

W
479

MICROFILMED
JAN 13 1965

479

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Tunnel, Inner Lining Points.

Profile of Invert R.C. Concrete	
Sta 1+31-3+50	1-2
" 3+60-7+00	14-16
Measured Sections inside R.C. Concrete	
Sta 1+31, 1+50, 2, 2+50, 3	3-5
" 4+17.6, 4+23.6, 3+50, 4, 4+25.59, 4+50, 5, 5+50, 6, 6+50, 7	8-13
Spring Line Points 1+31-7+00	6-7
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Revision Pipe Line loc. in Route 8	52-54
Tie to Alternate line of 1931	
Pipe line survey at sta. 111+97.52	55
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Profile of Concrete invert on 2
and at edges. (Diversion Tunnel)

Nov. 28-1934

Simpson

Sober

Isbell

Remmen

B.M. 6.45 563.67 557.22 Lead

Plug on 2, Sta. 3+00

1+31 2 (Wend of Plug) 3.71 559.96

" N. edge invert 1.59

" S. " " 1.59

1+40 2 Filled about 6' with concrete

Very Hard

1+50 2 4.01 559.66

" N. edge invert 1.93

" S. " " 1.91

1+60 2 4.11

+70 2 4.27

+80 2 4.52

+90 2 4.63

2+00 2 4.71 558.96

" N. edge invert 2.72 560.96

" S. " " 2.67

2+10 2 4.72

+20 2 4.93

+30 2 5.16

+40 2 5.37

Profile of Concrete invert on ϕ
and at edges. contd.

Nov. 28-1934

2.

563.67

2+50	ϕ	5.62	558.05
"	N. edge invert	3.58	
"	S. " "	3.50	
2+60	ϕ	5.81	
+70	ϕ	5.99	
+80	ϕ	6.17	
+90	ϕ	6.33	
3+00	ϕ	6.45	557.22
"	N. edge invert	4.38	
"	S. " "	4.25	

Dec. 12-1934

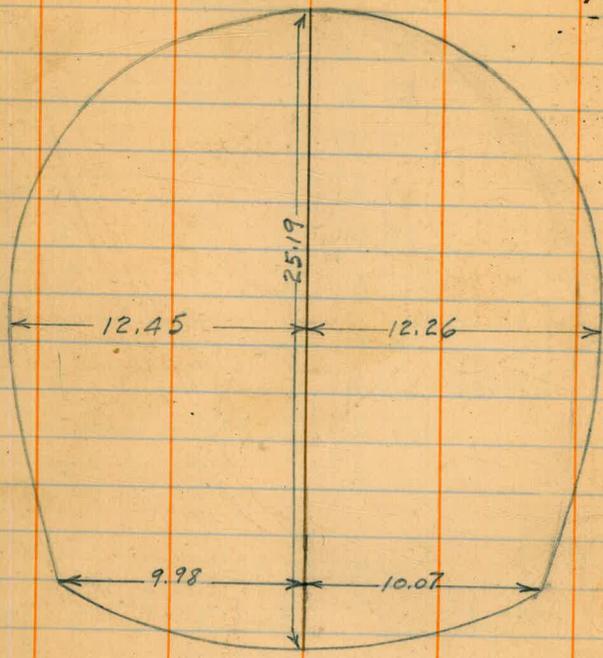
B.M. 4.24 561.47 557.23

3+10	ϕ	4.51	
+20	ϕ	4.73	
+30	ϕ	4.85	
+40	ϕ	4.88	
+50	ϕ	4.92	
"	N. edge invert	2.96	
"	S. " "	3.00	

Continued on Page 14.

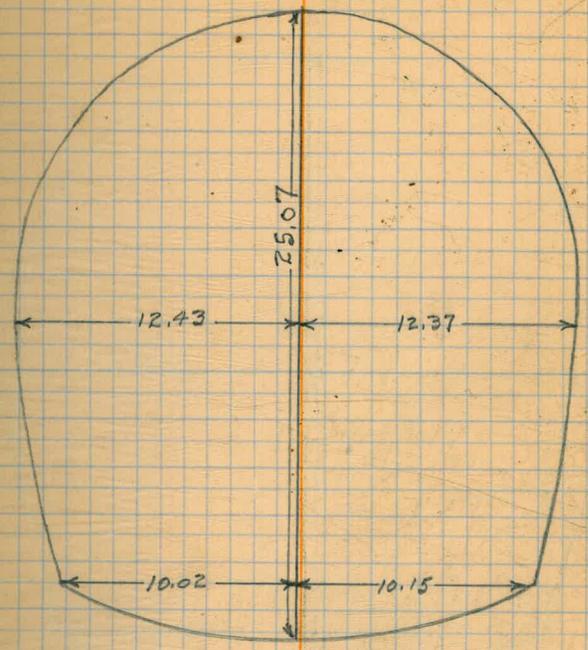
Measurements of Finished Concrete
Lines in Diversion Tunnel

Nov. 28-1934
Simpson
Soper
Isbell
Remmen



⊕

Sta. 1+31



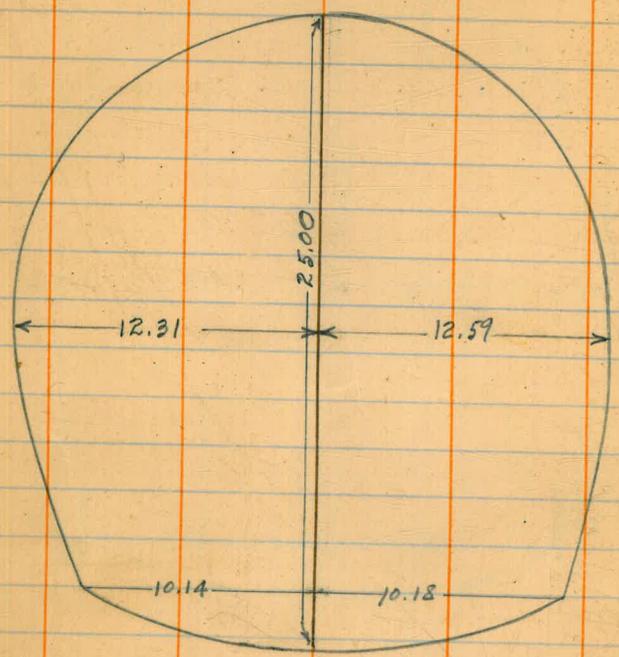
⊕

Sta. 1+50

Measurements of Finished Concrete
Lines in Diversion Tunnel Contd.

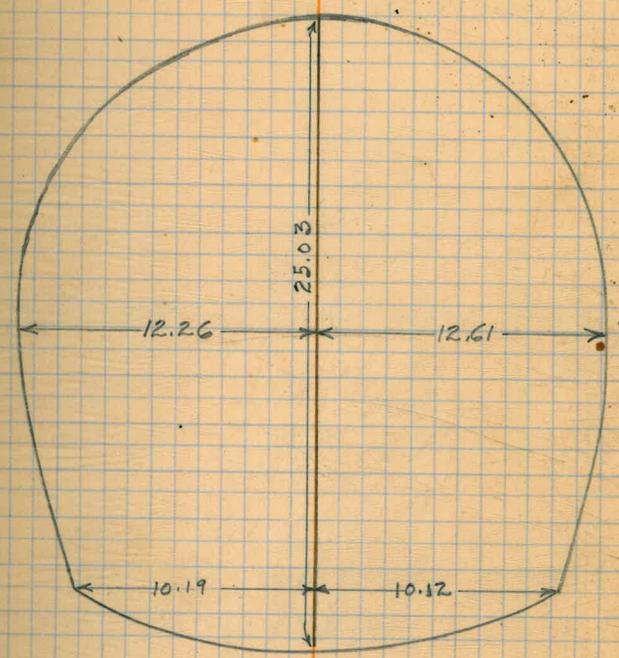
Nov. 28-1934.

4,



⊕

Sta. 2+00



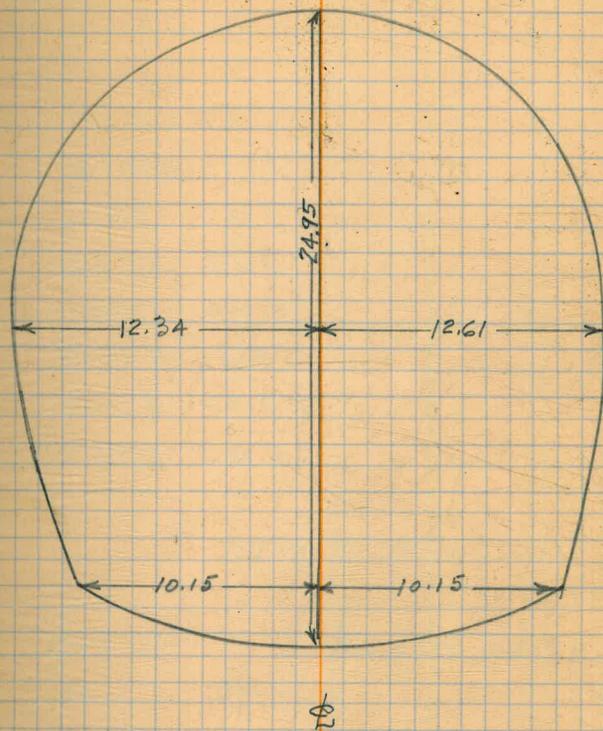
⊕

Sta. 2+50

Measurements of Finished Concrete
Lines in Diversion Tunnel cont'd.

