

SUTHERLAND SAN VICENTE CDMIT

Level Notes
Dam To Tunnel
L. L. L" Lines

PASTS

LEVEL BOOK

No. 380

W238

8

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Pages - 1 to 22 Inc. = L Line

Pages - 58 to 64 Inc. = L" Line

Pages - 67 to 73 Inc. = L' Line

Profile Levels over Line
Starting from New DAM
Axis, 0100, and continuing
South and West.

This line is marked L

JAN. 17, 1928
Simpson
Clavert.

1.

Sta.	+	H.I.	-	Elev.
				1931.44 = E.I. S.D.B.M.
	8.25	1939.69		"B" near Dam Axis
1+00			7.7	1932.0
+50			11.7	1928.0
2+00			19.7	1920.0
+50			21.0	1918.7
3+00			14.2	1925.5
+30			5.3	1934.4
+50			5.6	1934.1
T.P.			1.69	1938.00
	12.77	1950.77		
0+00			8.5	1942.3
3+75			8.7	1942.1
4+00			6.4	1944.9

Sta.	+	H.I.	-	Elev.
		1950.77		
4+50			4.9	1946.4
+80			1.7	1949.1
5+00			6.1	1944.7
+20			8.9	1941.9
+93			3.3	1947.5
6+00			9.1	1941.7
+45			1.2	1949.6
T.P.			1.40	1949.37
	1.02	1950.39		
+70			7.6	1942.8
7+00			7.1	1943.3
+50			6.1	1944.3

See Vol "N-1"

Line

2nd R.F. is 10²
Lower than Line
1943.3

2/28 checked JRM

Sta.	+	H.I.	-	Elev.
		1950.39		
8+00			5.4	1945.0 ✓
+46	^H P.I.		9.6	1940.8 ✓
+67			3.0	1947.4 ✓
T.F.			11.63	1938.76 ✓
	10.72	1949.98		
9+00			12.8	1936.7 ✓
+50			14.8	1939.7 ✓
10+00			14.4	1935.1 ✓
+50			10.1	1939.4 ✓
11+00			5.1	1944.4 ✓
+02	^H P.I.		5.1	1944.4 ✓
+50			1.1	1948.4 ✓ 1938.4

Sta.	+	H.I.	-	Elev.
		1949.48		
12+00			5.1	1944.4 ✓
T.F.			1.14	1948.34 ✓
	12.05	1960.39		
			5.6	1954.8 ✓ 32 R. 155 is Lower than Line
13+00			5.0	32 R. 155 is Lower than Line 1955.4 ✓
+15			11.3	1949.1 ✓
+50			8.0	1952.4 ✓
+78	⁵⁵ P.I.		6.0	1954.4 ✓
14+00			8.8	1951.6 ✓
T.F.			12.35	1948.04 ✓
	6.02	1954.06		
T.F.			12.31	1941.75 ✓
	0.62	1942.37		

NOT

USE 155

LINE HERE IS ON EARTH FILL

2/2/08 checked JF, new count

Sta.	+	H.I.	-	Elev.
		1942.37		
14+50			5.4	1937.0 ✓
15+00			13.3	1929.1 ✓
+26	²⁸ P.I.		10.4	1932.0 ✓
T.F.			10.74	1931.63 ✓
	3.81	1935.49		
+50			4.1	1931.3 ✓
16+00			4.6	1930.8 ✓
+50			5.10	1930.3 ✓
17+00			4.7	1930.7 ✓
+50			4.7	1930.7 ✓
T.F.			1.65	1933.79 ✓
	1.86	1935.65		
18+00			2.0	1933.6 ✓

Sta.	+	H.I.	-	Elev.
		1935.65		
18+50			4.0	1931.6 ✓
19+00			5.0	1930.6 ✓
+50			6.3	1929.3 ✓
20+00			5.0	1930.6 ✓
+50			4.6	1931.0 ✓
21+00			5.5	1930.1 ✓
+50			5.1	1930.5 ✓
T.F.			6.43	1929.22 ✓
	4.89	1934.11		
22+00			5.7	1928.4 ✓
+35	top of 8"x5" Boulder		0.0	1934.1 ✓
+50			3.6	1930.5 ✓

V.I.V. 11/15
 1935

checked
 2/1/36
 J.P.M.

Sta.	+ -	H.I.	-	Elev.
		1934.11		
22+90	³⁰ P.I.		4.7	1929.4 ✓
23+00			5.2	1928.9 ✓
+50			8.4	1925.7 ✓
+86			13.8	1920.3 ✓
24+18			27.1	1907.0 ✓
24+50			14.4	1919.7 ✓
25+00			10.9	1923.2 ✓
+50			7.0	1927.1 ✓
T.F.			7.17	1926.94 ✓
	4.24	1931.18		
+63	³⁰ P.I.		4.0	1927.2 ✓
26+00			7.1	1924.1 ✓

Sta.	+ -	H.I.	-	Elev.
		1931.18		
26+50			8.8	1922.4 ✓
27+00			6.2	1925.0 ✓
+25	⁰⁰ P.I.		5.1	1926.1 ✓
+50			3.7	1927.5 ✓
28+00			9.6	1921.6 ✓
T.F.			12.51	1918.67 ✓
		0.03		1918.70 ✓
+50			4.5	1914.2 ✓
+89	⁵¹ P.I.		11.7	1907.0 ✓
T.F.			12.87	1905.83 ✓
		0.07		1905.90 ✓
29+00			4.5	1901.4 ✓
T.F.			12.72	1893.18 ✓

LINE USED

12/1/48
Checked
J.M.

Cold And Windy

Jan. 18, 1928
Simpson - Inst.
Clavert - Rod

Sta.	+	H.I.	-	Elev.
				1893.18 ✓
	1.27	1894.45 ✓		
29+50			9.2	1885.2 ✓
T.F.			13.01	1881.94 ✓
	0.37	1881.81 ✓		
30+00			9.3	1872.5 ✓
T.F.			12.51	1869.30 ✓
	0.38	1869.68 ✓		
+50			11.4	1858.3 ✓
T.F.			12.56	1857.12 ✓
	6.18	1863.30 ✓		
+60	♀ creek Bed		8.4	1854.9 ✓
+85 ⁶⁶	P.I.		3.9	1859.4 ✓
31+00			4.1	1859.2 ✓

Sta.	+	H.I.	-	Elev.	5.
		1863.30 ✓			
31+30	♀ creek Bed		12.5	1850.8 ✓	
	+50		10.4	1852.9 ✓	
32+00			2.1	1861.2 ✓	
T.F.			0.18	1863.12 ✓	
	10.39	1873.51 ✓			
	+50		4.1	1869.4 ✓	
33+00			0.6	1872.9 ✓	
T.F.			0.61	1872.90 ✓	
	6.04	1878.94 ✓			
	+50		13.0	1866.9 ✓	
34+00			4.5	1874.4 ✓	
T.F.			0.98	1877.96 ✓	
	10.15	1888.11 ✓			
+27 ⁸⁰	P.I.	on 6" x 8" Boulder	4.3	1883.8 ✓	1/2/28 J.T.N.

