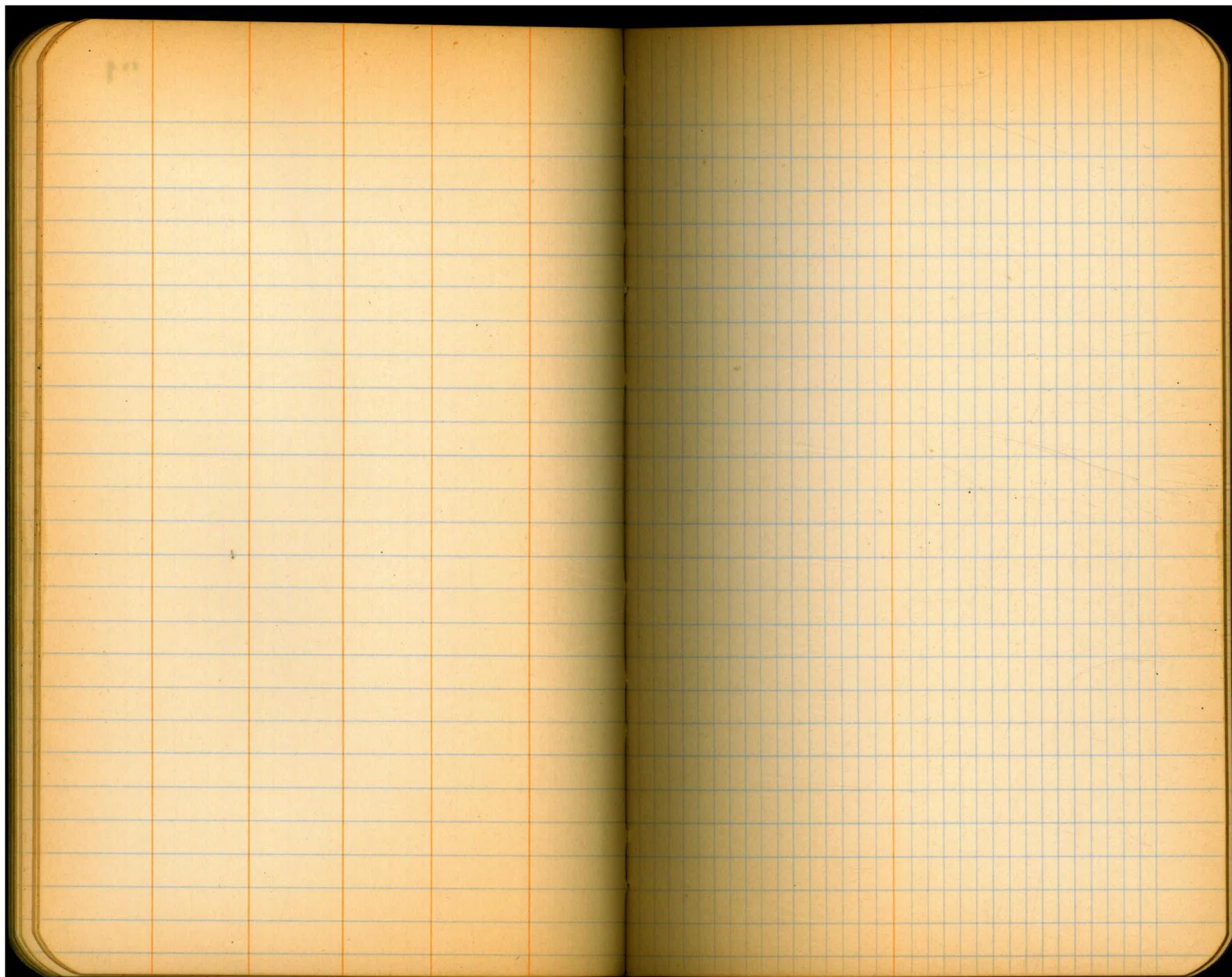
see p-13 →



rais point

78.04'
JWW





57

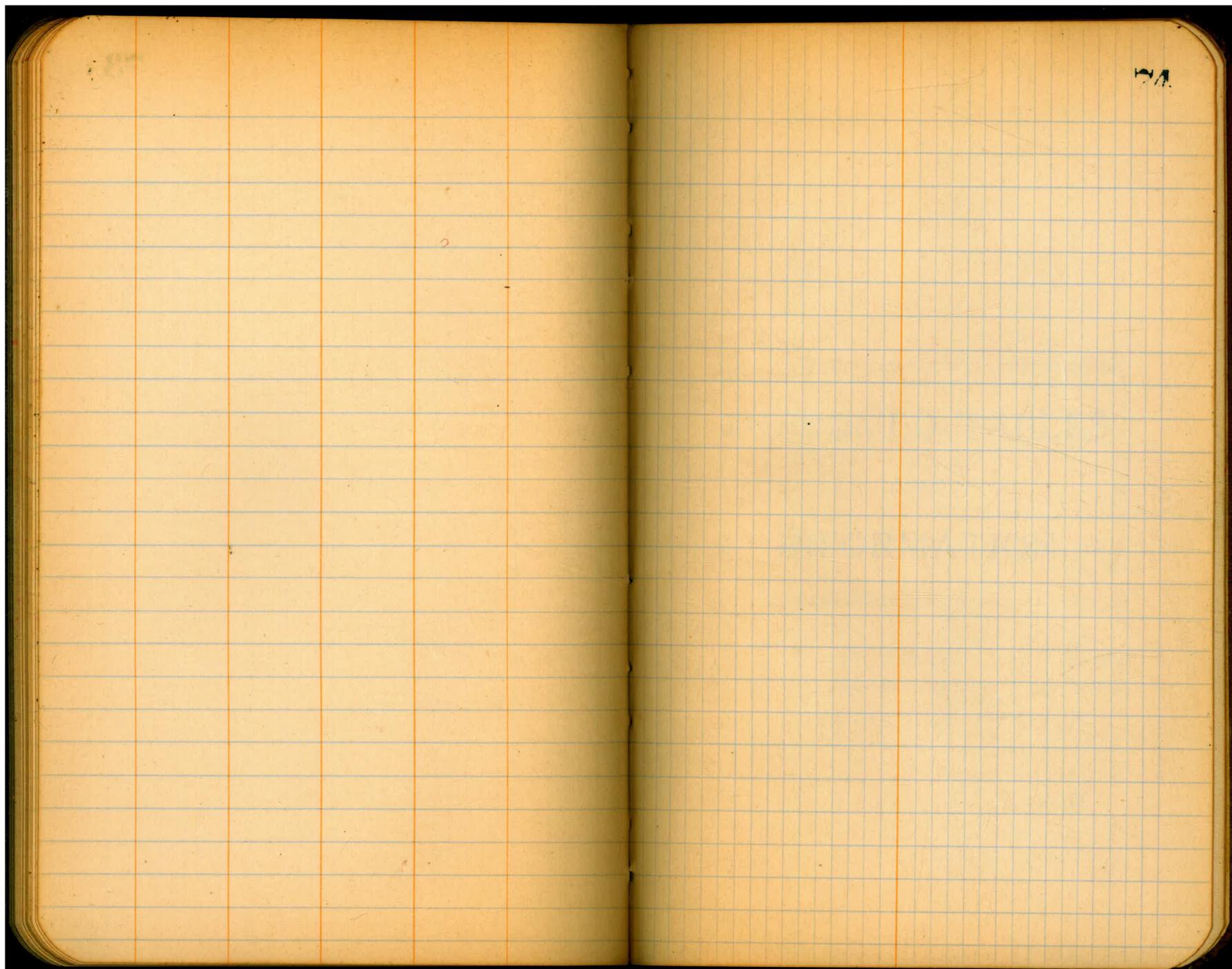
58

64

65

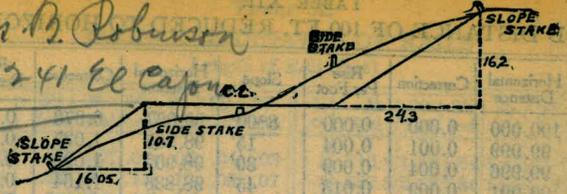
03

71



24

Thos B. Robinson
 P.O. 241 El Capitan, Cal.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

89° 58' West to North
 Set 1 x 2 c 95 North
 P.O.T 599.85 P.O.T on Post

100° 01'

3565
 .00115
 7.12000
 3565
 5580
 3565
 19850
 17825

1633
 .00115
 8165
 1633
 1633
 187795

329
 .00115
 1645
 329
 329
 37835

179 50
89°58'

99 59 15
4 399 57

42 92

437 49
402 92

34 57
45
35 02

180
57
4) 237 59
20
37
36
10

5' 30"

527775
383641.
1441.34
1434.09
200
81.57
1846

2.02
5 24

200.00

140.00

39.63

377.63

2.48

380.05

4

179 59 60

165-37-30

14 22 30

179-59-60

101-50-30

78° 09' 30"

5 30

78° 4' 00"

.65 = 9.812913
421.5 = 2.624798
7.188115

5' 30"

6-271-55
91-33

180 22

#55-495+82 9' L.

379.25

27.1-35
91 33

19.0-02

4.32

3.5

81

.08

432

.286

3456

3.4772

294

93.5

1470

492

10.290

4.32

.01

.0432

695
2
1390

4.94

5.46

29 6 4

197 6

2.27 2 4

46

2.4

184

92

1.104

200

3906

100.97

34 00

1.0

1000 = .6

2000 = .12

3000 = .18

.30

1.02

4.13 3404.82
160 37

3565.19

0.0017

4.130000

3565.19

564810

356519

2082910

801.4

4621.5

379.9

47	70.00	70
48	72.00	72
49	73.50	73
60	75.00	75