Nov. 28-1934

5.



Sta. 3+00

Continued on Page 9

Spring Line Points,

Dec. 8-1934.

B.M.	13.00	575.11	562.11	
			2.90	572.21 Rec. Elev. 572.22
1+31			2.64	572.47
+50			2.95	572.16
+75			3.37	571.74
2+00			3.78	571.33
+25			4.20	570.91
+50			4.61	570.50
+75			5.03	570.08
3+00			5.44	569.67

Dec. 12-1934

B.M.	7.26	564.4 ⁹	557.2 ³
2+50			+6.02 570.50
+75			+5.60 570.08
3+00			+5.21 569.67
+25			+4.77 569.25
+50			+4.36 568.84
+75			+3.94 568.42
4+00			+3.53 568.01
+20 ⁵⁹			+3.19 567.67

T.P. 9.24 555.2⁵ on lead and took on to
Sta. 4+20⁵⁹.

Spring Line Points.

Dec. 12 - 1934.

7,

T.P. 555.24

3.49 558.73

B.M. 8.46 550.27 = check on B.M. on 8' offset, Lead + tack.
Rec. Elev. 550.30. Sta. 8+17'¹⁵

Dec. 13 - 1934.

B.M. 6.92 562.17 555.25 L.A. & T.K. on ϕ Sta. 4+20⁵⁷

4+50 +5.01 567.18

+75 +4.59 566.76

5+00 +4.18 566.35

T.P. 6.92 555.25

4.88 560.13

5+00 check +6.22 566.35

+25 +5.80 565.93

+50 +5.39 565.52

+75 +4.97 565.10

6+00 +4.56 564.69

Dec. 14 - 1934.

B.M. 4.47 559.72 555.25

6+25 +4.55 564.27

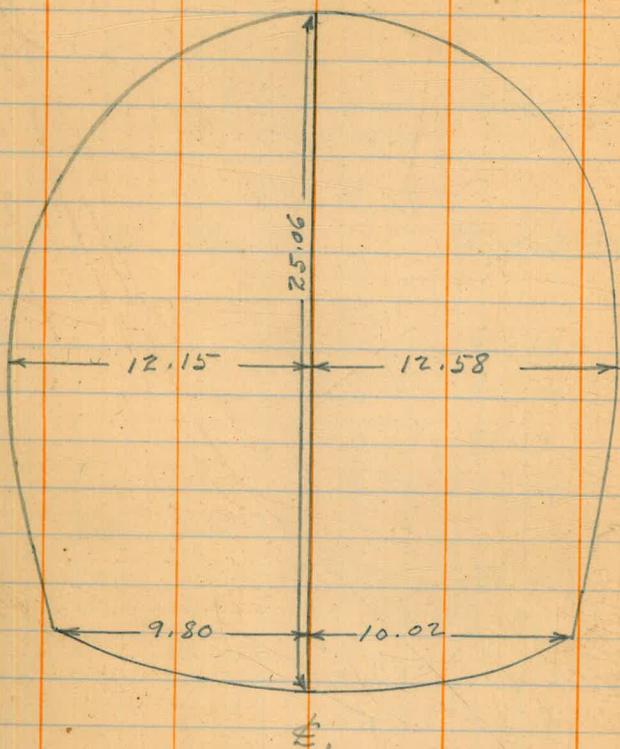
+50 +4.14 563.86

+75 +3.72 563.44

7+00 +3.31 563.03

B.M. 9.46 550.26 Rec. Elev. 550.30

Measurements of Finished Concrete Lines
in Diversion tunnel.



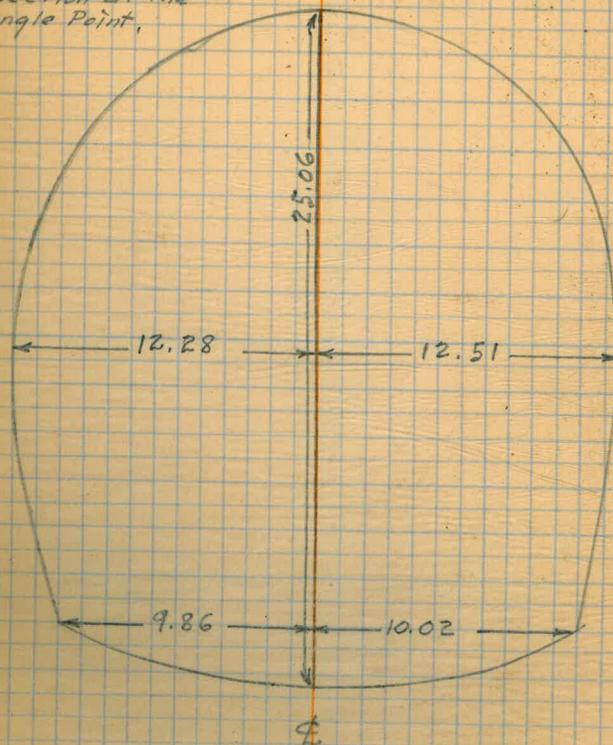
Sta. 4+17.6

Note: This X-section is taken Normal
to the East tangent.

Dec. 14-1934.

8.

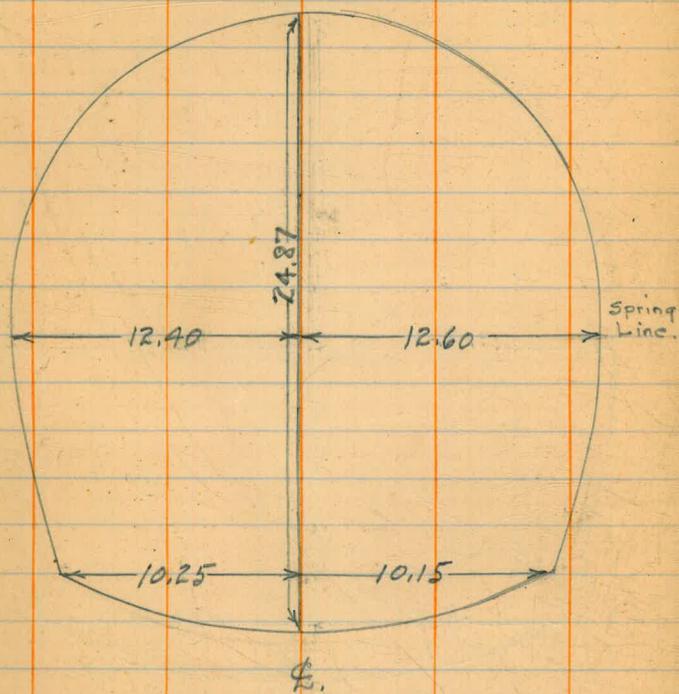
Note: See Page 10, For
X-section at the
Angle Point.



Sta. 4+23.6

Note: This X-section is taken Normal
to the West tangent.

Measurements of Finished Concrete
Lines of Diversion Tunnel
Dec. 12-1934.