Sta.	+	H.I.	-	Elev.
		1888.11 ✓		
34+50			3.7	1884.4 ✓
T.F.			0.60	1887.51 ✓
	10.53	1898.04 ✓		
35+00	Edge of Road		0.6	1897.4 ✓
+15	E of Road		2.2	1895.8 ✓
+50			4.6	1893.4 ✓
36+00			5.7	1892.3 ✓
T.F.			1.15	1896.89 ✓
	1.15	1898.04 ✓		
+06	¹² P.I.		5.2	1892.8 ✓
+31	16" Concrete Culvert		9.7	1888.3 ✓
+50			5.3	1892.7 ✓
T.F.			1.15	1896.89 ✓

LINE NOT USED
SEE Vol. 1
Pg 16-18 Leds.

6.

Sta.	+	H.I.	-	Elev.
		1896.89 ✓		
	10.52	1907.41 ✓		
36+85			4.1	1903.3 ✓
37+00			8.5	1898.9 ✓
+50			4.2	1903.2 ✓
+85	⁶¹ P.I.		3.1	1904.3 ✓
38+00			2.7	1904.7 ✓
T.F.			0.46	1906.95 ✓
	7.78	1914.73 ✓		
+50			8.0	1906.7 ✓
39+00			8.3	1906.4 ✓
+50			7.2	1907.5 ✓
+80	⁰² P.I.		4.8	1909.9 ✓
40+00			4.1	1910.6 ✓

2/2/28
MTR

Sta	Sta.	+	H.I.	-	Elev.
			1914.73 ✓		
34+	40+50			4.3	1910.4 ✓
T.	41+00			6.1	1908.6 ✓
	+50			8.3	1906.4 ✓
35+	42+00			9.8	1904.9 ✓
	+50			10.5	1904.2 ✓
	TF			10.17	1904.56 ✓
36+		6.52	1911.08 ✓		
	43+00			7.8	1906.3 ✓
	+41 ³⁵ P.I.			5.2	1905.9 ✓
	+50			5.1	1906.0 ✓
	TF			2.79	1910.29 ✓
		11.22	1921.51 ✓		
H	44+00			8.9	1912.6 ✓

USED L. LINE
 29.68

Sta	+	H.I.	-	Elev.
		1921.51		
44+50			4.9	1916.6 ✓
	+56 ²⁵ P.I.		5.0	1916.5 ✓
45+00			10.3	1911.2 ✓
TF			10.14	1911.37 ✓
		12.38	1923.75 ✓	
	+50		22.6	1901.2 ✓
46+00			19.2	1904.6 ✓
	+50		19.8	1909.0 ✓
47+00			11.3	1912.5 ✓
	+50		6.3	1917.5 ✓
48+00			5.7	1918.1 ✓
	+50		8.6	1915.2 ✓

Used L. Line See Page 6

Sta.	+	H.I.	-	Elev.
		1923.75 ✓		
49+00			5.6	1918.2 ✓
T.F.			6.97	1921.78 ✓
	8.08	1929.86 ✓		
+50			2.5	1927.4 ✓
+61	⁸⁰ P.O.T.		4.7	1925.2 ✓
50+00			8.1	1921.8 ✓
+50			5.9	1924.0 ✓
T.F.			5.03	1924.83 ✓
	2.21	1927.04 ✓		
51+00			8.9	1918.1 ✓
+50			13.1	1913.9 ✓
T.F.			11.99	1915.05 ✓
	0.32	1915.37 ✓		

Used L. Line

Jan. 19, 1928

Simpson-T
Clayert-Rod

Sta.	+	H.I.	-	Elev.
		1915.37 ✓		
52+00			9.2	1906.2 ✓
T.F.			12.32	1903.05 ✓
	0.87	1903.92 ✓		
+50			9.4	1894.5 ✓
T.F.			12.90	1891.02 ✓
	0.81	1891.83 ✓		
T.F.			12.43	1879.40 ✓
	0.72	1880.12 ✓		
53+00			3.6	1876.5 ✓
+40	♀ creek		37.5	1842.6 ✓
54+00			11.8	1868.3 ✓
+26	⁵³ P.O.T.		8.9	1871.2 ✓
T.F.			1.36	1878.76 ✓
	3.69	1882.45 ✓		

Used L. Line

2/2/28
H.F.R.

8.

Sta	+	H.I.	-	Elev.
		1882.45 ✓		
54+50			9.7	1872.7 ✓
55+00			5.3	1877.1 ✓
TF	11.32	1893.55 ✓	0.22	1882.23 ✓
+50			9.4	1884.2 ✓
56+00			4.7	1888.9 ✓
+50			5.3	1888.3 ✓
57+00			12.3	1881.3 ✓
TF	1.56	1883.19 ✓	11.92	1881.63 ✓
+50			8.2	1875.0 ✓
58+00			21.8	1861.4 ✓
+50			13.3	1869.9 ✓

USED LINE

Sta.	+	H.I.	-	Elev.
		1883.19 ✓		
59+00			10.3	1872.9 ✓
+50			5.9	1877.3 ✓
TF	1.89	1881.58 ✓	3.50	1879.69 ✓ ^{near} 59+80
60+00			2.6	1879.0 ✓
+50			12.3	1869.3 ✓
TF	0.52	1869.29 ✓	12.81	1868.77 ✓
TF	6.10	1862.87 ⁹⁰ ✓	12.49	1856.80 ✓ 1856.74 ✓
61+00			8.9	1854.0 ✓ 1853.9 ✓
+18			12.9	1850.0 ✓ 1849.9 ✓
+50			9.2	1853.8 ✓

USED LINE

10/28
A.T.N.