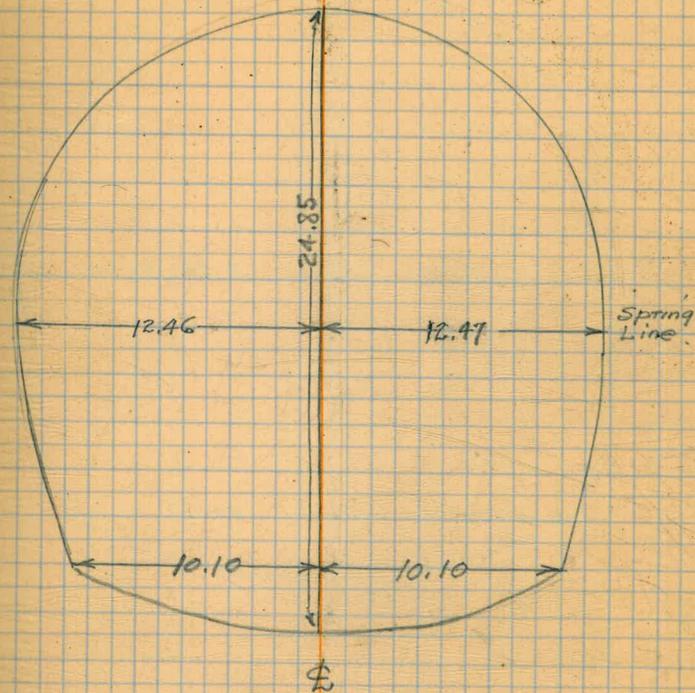
Sta. 3+50

25.00

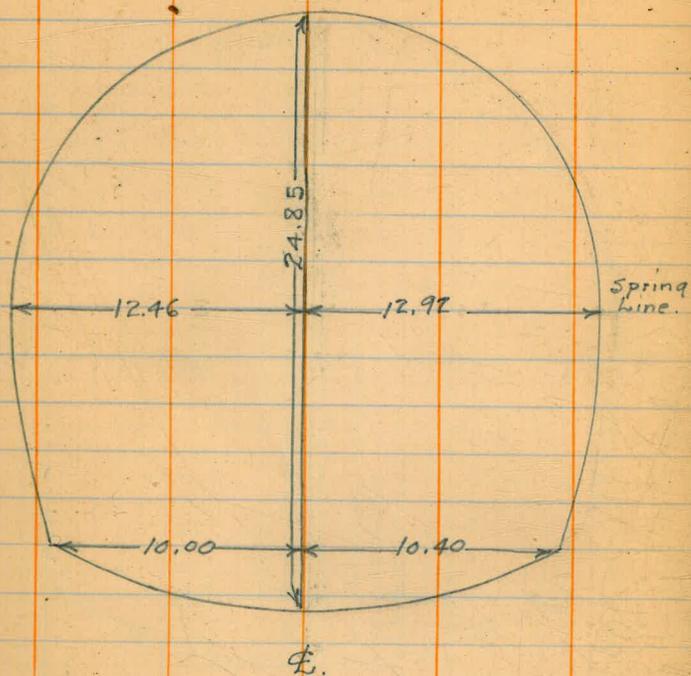
Simpson
Saper
Isbell
Remmen
Salgado

Cont'd. from Page 5.

9.



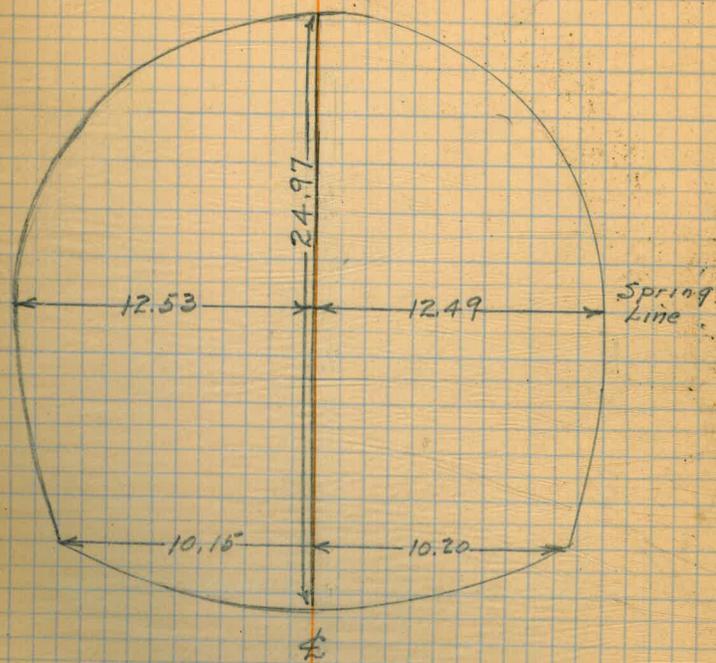
Sta. 4+00



Sta. 4 + 20⁵⁹ Δ

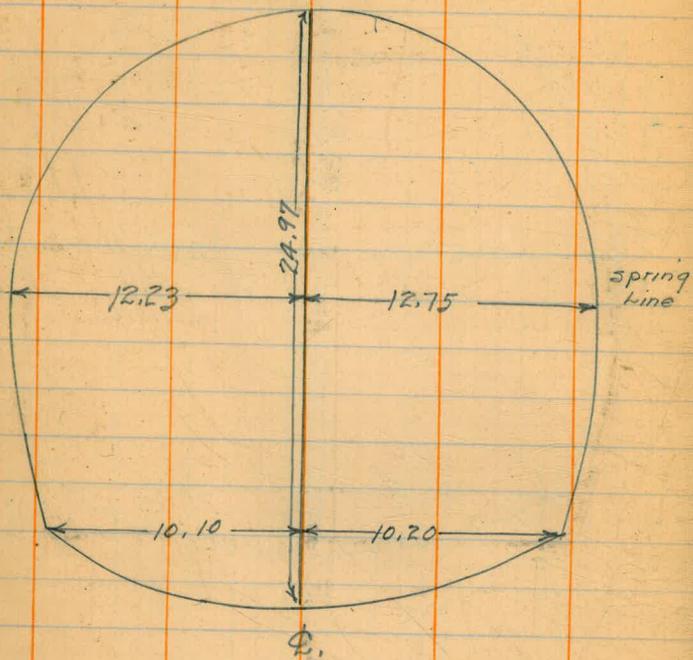
This Xsection is taken on the
Split of the Angle at Φ .

See Page 8, For Xsection on either
Side of the Angle Point.



Sta. 4 + 50

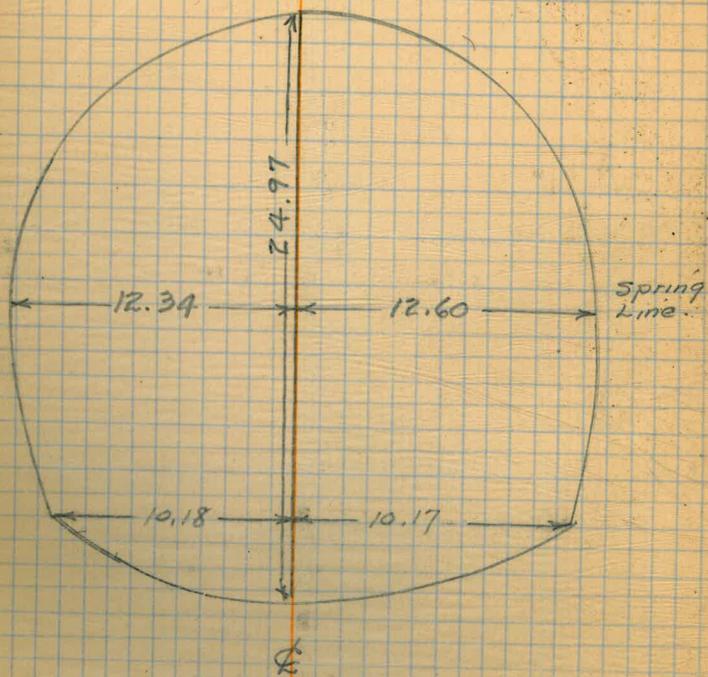
Measurements of Finished Concrete Lines
of Diversion Tunnel cont'd.



Sta. 5+00

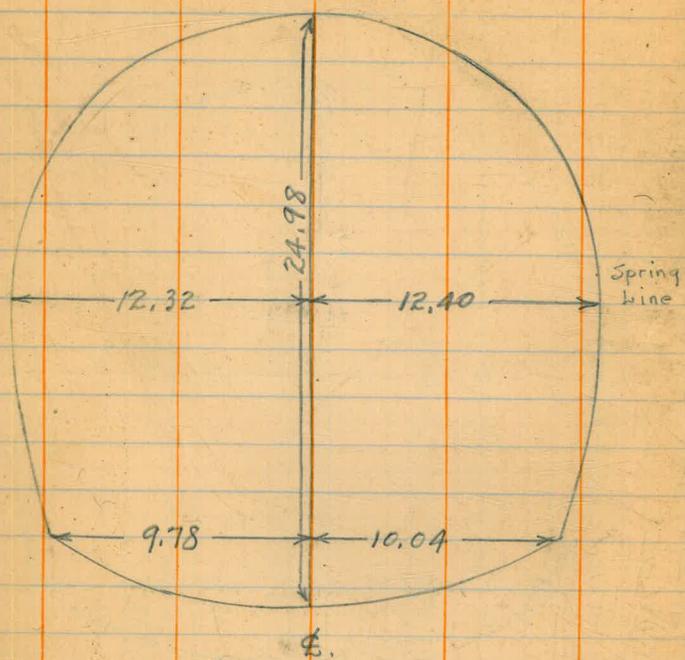
Dec. 12, 1934.

11

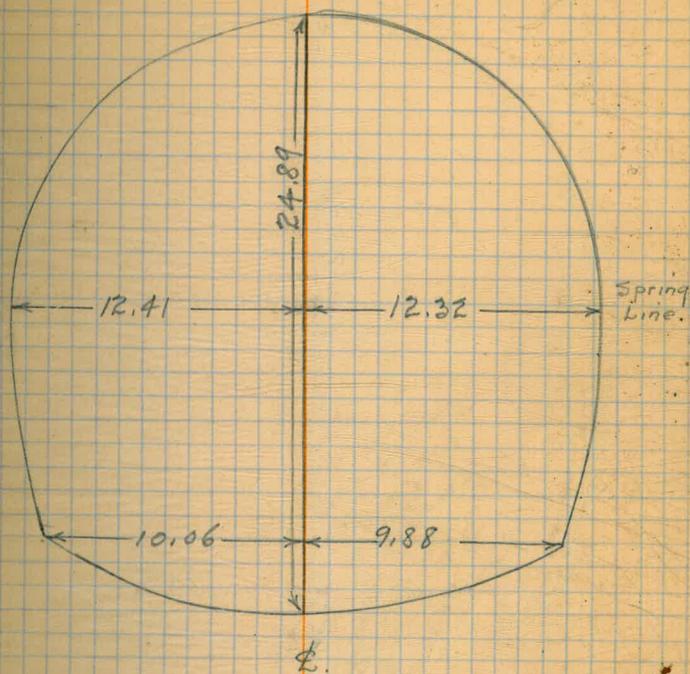


Sta. 5+50

Measurements of Finished Concrete Lines
of Diversion Tunnel. cont'd.



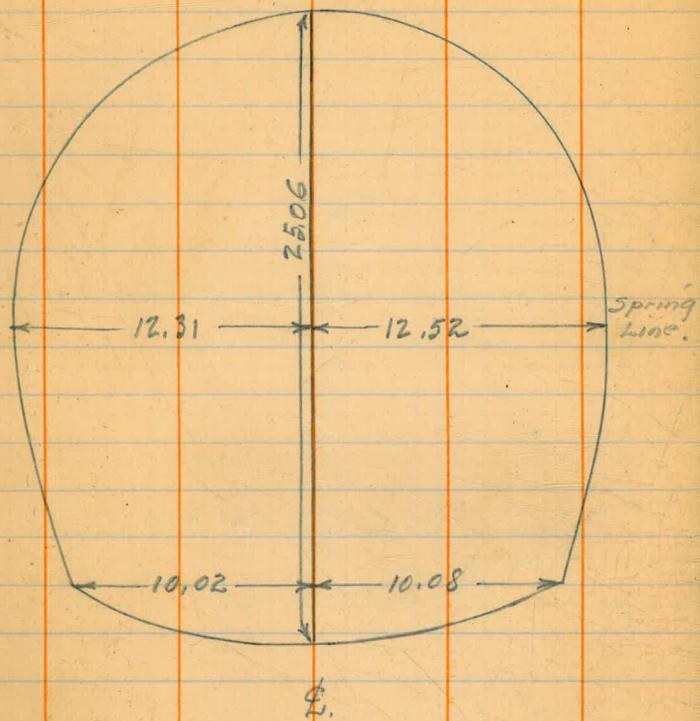
Sta. 6+00



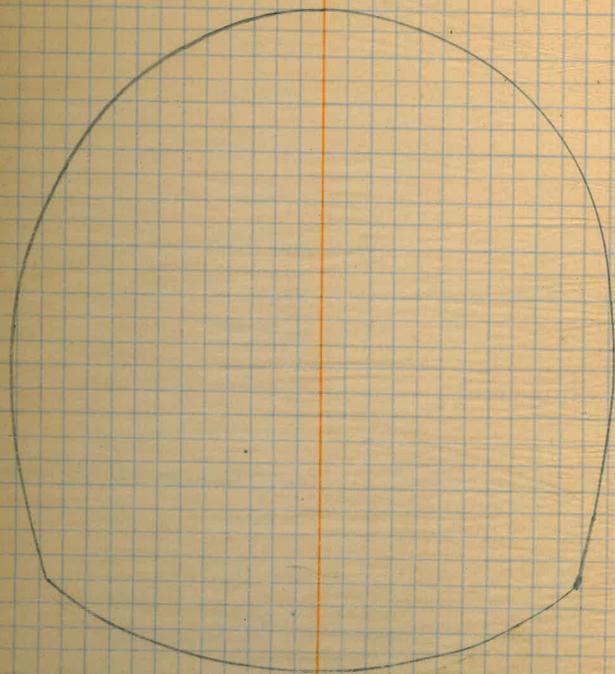
Sta. 6+50

Measurements of Finished Concrete
Lines in Diversion Tunnel contd.

13



Sta. 7+00



Profile of concrete invert on ϕ
and at edges. Cont'd. From Page 2.

Dec. 12-1934.

561.47

3+60 ϕ	5.07
+70 "	5.26
+80 "	5.50
+90 "	5.63
4+00 ϕ	5.80
" N. edge invert	3.89
" S. " "	3.96
+10 ϕ	6.03
+20 ⁵⁹ ϕ	6.20 555.27
" N. edge invert	4.25
" S. " "	4.13
+30 ϕ	6.39
+40 "	6.60
+50 "	6.71
" N. edge invert	4.67
" S. " "	4.77
+60 ϕ	6.89
+70 "	7.04
+80 "	7.25
+90 "	7.40
5+00 ϕ	7.53
" N. edge invert	5.49
" S. " "	5.51

on split of the angle
"

Profile of concrete invert on ϕ and
at edges cont'd.

Dec. 13 - 1934.

15

B.M. 7.93 558.23

550.30 = 8' offset

ld. & rk. on south side
of Δ sta. 8+17⁵/₂

5+10	ϕ	4.47
+20	"	4.70
+30	"	4.85
+40	"	5.06
+50	ϕ	5.11
"	N. edge invert	3.03
"	S. " "	3.05
+60	ϕ	5.20
+70	"	5.44
+80	"	5.64
+90	"	5.81
6+00	ϕ	5.94
"	N. edge invert	3.89
"	S. " "	3.94
+10	ϕ	6.12
+20	"	6.23
+30	"	6.43
+40	"	6.52
+50	ϕ	6.59
"	N. edge invert	4.72
"	S. " "	4.76

Profile of concrete invert on ϕ and at edges,
cont'd.

Dec. 13-1934

76

558.23

6+60 ϕ	6.81	
+70 "	7.02	
+80 "	7.18	
+90 "	7.43	
7+00 ϕ	7.68	50.55
" N. edge invert	5.55	
" S. " "	5.55	

7.93 550.30 = check on B.M. Elev. 550.30

Re-Tracing Co. Road Survey # 512
From El Monte Pumping Plant to El Monte
Park.

March - 27-1935
Hill - Simpson
Soper - Remmen

17

101+85.36 E.C.

+50 12° 19'

101+00 9° 27'

+50 6° 35'

100+00 3° 43'

99+50 0° 51'

99+35.20 B.C.

81+69.80 E.C.

Void - see loose leaf
book - J.W.W.
Page 65 this book

Δ 28° 40' R.
R-500
T-127.76
L-250.16

Blotted on Profile 99+17-25
4/4/35 J.W.W.

R.P. 30' □ 30' R.P. 30' □ 30' R.P.
Fd. 1/2" steel
Steel Pin Pin

El Monte
Pumping
Plant.

97+00
Fd. 1/2" steel
R.P. 29' □
1/2" Steel Pin

Void - see J.W.W.'s
loose leaf book.
Page 66, this book.

124+72.44 E.C.

+50

124+00

+50

123+00

+50

122+00

+50

121+00

+50

120+00

+50

119+00

+50

118+40.47 B.C.

Δ 36°12'30" L.

R. 1000'

T. 326.90

L. 631.95

152+65 P.O.T.

152+55.03 "

143+08.21 E.C.

143+00 4°06.9

+50 2°40.9

142+00 1°15'

141+56.38 B.C.

 $\Delta = 8^{\circ}42'30'' R$

R: 1000'

T: 76.14

L: 151.99

P.C. 50'
 R.P. 30' \square 30' \square
 1/2" steel pin R.P. 1/2" steel
 P.C. 1/2" pin

134+72.32 E.C.

+50 7°55.9

134+00 5°53.1

+50 3°50.3

133+00 1°47.5

132+56.38 = B.C.

132+06.38

 $\Delta 17^{\circ}40'30'' R$

R: 700'

T: 108.32

L: 215.94

Note: 50' Error in chaining.

Cont'd. From Page 19.

187+31.57 E.C.

A-33°00' R.
R-500'
T-148.11
L-287.98.

184+43.59 B.C.

181+34.93 E.C.

A 24°07'30" R.
R-1500'
T-320.54
L-631.59

175+03.34 B.C.

March-28-1935
Hill-Simpson
Soper-Remmen.

20

R.P. 30' R.P.
Fd. 1/2" Steel Pin Fd. 1/2" Steel Pin

E.C. 181+34.93 - 12°03'45"

181+00 - 11°23.8'
+50 - 10°26.5'
180+00 - 9°29.2'
+50 - 8°31.9'
179+00 - 7°34.6'
+50 - 6°37.3'
178+00 - 5°40'
+50 - 4°42.7'
177+00 - 3°45.4'
+50 - 2°48.1'
176+00 - 1°50.2'
175+50 - 0°53.5'

B.C. 175+03.34

30' R.P.
Fd. 1/2" Steel Pin

204+67.27 E.C.