JAN. 24, 1928

Simpson - 7
Claverf. Rod

1a

Sta.	+	H.I.	-	Elev.
		1862.90 ✓ 1862.84		
62+00			7.4	1858.7 ⁵ ✓
+50			4.9	1858.0 ✓ 1857.9
T.F.			7.00	1855.84 ⁹⁰ ✓ <small>Near Sta. 62+00</small>
	0.70	1856.54 ⁶⁰ ✓		
+93	⁷⁵ P.I.		3.4	1853.7 ✓
63+00			5.8	1850.7 ⁸ ✓
T.F.			12.62	1843.72 ⁹⁸ ✓
	0.73	1844.65 ⁷¹ ✓		
+50			9.9	1834.7 ⁸ ✓
T.F.			12.46	1832.79 ²⁵ ✓
	0.16	1832.35 ⁴¹ ✓		
T.F.			12.59	1819.76 ⁸² ✓
	0.54	1820.30 ³⁶ ✓		
64+00			12.4	1808.0 ✓ 1807.9
T.F.			12.33	1808.03 ✓ 1807.97

Sta.	+	H.I.	-	Elev.
		1808.60 ✓ 1808.54		1808.03 ✓ 1807.97
64+15	€ Gully		12.7	1795.8 ⁹ ✓
T.F.			0.88	1807.1 ✓ 1807.66
	12.18	1819.84 ⁹⁰ ✓		
+50			2.2	1817.6 ⁷ ✓
T.F.			0.19	1819.65 ⁷¹ ✓
	11.36	1831.01 ⁰⁷ ✓		
65+00			3.3	1827.7 ⁸ ✓
+50			1.5	1829.5 ⁶ ✓
+95			10.9	1820.7 ² ✓
66+00			7.6	1823.4 ⁵ ✓
T.F.			0.14	1830.87 ⁹³ ✓
	12.08	1843.01 ✓ 1842.95		
+50			2.6	1840.7 ⁵ ✓
T.F.			0.09	1842.86 ⁹² ✓

2 1/2" x 1" x 1/2" x 1/2"

Sta.	+	H.I.	-	Elev.
				1842.37 1842.86
	11.35	1854. 27 ²⁷		
67+00			79	1846. 3 ⁴
T.F.	8.94	1862. 76 ⁸²	0.39	1853. 82 ⁸⁸
+50			56	1857.2
68+00			9.1	1853.7
+25	♀ Gully		16.9	1845.9
+50			12.3	1850.5
69+00			7.1	1855.7
+50			2.1	1860.7
T.F.	2.25	1863. 77 ¹⁷	1.90	1860. 86 ⁹²
70+00			4.4	1858. 7 ⁸

Sta.	+	H.I.	-	Elev.
				1863.77
70+50			6.8	1856. 3 ⁴
71+00			6.2	1857.0 1856.9
+50			4.5	1858. 6 ⁷
72+00			4.3	1858. 8 ⁹
+50			1.8	1861. 8 ⁴
T.F.	12.18	1874. 76 ⁸²	0.53	1862. 58 ⁶⁴
73+00			11.9	1862.9
+22			4.5	1870.3
+50			2.2	1872.6
T.F.	12.55	1887.05 1886.97	0.32	1874. 77 ⁵⁰
T.F.			0.48	1886. 57 ⁵⁷

Sta.	+	H.I.	-	Elev.
				1886.5 ⁷ X ✓
	12.51	1899. ⁰⁸ 02 ✓		
74+00			3.3	1895. ⁸ X ✓
T.F.			0.33	1898. ⁷⁵ 69 ✓
	12.97	1911. ⁷² 66 ✓		
+30			4.5	1907. ²⁶ 2 ✓
T.F.			0.46	1911. ²⁶ 20 ✓
	11.12	1922. ³⁸ 32 ✓		
+50			9.6	1912. ⁸ X ✓
+82			5.1	1917. ³ X ✓
75+00			6.2	1916. ² X ✓
+50			2.2	1920. ² X ✓
76+00			3.9	1918. ⁵ X ✓
76+44 ⁶⁷ " L" Line				
75+45 ⁵¹ " L" Line			4.6	1917. ⁸ X ✓

USED LINE

Sta.	+	H.I.	-	Elev.
				1922. ³⁸ 32 ✓
			0.26	1922. ¹² 06 = Check ✓
				1921.95 on S.D.B.M. ✓
				El.=1921.95 ✓
	0.71	1922.66		
77+18 ²² P.I.			4.1	1918.6 ✓
+50			4.9	1917.8 ✓
+69 ⁵⁶ P.I.			6.3	1916.4 ✓
78+00			11.2	1911.5 ✓
T.F.			12.32	1910.34 ✓
	3.34	1913.68		
+50			12.8	1900.9 ✓
79+00			17.7	1896.0 ✓
+50			15.6	1898.1 ✓
80+00			11.0	1902.7 ✓
T.F.			11.81	1901.87 ✓

USED LINE

11.81
1901.87

JAN. 26, 1928.

Simpson-Inst.
Clavert-Rod.

Warm And Windy

14

Sta.	+ H.I.	-	Elev.
	1909.31 ✓		
88+89 ⁷⁰ P.I.	12.9	1896.4 ✓	
89+00	12.4	1896.9 ✓ 1897.7 ✓	
T.F.	2.74	1906.57 ✓	
12.95	1919.52 ✓		
+50	8.5	1911.0 ✓	
+62 ⁶⁵ P.I.	7.1	1912.4 ✓	
90+00	4.2	1915.3 ✓	
+50	3.2	1916.3 ✓	
+78 ⁸⁹ P.I.	2.6	1916.9 ✓	
T.F.	2.61	1916.91 ✓	
2.49	1919.40 ✓		
91+00	4.3	1915.1 ✓	
+50	6.8	1912.6 ✓	

USED L'LINE

Sta.	+ H.I.	-	Elev.
	1919.40 ✓		
91+58 ¹⁶ P.I.	7.9	1911.5 ✓	
T.F.	12.65	1906.75 ✓	
0.72	1907.47 ✓		
92+00	4.3	1903.2 ✓	
T.F.	12.63	1894.84 ✓	
0.64	1895.48 ✓		
+50	2.0	1893.5 ✓	
T.F.	12.75	1882.73 ✓	
0.49	1883.22 ✓		
93+00	12.2	1871.0 ✓	
+10 ♀ Gully	17.2	1866.0 ✓	
T.F.	0.82	1882.40 ✓	
5.23	1887.63 ✓		
+41 ²⁶ P.I.	2.9	1884.7 ✓	

USED L'LINE

✓ 2/2/28
2/2/28

Sta.	+	H.I.	-	Elev.
		1887.63 ✓		
93+50			7.1	1883.5 ✓
94+00			4.8	1882.8 ✓
+25	E Gully		17.2	1870.4 ✓
+50			4.9	1882.7 ✓
T.F.			0.19	1887.44 ✓
		12.35 1899.79 ✓		
+83	⁹⁶ P.I.		5.1	1894.7 ✓
95+00			0.0	1899.8 ✓
T.F.			0.01	1899.78 ✓
		11.81 1911.59 ✓		
+25			4.0	1907.6 ✓
+52	²³ P.I.		2.4	1909.2 ✓
T.F.			0.67	1910.92 ✓

USED LINE

Sta.	+	H.I.	-	Elev.
		1910.92 ✓		
		10.20 1921.12 ✓		
96+00			8.0	1913.1 ✓
+38	³⁶ P.I.		4.9	1916.2 ✓
+50			5.1	1916.0 ✓
97+00			5.2	1915.9 ✓
122 ⁰⁰	P.I.		6.0	1915.1 ✓
+50			8.6	1912.5 ✓
T.F.			8.50	1912.62 ✓
		0.48 1913.10 ✓		
+86	¹⁰ P.I.		3.0	1910.1 ✓
98+00			4.3	1908.8 ✓
+50			5.8	1907.3 ✓
+97	³³ P.I.		4.8	1908.3 ✓

USED LINE

✓ 1/28
J.T.