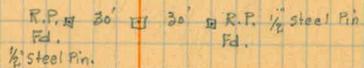
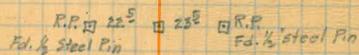
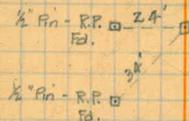
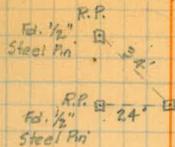
A-47°22' L
 R-600'
 T-263.17
 L-496.02

199+71.25 B.C.

192+66.74 E.C.

A-38°58' L
 R-600'
 T-212.27
 L-408.06

188+58.68 B.C.



Contd. From Page 21

March-29-1935
Hill - Simpson
Soper - Remmen.

22

234+88.32 E.C.
234+95.28 P.O.T.

O.K. to Here.
Contd. on Page 26.

234+84.24 E.C.

A-32°57'R
R-1200'
T-354.89
L-690.10

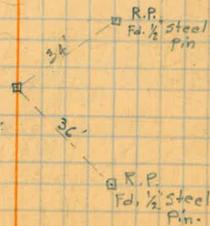
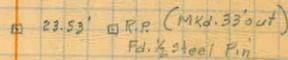
227+94.14 B.C.

223+01.61 E.C.

222+10.00 P.I.

A-3°00'L
R-3500'
T-91.65
L-183.26

221+18.35 B.C.



255+49.06 E.C.

Δ -21°04'30" L.
R-1000'
T-186.02
L-367.83

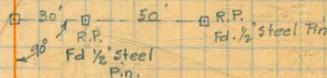
251+81.23 B.C.

244+07.99 E.C.

Void
See Page 26

Δ -26°30' L.
R-1000'
T-235.47
L-462.51

239+45.48 B.C.



Void



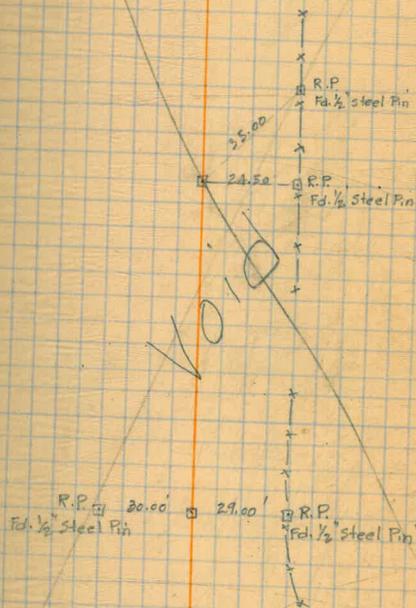
279+08.09 E.C.

Void
See Pages 26-

A-60°02'R.
R-625'
T-361.09
L-654.86

272+53.23 B.C.

265+40.75 P.O.T.



287+29.28 F.C.

Void.
See Pages 26-

$\Delta = 17^{\circ}34'30''$ R.
R. 1500'
T. 281.88
L. 460.11

282+69.17 B.C.

R.P. 30.00 Fd. $\frac{1}{2}$ Steel Pin
25.00 R.P. Fd. $\frac{1}{2}$ Steel Pin

Void

30.00 R.P. Fd. $\frac{1}{2}$ Steel Pin

Gate to El Monte Park

13.50 R.P. Fd. $\frac{1}{2}$ Steel Pin

Co. Road Survey # 512, Transit Notes.
Contd. From Page 22.

255+96.85 E.C.

Void see Page 58

$\Delta 2519'50''$ L.

R. 1000'

T. 224.72

L. 442.10

251+54.75 B.C.

244+90.00 P.O.T.

$N43^{\circ}22'50''$ E.

243+88.61 E.C.

$\Delta 24^{\circ}09'40''$ L.

R. 1000'

T. 214.03

L. 421.69

239+66.92 B.C.

$N67^{\circ}32'30''$ E

Co. Road Survey #512 - Transit Notes.
Cont'd. From Page 27.

310+91.10 E.C.

$\Delta = 10^{\circ}00' R.$
 $R = 1500'$
 $T = 131.23$
 $L = 261.80$

547°55'E.

308+29.30 B.C.

304+23.72 P.O.T.

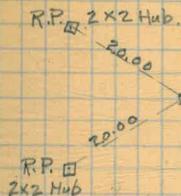
557°55'E.

294+41.92 E.C.

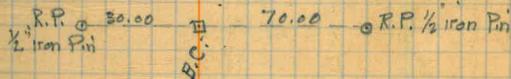
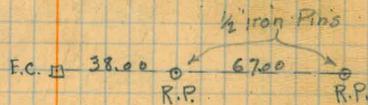
$\Delta = 24^{\circ}30'30'' R.$
 $R = 600'$
 $T = 130.32$
 $L = 256.65$

291+85.27 B.C.

582°25'30"E.



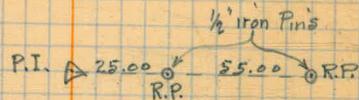
$\Delta PI.$



278°47'E ✓

325+53.71 E.C.

$\Delta = 16^\circ 17' L$
 $R = 1500'$
 $T = 214.59$
 $L = 426.30$

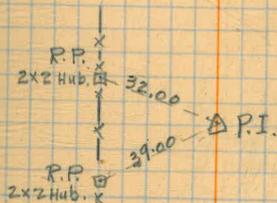


321+27.41 B.C.

562°30'E ✓

316+71.88 E.C.

$\Delta = 7^\circ 05' 30'' R$
 $R = 1500'$
 $T = 92.94$
 $L = 185.66$

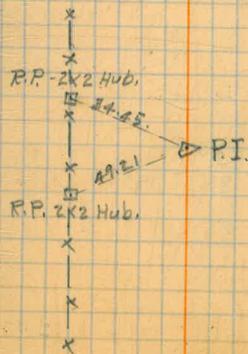


314+86.22 B.C.

569°35'30"E ✓

314+40.39 E.C.

$\Delta = 21^\circ 40' 30'' L$
 $R = 600'$
 $T = 114.86$
 $L = 226.98$



312+13.41 B.C.

547°55'E ✓

Co. Road Survey #512 - Transit Notes.
Cont'd. From Page 29.

342+73.80 P.O.T.

S 45° 02' E.

341+22.12 E.C.

A = 16° 43' R.
R = 500'
T = 215.94
L = 407.68

337+14.44 B.C.

336+30.00 P.O.T.

334+65.65 P.O.T.

330+95.78 Intersection with El Monte Ranch Line

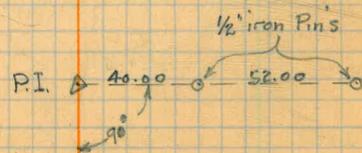
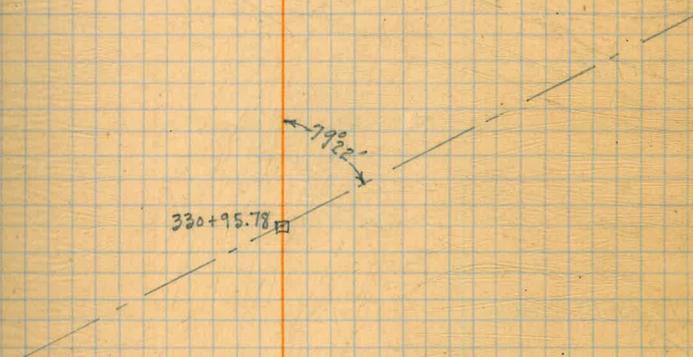
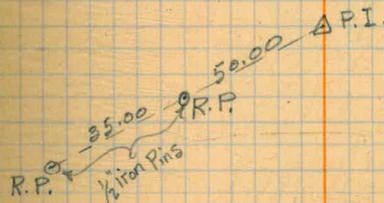
N 88° 15' E.

330+87.15 E.C.

A = 12° 58' L.
R = 1000'
T = 113.64
L = 226.31

328+60.84 B.C.

S 78° 47' E.

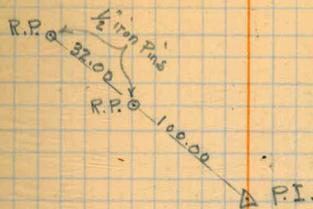


Co. Road Survey #512 - Transit Notes.
Contd. From Page 30.

S86°11'E ✓

357+26.28 F.C.

$\Delta = 14^{\circ}31' L.$
 $R = 600'$
 $T = 75.84$
 $L = 152.02$



355+74.26 B.C.

S71°40'E ✓

352+17.16 F.C.

$\Delta 8^{\circ}11'30'' L.$
 $R = 1774.25$
 $T = 127.05$
 $L = 253.67$



349+63.49 P.C.C.

$\Delta = 18^{\circ}26'30'' L.$
 $R = 1000'$
 $T = 162.34$
 $L = 321.84$

346+41.65 B.C.

344+89.48 P.O.T.

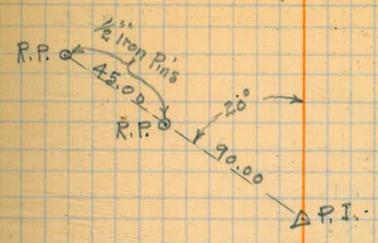
S45°02'E

Co. Road Survey #512. - Transit Notes.
Cont'd: From Page 31.

369+43.10 E.C.

$\Delta = 7^{\circ}55' L.$
 $R = 1500'$
 $T = 103.79$
 $L = 207.06$

$579^{\circ}48' E.$



367+35.84 B.C.

$\Delta = 20^{\circ}12' L.$
 $R = 400'$
 $T = 71.25$
 $L = 141.02$

$571^{\circ}53' E.$

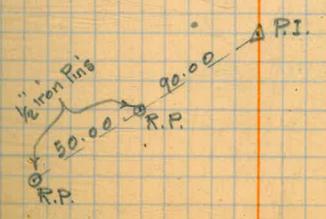
366+07.48 E.C.

364+66.46 B.C.

$\Delta = 34^{\circ}30' R.$
 $R = 450'$
 $T = 139.73$
 $L = 270.96$

$551^{\circ}41' E.$

362+76.07 E.C.



360+05.11 B.C.

$586^{\circ}11' E.$

Co. Road Survey #512 - Transit Notes.
Cont'd. from Page 32.

378+61.72 E.C.

S71°43'E ✓

Δ=21°50'R.
R=500'
T=96.44
L=190.53

376+71.19 B.C.

N86°27'E

Δ=19°45'L.
R=600'
T=104.45
L=206.82

376+05.08 E.C.

373+98.26 B.C.

S73°48'E ✓

Δ680'R.
R=2000'
T=104.82.
L=209.44

373+63.33 E.C.

371+53.89 B.C.

S79°48'E

1/2 Iron Pin
R.P. @

89.00

←21°50'→

6.4% Road Survey to Top of Dam
And Co. Rd. Survey Forward to next

42.77

□ 30+99.74
6.4% Road From
Top of Dam.

377+67.63 =

23+26.08 = Pipe Line
30+56.96 = 6.4% Road From
Top of Dam.

P.I. A

26.50

⊙ Nail in Oak

⊙ Nail in Oak.

P.I. A 23.00

1/2 Iron Pins

43.00

←12°

Co. Road Survey #606. Transit Notes.
From Lakeside to El Monte Pumping
Plant.

34

N 81° 01' E

0+00

MAINE
St.

⊙ = 0+00, Co. Rd. Survey #606
P.I. Julian Rd. Stone Mon.

Woodside

Ave

27' 13"

Co. Road Survey #606 - Transit Notes
From Lakeside to El Monte Pumping Plant
Cont'd. From Page 34.

N25°49'30"E

69+34.35 E.C.

$\Delta = 54^{\circ}59' L.$
R = 1000'
T = 520.40
L = 959.64

59+74.71 B.C.

N80°48'30"E

25+50.36 P.I.

0°12'30" L.

N81°01'E

R.P. \odot 30.00 \square 30.00 \odot R.P.
 $\frac{1}{2}$ Iron Pin $\frac{1}{2}$ Iron Pin

R.P. \odot 30.00 \square 30.00 \odot R.P.
 $\frac{1}{2}$ Iron Pin $\frac{1}{2}$ Iron Pin

R.P. \odot 30.00 Δ
 $\frac{1}{2}$ Iron Pin

Co. Road Survey #606. - Transit Notes
From Lakeside to El-Monte Pumping Plant,
Cont'd. From Page 35.

Cont'd. On Page 17 - This Book.

99+35.20 B.C.

N47°57'30"E

81+69.80 E.C.

Δ 22°08'
R. - 1000'
T. = 195.59
L. = 386.30

77+83.50 B.C.

N25°49'30"E

May - 7 - 1935.

Tel. And Power Poles that will have
to be Moved For Pipe Line or Road
Construction.

62+27 Power Pole #78768 - 7' Rt. of E. Rd. Survey

79+78 " " #74100 - 5' Rt. " " " "

115+77 " " #173401 - 15' Rt. " " " "

116+80 36" Sycamore Tree - 14' Lf. " " " "

118+89 Tel. Pole #305872H - 45' Lf. " " " "

126+07. " " #B28870P - 11' Lf. " " " "

130+93 " " #D28872T - 23' Rt. " " " "

133+42 Power Pole #72763 - 16' Rt. " " " "

135+57 Tel. Pole #D28874T - 20' Rt. " " " "

138+06 " " #D28875T - 10' Rt. " " " "

143+94 " " #306165H - 14' Rt. " " " "

152+32 " " #D28880T - 14' Lf. " " " "

180+97 " " #D28895T - 2' Lf. " " " "

190+70 " " #305919H - 9' Rt. " " " "

194+95 Guy Pole 17' Lf. " " " "

194+95 Power Pole #173423 - 18' Rt. " " " "

Hill - Simpson
Soper - Remmen,

37

Note: Location From Alternate Line #3.

" " " " " "

" " " " " "

" " " " " "

Note: Location From Orig. Co. Survey

" " " " " "

" " " " " "

Tel. And Power Poles that Will Have to Be
Moved For Pipe Line or Road construction
cont'd. From Page 37.

225+87	Tel. Pole	#D29177T	14' Lf.	of & Road Survey
228+84	" "	#D29178T	45' Lf.	" " " "
231+73	" "	#D29179T	22' Lf.	" " " "
238+75	" "	#D29182T	2' Lf.	" " " "
240+71	" "	#D29183T	105' Lf.	" " " "
242+74	" "	#D29184T	145' Rt.	" " " "
255+00	" "	#D29189T	8' Rt.	" " " "
279+82	Power Pole	#76577	14' Lf.	" " " "

May-8-1935.

38

Note: Location is From Revised Line

" " " " "

" " " " "

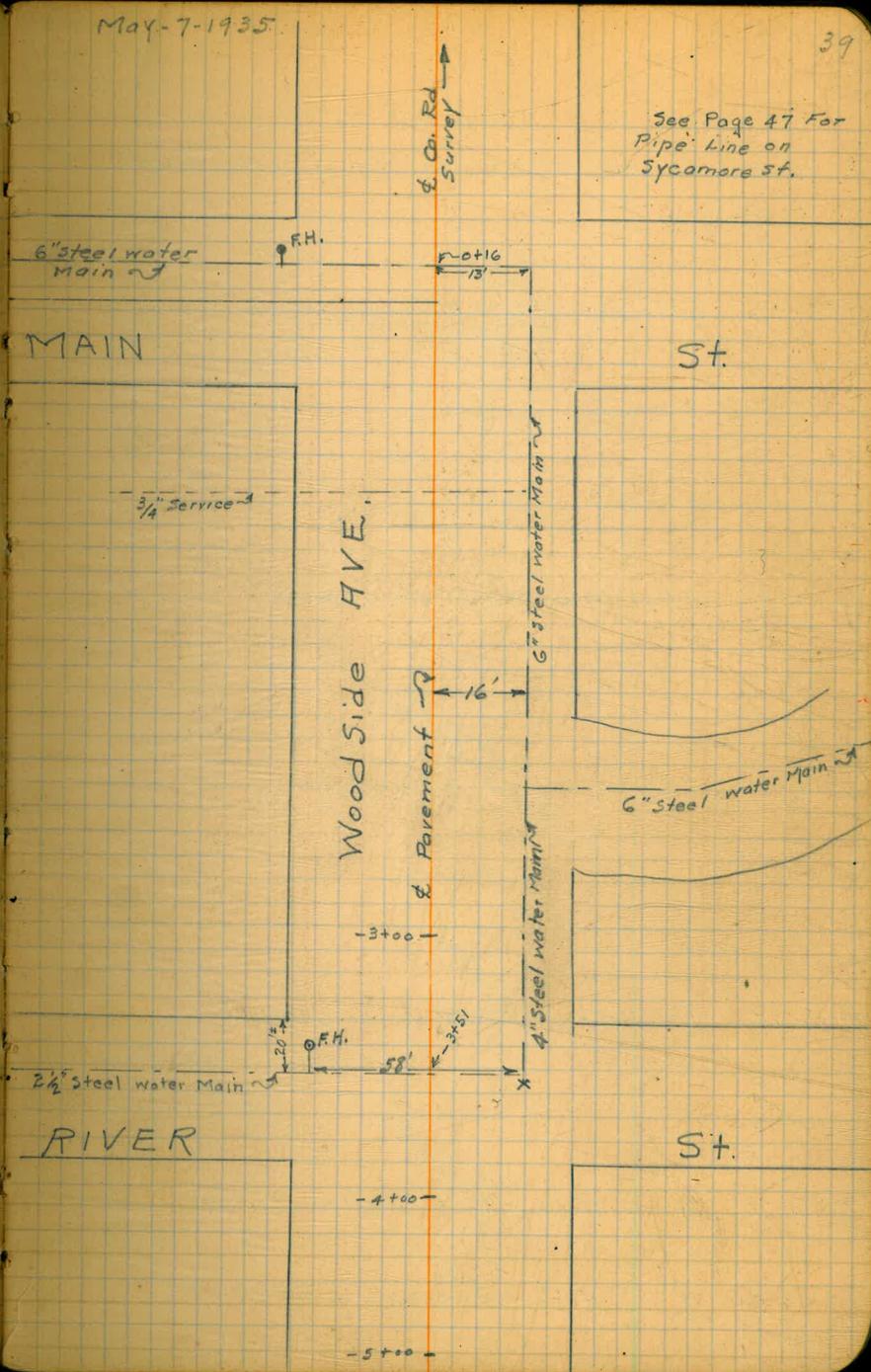
Location And Elev. of Culverts And Water Lines Along Co. Rd. Survey # 606.