Sta.	+	H.I.	-	Elev.
		1913.10 ✓		
99+50			4.7	1908.4 ✓
100+00			5.2	1907.9 ✓
+22	¹⁰ P.I.		3.9	1909.2 ✓
TF			5.22	1907.88 ✓
		6.14 1914.02 ✓		
+50			8.9	1905.1 ✓
+74	⁴² P.I.		8.9	1905.6 ✓
101+00			6.6	1907.4 ✓
+50			1.4	1912.6 ✓
TF			1.19	1912.83 ✓
		8.43 1921.26 ✓		
+77	⁵⁹ P.I.		7.4	1913.9 ✓
102+00			6.2	1915.1 ✓

USED LINE

Sta.	+	H.I.	-	Elev.
		1921.26 ✓		
102+50			7.6	1913.7 ✓
			7.1° P.I.	6.3 1915.0 ✓
103+00			7.9	1913.4 ✓
+50			7.9	1913.4 ✓
104+00			10.5	1910.8 ✓
+50			14.3	1907.0 ✓
105+00			12.2	1909.1 ✓
+50			8.3	1913.0 ✓
TF			6.71	1914.55 = check on
				1914.65 S.D.E.M.
				EI = 1914.65
		9.79 1924.44 ✓		
+90	⁸⁷ P.I.		10.1	1914.3 ✓
106+00			10.5	1913.9 ✓

USED LINE

Sta	+	H.I.	-	Elev.
		1924.44 ✓		
106+50			17.0	1907.4 ✓
107+00			14.9	1909.5 ✓
+50			11.7	1912.7 ✓
108+00			10.9	1913.5 ✓
TF			12.35	1912.09 ✓
	0.97	1913.06 ✓		
✓ +41 ⁷⁵ P.I.			0.5	1912.6 ✓
+50			3.1	1910.0 ✓
TF			12.78	1900.28 ✓
	0.13	1900.41 ✓		
109+00			3.5	1896.9 ✓
TF			13.02	1887.39 ✓
	0.24	1887.63 ✓		

USED LINE

Sta	+	H.I.	-	Elev.
		1887.63 ✓		
109+50			8.0	1879.6 ✓
TF			12.64	1874.99 ✓
	0.37	1875.36 ✓		
+80			11.9	1863.5 ✓
110+00			7.8	1867.6 ✓
+30			5.0	1870.4 ✓
+50			6.9	1868.5 ✓
TF			12.93	1862.43 ✓
	0.59	1863.02 ✓		
111+00			5.7	1857.3 ✓
TF			12.55	1850.47 ✓
	0.72	1851.19 ✓		
+50			12.5	1838.7 ✓
TF			12.53	1838.66 ✓

2/1/28
J.H.L.

Sta.	+	H.I.	-	Elev.
				1838.66 ✓
	0.30	1838.96 ✓		
TF			12.93	1826.03 ✓
	0.39	1826.42 ✓		
112+00			4.9	1821.5 ✓
TF			12.99	1813.43 ✓
	0.27	1813.70 ✓		
+50			10.4	1803.3 ✓
TF			12.59	1801.11 ✓
	0.53	1801.64 ✓		
TF			12.64	1789.00 ✓
	0.05	1789.05 ✓		
113+00			12.3	1776.7 ✓
+20	φ creek		19.2	1769.8 ✓
+50			14.4	1774.6 ✓
114+00			6.7	1782.3 ✓

Sta.	+	H.I.	-	Elev.
				1789.05 ✓
114+50			1.7	1787.3 ✓
TF			1.34	1787.71 ✓
	12.48	1800.19 ✓		
115+00			8.6	1791.6 ✓
+50			3.5	1796.7 ✓
116+00			1.9	1798.3 ✓
TF			0.80	1799.39 ✓
	12.75	1812.14 ✓		
+50			11.1	1801.0 ✓
+78			8.8	1803.3 ✓
TF			0.02	1812.12 ✓
	11.70	1823.82 ✓		
117+00			11.1	1812.7 ✓
TF			0.43	1823.39 ✓

18
 ✓ 2/28
 2977 measurement

Sta	+	H.I.	-	Elev.
	13.04	1836.43		1823.39 ✓
117+50			3.6	1832.8 ✓
TF	11.57	1847.79	0.23	1836.20 ✓
TF	12.51	1860.22	0.08	1847.71 ✓
118+00			11.4	1848.8 ✓
TF	12.41	1872.49	0.17	1860.08 ✓
+50			3.2	1869.3 ✓
TF	12.75	1885.13	0.11	1872.38 ✓
TF	12.56	1897.61	0.08	1885.05 ✓
119+00			5.5	1892.1 ✓

Sta	+	H.I.	-	Elev.
		1897.61 ✓		
TF	12.95	1910.21	0.35	1897.26 ✓
119+50			0.5	1909.7 ✓
TF	4.49	1914.36	0.34	1909.87 ✓
+86 ⁶⁰ P.I.			4.1	1910.3 ✓
*120+00			4.8	1909.6 ✓
+50			7.9	1907.0 ✓
121+00			12.3	1902.1 ✓
+50			9.2	1905.2 ✓
+72 ⁵⁶ P.I.			8.4	1906.0 ✓
122+00			11.1	1903.3 ✓
TF	12.47	1901.89		✓

4/26/28
J.H.

Jan. 27, 1928

Simpson - Inst.
Clavert - Rod.

Cloudy And Windy

20.

Sta.	+	H.I.	-	Elev.
	1.01	1902.90		1901.89 ✓
122+50			9.5	1893.4 ✓
T.F.			11.82	1891.08 ✓ <small>T.P. on Rock</small>
	0.64	1891.72		<small>near 122+60</small>
T.F.			12.34	1879.38 ✓
	5.40	1884.78		
123+00			6.4	1878.4 ✓
+50			6.9	1877.9 ✓
124+00			4.4	1880.4 ✓
+50			5.3	1879.5 ✓
T.F.			12.12	1872.66 ✓
	3.15	1875.81		
125+00	£ Gully		15.9	1859.9 ✓
+25	¹³ P.I.		5.4	1870.4 ✓

Sta.	+	H.I.	-	Elev.
		1875.81		
125+50			5.2	1870.6 ✓
126+00			8.1	1867.7 ✓
T.F.			7.22	1868.59 ✓
	5.93	1874.52		
+20	⁵² P.I.		6.0	1868.5 ✓
+50			7.6	1866.9 ✓
127+00			8.4	1866.1 ✓
+50			5.0	1869.5 ✓
128+00			7.0	1867.5 ✓
+50			5.5	1869.0 ✓ 1819.0
129+00			5.8	1868.7 ✓
T.F.			0.13	1874.39 ✓

✓ 1-1/2
T.F.