May-7-1935

See Page 47 For Pipe Line on Sycamore St.

413.3
 +16 ϕ Elev. $0+20 - 1\frac{1}{2}$ = Top of 6" Water Main 13' Rt. of Sta. 0+16.
 This Main Runs Practically Level on North.

406.6
 -3+51 ϕ Elev. $-3+50 - 1\frac{1}{2}$ = Top of 2 1/2" Steel Water Main 21' Lf of ϕ Pavement.



May-7-1935
 Hill - Simpson
 Soper - Remmen.

40

Location And Elev. of Culverts and
 Water Lines Along Co. Rd. Survey #606
 Cont'd.

83+23 ϕ Elev. 83+00 - 2' = 83.0 = Flow Line 13' Rt.
 " " " - 3' = 82.7 = " " 16' Lt.

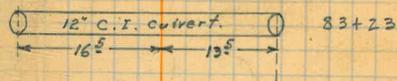
81+64 ϕ Elev. 81+50 - 2' = 81.3 = Flow Line

81+42 ϕ Elev. 81+50 - 1' = 81.4 = Flow Line

78+95 ϕ Elev. 79+00 - 2' = 79.8 = Flow Line Culvert

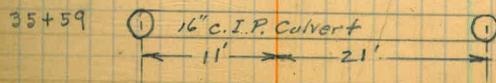
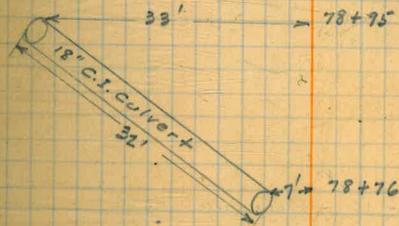
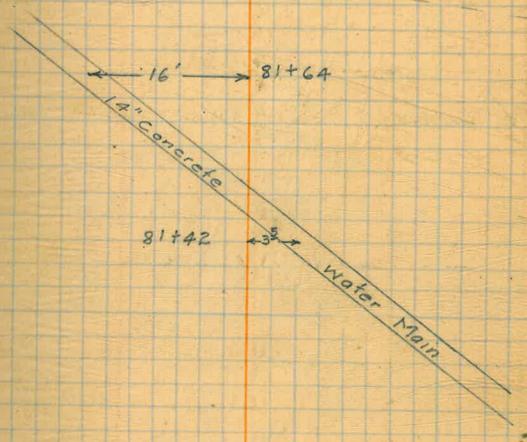
78+76 ϕ Elev. 79+00 - 1' = 78.9 = Flow Line Culvert

35+59 ϕ Elev. 35+50 - 2' = 35.3 = Flow Line 21' Rt. ϕ
 " " " - 2' = 35.0 = " " 11' Lt. ϕ



82+34 2" water line xing ϕ

81+84 2" water line xing ϕ



Location And Elev. of Culverts And water Lines contd.

103+77 $\frac{1}{2}$ Elev. 103+50 - 2' = Flow Line Culvert
 (Orig. Co. Survey) = 436.1

103+64 $\frac{1}{2}$ Elev. 103+50 - 2' = Flow Line "
 (Orig. Co. Survey) = 436.7

99+22 $\frac{1}{2}$ $\frac{1}{2}$ Elev. 99+00 - 4' = Flow Line 12" steel Pipe 16' Lf $\frac{1}{2}$
 = 434.2

99+10 " " " - 3' = 435.0 " " 12" iron Pipe 16' Lf $\frac{1}{2}$

99+03 $\frac{1}{2}$ " " " - 3' = 435.4 " " " steel " 32' Rt. $\frac{1}{2}$

98+93 " " " - 5' = 433.1 " " " iron " 21' Lf $\frac{1}{2}$

98+79 " " " - 3' = 435.6 " " " " " 32' Rt. $\frac{1}{2}$

98+73 $\frac{1}{2}$ " " " - 3' = 435.6 " " " " " 32' Rt. $\frac{1}{2}$

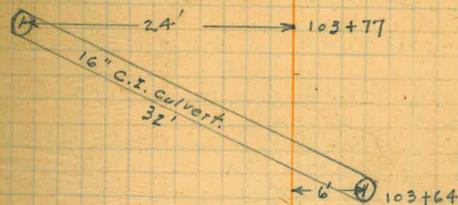
" " " - 6' = 432.4 = Elev. Bottom of Reservoir

88+21 $\frac{1}{2}$ Elev. 88+00 - 1' = Flow Line 19' Rt. $\frac{1}{2}$
 = 433.8

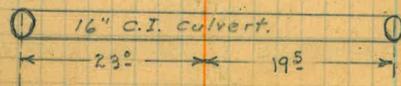
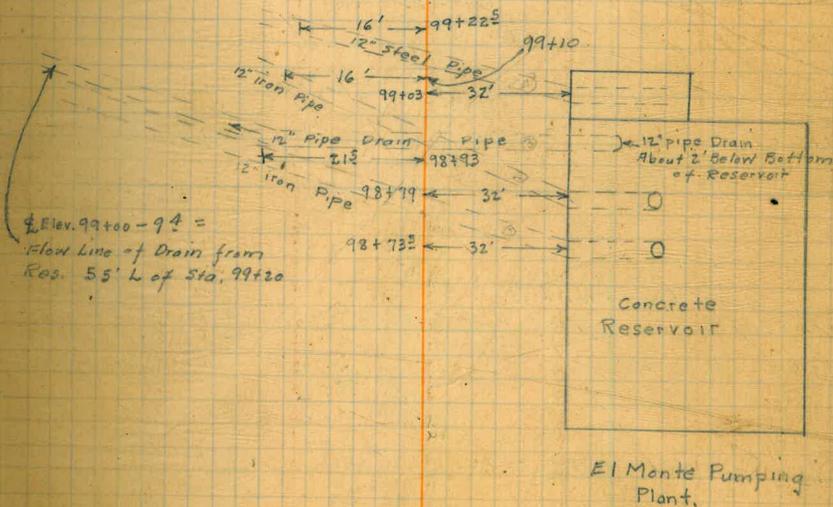
" " " - 2' = 433.3 " " 23' Lf.

May-7-1935.

41



Note: Location From Alternate Line "2"



Location And Elev. of Culverts And water Lines Contd.

May-7-1935.

42

122+22 (Alternate Line #3) ϕ Elev. 122+00 - 2' = 122.0 = Flow Line culvert = 122.1

122+09 " - 1' = 122.0 = " " " = 122.6

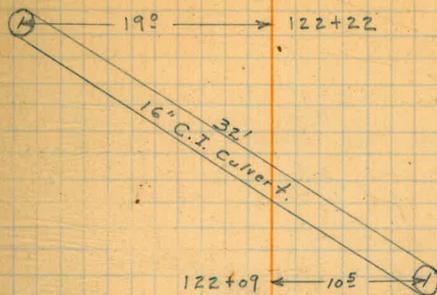
116+97 (Alternate Line #3) ϕ Elev. 117+00 - 4' = 117.0 = Flow Line 14' Rt. of ϕ = 117.4

116+85 " - 5' = 116.0 = " " 45' Lf. of ϕ = 116.3

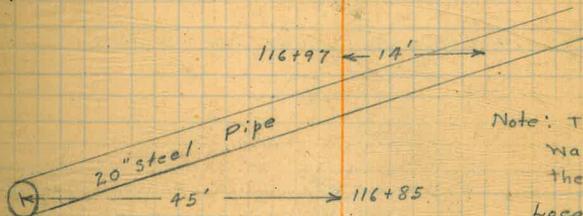
114+20 (Alternate Line #2) ϕ Elev. 114+00 - 3' = 114.0 = Flow Line culvert = 114.0

114+11 " - 2' = 114.0 = " " " = 114.0

110+07 (Orig. Co. Survey) ϕ Elev. 110+00 + 0' = 110.0 = Flow Line 3' Rt. of ϕ = 110.3
" " " + 1' = 110.0 = " " 25' Lf. of ϕ = 110.3



Note: Location From Alternate Line #3



Note: This Pipe is for waste water from the flume.