Sta.	+	H.I.	-	Elev.
				1874.39 ✓
	11.48	1885.87 ✓		
129+50			8.7	1877.2 ✓
T.F.			0.64	1885.23 ✓
	11.89	1897.12 ✓		
130+00			9.3	1887.8 ✓
+41	³⁵ P.I.		6.0	1891.1 ✓
+50			5.2	1891.9 ✓
131+00			4.5	1892.6 ✓
T.F.			7.44	1889.68 ✓
	12.16	1901.84 ✓		
+51	" P.I.		9.3	1892.5 ✓
132+00			5.5	1896.3 ✓
+50	φ Gully		11.4	1890.4 ✓

Sta.	+	H.I.	-	Elev.
				1901.84 ✓
133+00			3.7	1898.1 ✓
T.F.			0.26	1901.58 ✓
	9.74	1911.32 ✓		
+50			5.1	1906.2 ✓
+80			2.6	1908.7 ✓
134+00			6.8	1904.5 ✓
T.F.			12.90	1898.42 ✓
	1.01	1899.43 ✓		
+50			3.7	1895.7 ✓
T.F.			12.54	1886.89 ✓
	0.73	1887.62 ✓		
135+00			11.9	1875.7 ✓
T.F.			12.49	1875.13 ✓

1/2
27/2

Sta.	+	H.I.	-	Elev.
	2.98	1878.11		1875.13 ✓
135+25			18.4	1859.7 ✓
+50			10.7	1867.4 ✓
T.F.	0.63	1865.94	12.80	1865.31 ✓
136+00			12.1	1853.8 ✓
+18	♀ Gully		20.0	1845.9 ✓
T.F.	12.26	1877.81	0.39	1865.55 ✓
+50			11.6	1866.2 ✓
+78			0.5	1877.3 ✓
T.F.	12.28	1889.62	0.47	1877.34 ✓
137+00			10.5	1879.1 ✓

Sta	+	H.I.	-	Elev.
		1889.62		
137+50			4.0	1885.6 ✓
T.F.	12.92	1902.07	0.47	1889.15 ✓
138+00			5.4	1896.7 ✓
+10 ⁰⁵ P.I.			4.4	1897.7 ✓
+58 ⁰⁷ End of L-Line			8.9	1893.2 ✓
T.F.	13.11	1914.57	0.61	1901.46 ✓
T.F.	12.88	1926.95	0.50	1914.07 ✓
T.F.	12.00	1938.42	0.53	1926.42 ✓
T.F.			2.26	1936.16 = check

22

on S.P.B.M.
#16

Elev. = 1936.10

Related to above
 2/3/28 m 12.00
 12.00
 12.00
 12.00
 ✓ 2/2/28
 J.P.N.

Sutherland San Vicente Conduit Simpson
Covert.

23.

1-31-28

Profile Levels over Last 100 ft
of L Line Near North Portal
of Tunnel #2. These are run with
Hand Level.

Sta	+ H.I.	-	Elev.
			138+10.05 = P.I.
	3.20 ✓	1900.90 ✓	1897.7 ✓
138+50		7.1 ✓	1893.8 ✓
+85		2.7 ✓	1896.2 ✓
T.P.	12.80 ✓	1913.10 ✓	0.60 ✓ 1900.30 ✓
139+00		7.8 ✓	1905.3 ✓
T.P.	7.50 ✓	1920.60 ✓	0.00 ✓ 1913.10 ✓
139+26.45 = Int of		4.7 ✓	1915.9 ✓

Line to Tunnel Line

2/29/28

Note: Copied from Single Loose
Leaf So as to have Notes together

STN.

Jan. 25, 1928

Simpson - Inst.

Clavert - Rod

Profile Levels, over L" Line
starting from P.I. Sta. 43+41⁵⁵
L Line And continuing
along old pipe Grade.

USED
L LINE

L''

Sta.	+	H.I.	-	Elev.
		1916.22		= El. S.D.B.M.
	0.42	1916.64		
43+41 ⁵⁵	P.I.		10.4	1906.2 ✓
+50			11.3	1905.3 ✓
44+00			10.0	1906.6 ✓
+29 ⁶⁹	P.I.		7.5	1909.1 ✓
+50			4.9	1911.7 ✓
+77°	P.I.		4.1	1912.5 ✓
45+00			5.0	1911.6 ✓
+50			6.1	1910.5 ✓
+99°	P.I.		1.5	1915.1 ✓
46+00			1.1	1915.5 ✓
T.F.			0.28	1916.36 ✓

USED LINE

Sta.	+	H.I.	-	Elev.
		1916.36		
	12.78	1929.14		
46+50			7.0	1922.1 ✓
+72 ¹⁸	P.I.		4.9	1924.7 ✓
47+00			3.7	1925.4 ✓
+50			3.5	1925.6 ✓
+90 ²⁹	P.I.		1.9	1927.7 ✓
T.F.			1.08	1928.06 ✓
	2.55	1930.61		
48+50			4.1	1926.5 ✓
+84 ⁸⁸	P.I.		4.9	1926.2 ✓
49+00			4.7	1925.9 ✓
+50			5.0	1925.6 ✓
+58 ¹³	P.I.		5.0	1925.6 ✓

USED LINE

1/2/66
J.T.W.

Sta	+	H.I.	-	Elev.
		1930.61		
50+00			6.1	1924.5
+50			5.8	1924.8
T.F.			6.25	1924.36
	6.27	1930.63		
+86 ¹ / ₂ P.I.			6.1	1924.5
51+00			5.9	1924.7
+50			4.6	1926.0
52+00			4.3	1926.3
+21 ⁸⁰ / ₁₀₀ P.I.			4.8	1925.8
T.F.			4.58	1926.05
	2.83	1928.88		
+50			2.8	1926.1
53+00			5.8	1923.1

USED L.L.H.S.

Sta	+	H.I.	-	Elev.
		1928.88		
T.F.			12.43	1916.45
	4.28	1917.73		
53+30			6.2	1911.5
+70 ⁵⁹ / ₁₀₀ P.I.			13.2	1904.5
T.F.			12.93	1904.80
	4.84	1909.64		
54+00	⊕ Gully		20.1	1889.5
+30			2.6	1907.0
+50			0.2	1909.4
T.F.			0.07	1909.57
	12.00	1921.57		
55+00			6.8	1914.8
T.F.			0.27	1921.30
	8.04	1929.34		
+42 ¹² / ₁₀₀ P.I.			8.0	1921.3

USED L.L.H.S.

✓ 1/2/28
K.T.N.

Sta.	+	H.I.	-	Elev.
		1929.34 ✓		
55+50			7.1	1922.2 ✓
56+00			4.8	1924.5 ✓
+50			5.5	1923.8 ✓
495 ¹⁵ P.I.			6.0	1923.3 ✓
T.P.			6.02	1923.32 ✓
	0.61	1923.93		
57+50			2.7	1921.2 ✓
58+00			6.7	1917.2 ✓
+35 ⁷³ P.I.			11.2	1912.7 ✓
+50			11.7	1912.2 ✓
T.P.			12.19	1911.74 ✓
	5.40	1917.14 ✓		
+84 ⁶⁹ P.I.			7.0	1910.1 ✓

USED LINE

Sta.	+	H.I.	-	Elev.
		1917.14 ✓		
59+00			8.0	1909.1 ✓
+50			0.2	1916.9 ✓
T.P.			0.7	1916.97 ✓
	10.98	1927.95 ✓		
60+00			6.7	1921.3 ✓
+28 ⁹⁷ P.I.			5.0	1923.0 ✓
+50			4.8	1923.2 ✓
+81 ⁵³ P.I.			5.0	1923.0 ✓
T.P.			4.53	1923.42 ✓
	1.30	1924.72 ✓		
61+00			2.1	1922.6 ✓
+50			4.7	1920.0 ✓
+71 ³⁷ P.I.			4.9	1919.8 ✓
62+00			3.3	1921.4 ✓

USED LINE

✓ 2/28
1922

Sta.	+	H.I.	-	Elev.
		1924.72		
62+50			1.2	1923.5 ✓
+99 ⁸⁸ P.I.			0.1	1924.6 ✓
T.F.			0.07	1924.65 ✓
	2.25	1926.90 ✓		
63+50			3.5	1923.4 ✓
64+00			6.0	1920.9 ✓
+04 ⁶⁷ P.I.			6.4	1920.5 ✓
T.F.			12.77	1914.13 ✓
	2.21	1916.34 ✓		
+50			3.3	1913.0 ✓
65+00			4.7	1911.6 ✓
+50			11.6	1904.7 ✓
+55 ⁹ P.I.			12.1	1904.2 ✓

USED LINE

Sta.	+	H.I.	-	Elev.
		1916.34 ✓		
65+65			16.3	1900.0 ✓
66+00			5.5	1910.8 ✓
T.F.			6.84	1909.50 ✓
	11.82	1921.32 ✓		
+50			1.4	1919.9 ✓
+71 ⁸² P.I.			0.3	1921.0 ✓
T.F.			0.33	1920.99 ✓
	4.21	1925.20 ✓		
67+00			4.5	1920.7 ✓
+50			7.0	1918.2 ✓
+68 ⁶² P.I.			7.1	1918.1 ✓
68+00			7.7	1920.5 ✓
+41 ⁹⁹ P.I.			4.4	1920.8 ✓

USED LINE

✓ 2/25
JRM

Sta.	+	H.I.	-	Elev.
		1925.20 [✓]		
68+50			5.0	1920.2 [✓]
69+00			4.1	1921.1 [✓]
+50			3.5	1921.7 [✓]
70+00			4.4	1920.8 [✓]
+16 ⁶⁶ P.I.			6.0	1919.2 [✓]
T.F.			5.89	1919.36 [✓]
	1.26	1920.62		
+50			2.0	1918.6 [✓]
71+00			3.7	1916.9 [✓]
+50			7.9	1912.7 [✓]
72+00			18.9	1901.7 [✓]
+20 ♀ Gully			27.2	1893.4 [✓]

Sta.	+	H.I.	-	Elev.
		1920.62 [✓]		
72+50			9.9	1910.7 [✓]
73+00			4.0	1916.6 [✓]
+50			1.3	1919.3 [✓]
T.F.			1.31	1919.31 [✓]
	3.26	1922.57		
74+00			1.5	1921.1 [✓]
+05 ⁹³ P.I.			1.7	1920.9 [✓]
+50			3.1	1919.5 [✓]
75+00			5.7	1916.9 [✓]
+50			12.6	1910.0 [✓]
T.F.			12.83	1909.74 [✓]
	0.93	1910.67		
76+00			6.7	1904.0 [✓]

2/2/28
JST

Sta.	+	H.I.	-	Elev.
		1910.67 [✓]		
76+50			11.4	1899.3 [✓]
77+00			9.1	1901.6 [✓]
+90			16.1	1894.6 [✓]
+50			11.0	1899.7 [✓]
T.F.			0.31	1910.36 [✓]
	11.93	1922.29 [✓]		
78+00			6.8	1915.5 [✓]
+50			2.0	1920.3 [✓]
+72 ²¹	P.I.		1.9	1920.4 [✓]
T.F.			2.71	1919.58 [✓]
	3.40	1922.98 [✓]		
79+50			5.0	1918.0 [✓]
+83 ¹³	End of 1 st Line		5.9	1917.6 [✓]
T.F.			0.90	1922.08 [✓]

USED L LINE

✓ 2/2/28
J.M.

= CHECK ON S.D.B.M. - E.I. = 1921.95

Jan 23, 1928

Simpson

Clavert.

Profile Levels over "L" Line
Starting from P.O.T. 43+60⁷² "L"
Line and P.I. on "L" Line

2+10.75

Sta.	+	H.I.	-	Elev.
				1924.36 = S.D.B.M.
	5.91	1930.33 ✓		
T.F.			3.05	1927.28 ✓
	4.61	1931.89 ✓		
T.F.			6.39	1925.50 ✓
	0.70	1926.20 ✓		
T.F.			1.04	1925.16 ✓
	4.45	1929.61 ✓		
43+10 ⁷⁰			23.1	1906.5 ✓
				Pt. on L Line Pt. " L "
+50			8.9	1920.7 ✓
44+00			4.8	1924.8 ✓
+20			7.2	1925.4 ✓
+50			6.6	1923.0 ✓
T.F.			12.93	1916.68 ✓
	1.40	1918.08 ✓		
45+00			5.1	1913.0 ✓
+13			7.8	1910.3 ✓
				old Pipe Grade

Sta.	+	H.I.	-	Elev.
				1918.08 ✓
T.F.			12.62	1905.46 ✓
	0.58	1906.04 ✓		
45+50			3.8	1902.2 ✓
46+00			3.8	1902.2 ✓
+50			5.8	1900.2 ✓
47+00			10.5	1895.5 ✓
T.F.			12.24	1893.80 ✓
	1.20	1895.00 ✓		
+50			2.2	1892.8 ✓
48+00			7.8	1887.2 ✓
T.F.			12.87	1882.13 ✓
	1.93	1884.06 ✓		
+50			7.0	1877.1 ✓
49+00			3.1	1881.0 ✓

68.

✓ 1/2/28
J.T.M.

Sta.	+	H.I.	-	Elev.
		1884.06 ✓		
49+50			6.1	1878.0 ✓
T.F.			12.70	1871.36 ✓
	1.37	1872.73		
50+00			10.3	1862.4 ✓
+50			11.1	1861.6 ✓
T.F.			13.04	1859.69 ✓
	0.43	1860.12		
51+00			12.0	1848.1 ✓
T.F.			12.96	1847.16 ✓
	0.49	1847.65		
+50			10.8	1836.8 ✓
T.F.			12.64	1835.01 ✓
	0.97	1835.98		
52+00			4.3	1831.7 ✓

69.

Sta.	+	H.I.	-	Elev.
		1835.98		
52+50			6.2	1829.8 ✓
T.F.			12.22	1823.76 ✓
	0.82	1824.58		
53+00			2.1	1822.5 ✓
T.F.			12.92	1811.66 ✓
	0.68	1812.34		
+50			1.5	1810.8 ✓
T.F.			12.69	1799.65 ✓
	1.66	1801.31		
T.F.			12.31	1788.94 ✓
	5.17	1794.11		
54+07			16.4	1777.7 ✓
				\$ Gully
T.F.			0.63	1793.48 ✓
	11.61	1805.09		
+50			8.2	1796.9 ✓

1/2/28
X172

Sta.	+	H.I.	-	Elev.
		1805.09 ✓		
55+00			1.5	1803.6 ✓
T.F.			1.46	1803.63 ✓
	6.39	1810.02 ✓		
+50			5.2	1804.8 ✓
56+00			9.3	1800.7 ✓
T.F.			12.96	1797.06 ✓
	0.83	1797.89 ✓		
+50			5.8	1792.1 ✓
T.F.			12.67	1785.22 ✓
	0.48	1785.70 ✓		
57+00			2.7	1783.0 ✓
+50			11.3	1774.4 ✓
T.F.			12.19	1773.51 ✓
	0.55	1774.06 ✓		

Sta.	+	H.I.	-	Elev.
		1774.06 ✓		
58+00			11.5	1762.6 ✓
T.F.			12.55	1761.51 ✓
	0.99	1762.50 ✓		
+50			3.2	1759.3 ✓
59+00			7.2	1755.3 ✓
T.F.			12.37	1750.13 ✓
	1.60	1751.73 ✓		
+30			1.6	1750.1 ✓
+50			11.9	1739.8 ✓
+60			21.3	1730.4 ✓
+79			11.6	1740.1 ✓
60+00			7.9	1743.8 ✓
T.F.			5.83	1745.90 ✓

70.

1/2/2/2/8
21.72

Jan. 24, 1928
Cold.

Simpson - K
Clavert. - Red

71.

Sta.	+	H.I.	-	Elev.
				1745.90 ✓
	4.90	1750.80 ✓		
60+50			3.7	1747.1 ✓
61+00			4.6	1746.2 ✓
+50			7.9	1742.9 ✓
T.F.			12.08	1738.72 ✓
	0.20	1738.92 ✓		
62+00.			3.8	1735.1 ✓
+18 ⁰⁶ P.I.			5.6	1733.3 ✓
T.F.			2.38	1736.54 ✓
	7.37	1743.91 ✓		
+50			5.6	1738.3 ✓
63+00			4.2	1739.7 ✓
T.F.			12.74	1731.17 ✓

Sta.	+	H.I.	-	Elev.
				1731.17 ✓
	6.83	1738.00 ✓		
63+45 & Gully			14.3	1723.7 ✓
+53 ⁶⁵ P.I.			10.6	1727.4 ✓
T.F.			0.14	1737.86 ✓
	12.39	1750.25 ✓		
64+00			11.5	1738.7 ✓
+50			3.6	1746.6 ✓
T.F.			0.74	1749.51 ✓
	13.10	1762.61 ✓		
65+00			2.6	1760.0 ✓
T.F.			0.13	1762.48 ✓
	12.21	1774.69 ✓		
+50			5.2	1769.5 ✓
T.F.			0.10	1774.59 ✓

1/27/28
27.20

Sta.	+	H.I.	-	Elev.
				1774.59 ✓
	8.03	1782.62 ✓		
66+00			6.7	1775.9 ✓
+50			5.0	1777.6 ✓
67+18			26.5	1756.1 ✓
67+50			10.0	1772.6 ✓
68+00			6.0	1776.6 ✓
T.F.			1.12	1781.50 ✓
	7.87	1789.37 ✓		
+50			6.5	1782.9 ✓
69+00			5.1	1784.3 ✓
+50			6.2	1783.2 ✓
70+00			5.0	1784.4 ✓
T.F.			0.83	1788.54 ✓

Sta.	+	H.I.	-	Elev.
				1788.54 ✓
	11.31	1799.85 ✓		
70+50			12.1	1787.7 ✓
71+00			3.6	1796.2 ✓
T.F.			0.20	1799.65 ✓
	12.68	1812.33 ✓		
T.F.			0.39	1811.94 ✓
	12.14	1824.08 ✓		
T.F.			0.71	1823.37 ✓
	12.30	1835.67 ✓		
+50			9.8	1825.9 ✓
T.F.			0.27	1835.40 ✓
	12.21	1847.61 ✓		
T.F.			0.51	1847.10 ✓
	11.78	1858.88 ✓		
72+00			5.9	1853.5 ✓
T.F.			0.03	1858.85 ✓

✓ 12/2/28
J.T.N.

Sotherland Sam Steents
PROFILE LEVELS over L'

Conduit
LINE.

73.

Sta.	+	H.I.	-	Elev.
				1858.85 ✓
	11.67	1870.52 ✓		
T.F.			0.11	1870.41 ✓
	13.00	1883.41 ✓		
72+50			3.2	1880.2 ✓
T.F.			0.11	1883.30 ✓
	12.17	1895.47 ✓		
T.F.			0.35	1895.12 ✓
	10.02	1905.14 ✓		
73+00			7.0	1898.1 ✓
T.F.			0.05	1905.09 ✓
	11.34	1916.43 ✓		
+20			7.7	1908.7 ✓
+50			7.0	1909.4 ✓
74+00			8.9	1907.5 ✓
+50			6.5	1909.9 ✓

Sta.	+	H.I.	-	Elev.	Notes
		1916.43 ✓			
75+00			2.9	1914.0 ✓	
T.F.			0.82	1915.61 ✓	
	7.27	1922.88 ✓			
+45 ⁵²			5.2	1917.7 ✓	End of L' Line
T.P.			0.70	1922.18 ✓	Highest Point on
				1921.95	Large Boulder
75+45.5			6.2	1917.5 ✓	at Edge of
76+19.12			5.1	1918.6 ✓	old Pipe
+50			6.0	1917.7 ✓	Grade
+90			10.1	1913.6 ✓	
T.P.	0.66	1911.73 ✓	12.65	1911.07 ✓	1-30-28
77+00			3.4	1908.3 ✓	Simpson
T.P.	0.19	1899.57 ✓	12.35	1899.38 ✓	Clavert
+50			10.0	1889.6 ✓	Cloudy War
T.P.	0.38	1887.21 ✓	12.74	1886.83 ✓	
T.P.	0.21	1874.75 ✓	12.67	1874.54 ✓	
78+00			7.0	1867.8 ✓	
T.P.	0.79	1862.77 ✓	12.77	1861.98 ✓	checked 5/28 J.F.N.
+20 & Gully			5.9	1856.9 ✓	

1/29/28 checked Copying
 Copied these notes from Loose Leaf to get
 Notes all together J.F.N.
 S.D.B.M. 1.77 ✓ 1923.72 ✓

Highest Point on
 Large Boulder
 at Edge of
 old Pipe
 Grade
 1-30-28
 Simpson
 Clavert
 Cloudy War

Sutherland San Vicente
Profile Levels over

Conduit
L' Line.

79

		1862.77		
78+50		4.4	1858.4	
T.P.	0.48	1850.77	12.48	1850.29
79		1.4	1849.4	
T.P.	0.99	1838.76	13.00	1837.77
+50		4.3	1834.5	
T.P.	0.45	1827.24	11.97	1826.79
80+00		9.8	1817.4	
T.P.	0.94	1815.32	12.86	1814.38
80+25 H. edge of Road		6.5	1808.8	
+50 S " " "		5.6	1809.7	
T.P.	2.89	1805.53	12.68	1802.64
T.P.	1.97	1794.55	12.95	1792.58
81+00		5.4	1789.2	
T.P.	0.31	1782.47	12.39	1782.16
T.P.	0.09	1769.83	12.73	1769.74
T.P.	0.49	1757.52	12.80	1757.03
+50		1.5	1756.0	
+75		9.6	1747.9	
82+00		6.4	1751.1	
+50		17.2	1740.3	
+68		23.8	1733.7	
83+00		15.9	1741.6	
+25		13.2	1744.3	
T.P.	0.67	1745.25	12.94	1744.58
+50		6.5	1738.7	

		1745.25		
T.P.	0.78	1733.10	12.93	1732.32
84+00			10.9	1722.2
T.P.	1.22	1721.65	12.67	1720.43
T.P.	1.10	1710.53	12.22	1709.43
+50			2.8	1707.7
T.P.	1.88	1699.70	12.71	1697.82
85+00			3.0	1696.7
+50			13.2	1686.5
T.P.	0.18	1686.89	12.99	1686.71
86+00			10.0	1676.9
T.P.	1.15	1675.49	12.55	1674.34
+25			9.5	1666.0
+50			5.8	1669.7
87+00			9.2	1666.3
T.P.	0.54	1663.13	12.90	1662.59
+50			5.0	1658.1
+60			9.0	1654.1
88+00	± Gully		35.8	1627.3
+50			12.5	1650.6
+65			9.9	1653.2
T.P.	1.59	1652.23	12.49	1650.64
89+00			9.9	1642.3
+25	± Gully Running Water		28.8	1623.4
T.P.	11.00	1658.75	4.48	1647.75
+50			17.9	1640.8

Sutherland Pass
Profile Levels

		1658.75		
89+60			9.7	1649.0
T.P.	10.93	1668.96	0.72	1658.03
90+00			7.9	1661.1
T.P.	11.76	1680.29	0.43	1668.53
+50			9.3	1671.0
T.P.	12.28	1692.24	0.33	1679.96
91+00			12.2	1680.0
+50			4.0	1688.2
T.P.	12.61	1703.94	0.91	1691.33
92+00			6.5	1697.4
T.P.	12.30	1715.22	1.02	1702.92
92+50			7.7	1707.5
93+00			1.0	1714.2
T.P.	12.73	1727.94	0.01	1715.21
+50			3.3	1724.6
T.P.	12.74	1740.27	0.41	1727.53
94+00			5.9	1734.4
T.P.	12.17	1752.14	0.30	1739.97
+50			10.6	1741.5
+65			11.8	1740.3
T.P.	12.90	1764.85	0.19	1751.95
95			10.0	1754.8
T.P.	12.71	1777.37	0.19	1764.66
+50			8.1	1769.3
T.P.	12.8A	1789.74	0.47	1776.90

Yicente Conduit
over L' Line.

75

				1789.74
96+00			1.2	1788.5
T.P.	12.53	1801.87	0.40	1789.34
T.P.	12.57	1814.44	0.00	1801.87
+50			10.5	1803.9
T.P.	13.11	1827.20	0.35	1814.09
97+00			5.4	1821.8
+25			2.5	1824.7
T.P.	12.70	1839.78	0.12	1827.08
+50			4.3	1835.5
T.P.	12.82	1852.22	0.31	1839.47
T.P.	12.75	1864.89	0.15	1852.14
98+00			9.7	1855.2
T.P.	12.94	1877.72	0.11	1864.78
+50			8.2	1869.5
T.P.	12.93	1890.32	0.33	1877.39
99+00			5.0	1885.3
T.P.	12.47	1902.67	0.12	1890.20
+50			4.9	1897.8
T.P.	13.10	1915.62	0.15	1902.57
100+00			7.0	1908.6
+10.48	PI Int to L Line.		4.9	1910.7
+50			0.4	1915.2
100+84.14	L Line = 108+41.75 L Line		3.2	1912.4
T.P.	13.01	1928.01	0.62	1915.00
T.P.	7.37	1935.14	0.24	1927.77
T.P. (BM)			4.29	1930.85
				1930.98

50 AM 1/2
Point on Road 1930.98
of Old Sta 108+75
108+75

Check on
5+ BM #

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in

left column and top row. The number in body

of table in same row and column gives distance level estimate the difference in elevation between

the side stake and slope stake by this amount if cut, elevate it fill. Add this amount

to cut or fill and distance from side stake to cut rod at the slope stake. If it does not make the slight adjustment

necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

1930.98
+ 3.55

1934.53
- 11.14

1923.39
+ 1.35

1924.74
- 10.09

1914.65

2629
315
52999.4 W
19070
1769.8
137.2 2926
 315