Location From Alternate Line #3



Note: Location From Alternate Line #2



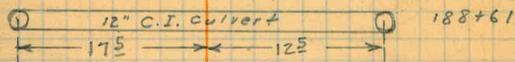
Note: Location From Alternate Line #2.

Location And Elevs. of Culverts. And Water Lines Cont'd.

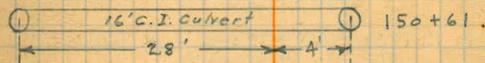
May-7-1935

43

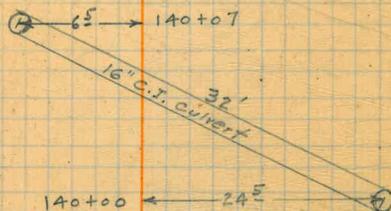
188+61 $\frac{1}{2}$ Elev. 188+50 - 2° = Flow Line Culvert 12⁵ Rt. $\frac{1}{2}$
 " " " " - 2° = " " " 17⁵ Lf. $\frac{1}{2}$
 A77.1
 A76.4



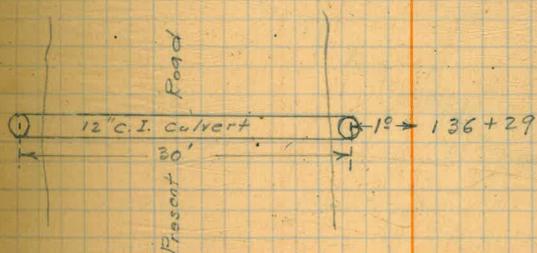
150+61 $\frac{1}{2}$ Elev. 150+50 - 2° = Flow Line Culvert 4' Rt. $\frac{1}{2}$
 " " " " - 2° = " " " 28' Lf. $\frac{1}{2}$
 457.4
 457.0



140+07 $\frac{1}{2}$ Elev. 140+00 - 3° = Flow Line Culvert



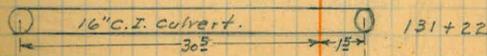
140+00 $\frac{1}{2}$ Elev. 140+00 - 12° = " " "



136+29 $\frac{1}{2}$ Elev. 136+50 - 1° = Flow Line Culvert 1⁰ Lf. of $\frac{1}{2}$
 " " " " - 1° = " " " 31' " " "

Note: Locations and Elevs. from Orig. Co. Survey from 131+22 on.

131+22 $\frac{1}{2}$ Elev. 131+00 - 2° = Flow Line Culvert 15⁵ Rt. of $\frac{1}{2}$
 " " " " - 3° = " " " 30⁵ Lf. of $\frac{1}{2}$
 452.1
 450.7



Location And Elev. of Culverts And Water Lines Cont'd.

May-8-1935

44

197+53 $\frac{480.8}{-2.5}$ Elev. 197+50 = Flow line Culvert

197+41 " " " $\frac{480.0}{-3.3}$ " " "

196+34 $\frac{478.3}{-4.5}$ Elev. 196+00 = Flow Line Pipe

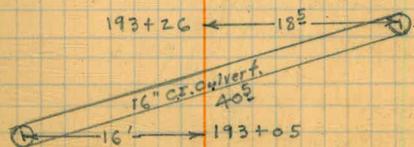
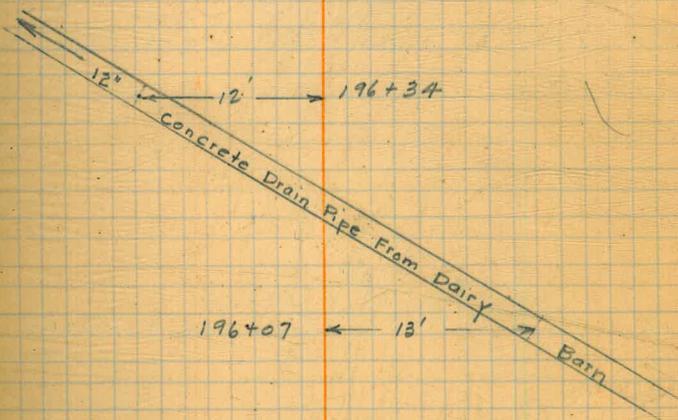
196+07 " " " $\frac{480.3}{-2.5}$ " " "

193+26 $\frac{481.2}{-1.1}$ Elev. 193+00 = Flow Line Culvert

193+05 " " " $\frac{480.0}{-2.2}$ " " "



196+52 2" water line Xing



Location And Elevs. of Culverts and water Lines Cont'd.

225+05 ϕ Elev. 225+00 - 2⁵ = Flow line of Pipe 7' l. ϕ

486.5

224+98 " " " - 1⁵ = " " " 21' Rt. ϕ

487.6

203+00 ϕ Elev. 202+00 - 2⁹ = Flow Line in Manhole

480.9

202+42 ϕ Elev. 202+50 - 2⁴ = Flow Line in Manhole

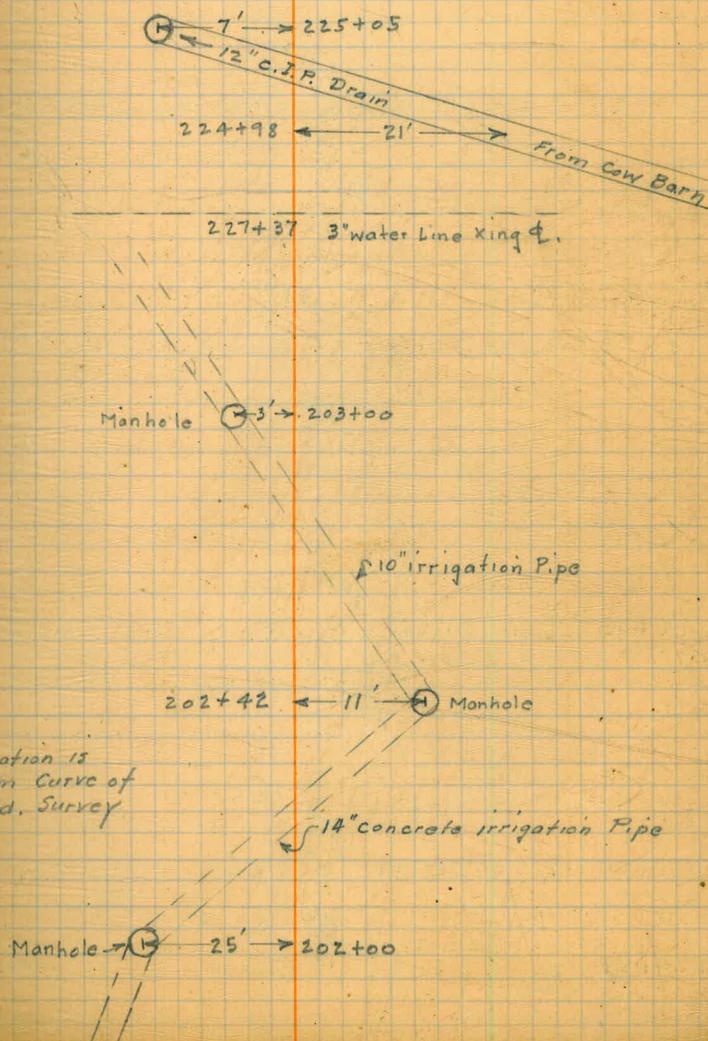
480.3

202+00 ϕ Elev. 202+00 - 2⁵ = Flow Line in Manhole

479.6

May-8-1935

45



Location And Elevs. of Culverts And Water Lines Cont'd.

251+92 ϕ Elev. 252+00 - ^{A99.6} 42 = Flow Line Culvert 26' Lt. of ϕ .
 " " " - ^{A98.7} 51 = " " " 56' " " "

244+23 ϕ Elev. 244+00 - ^{A99.1} 17 = Flow Line Culvert 19' Lt. of ϕ .
 " " " - ^{A98.5} 18 = " " " 43' Lt. of ϕ .

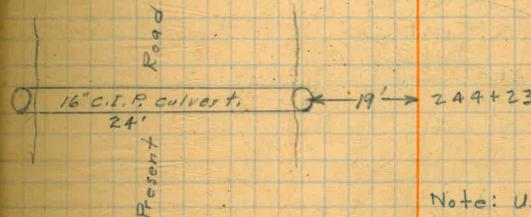
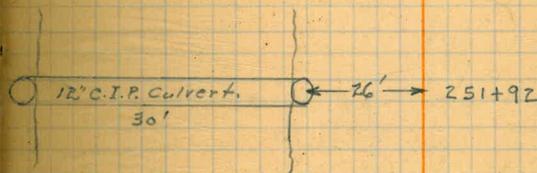
241+10 ϕ Elev. 241+00 - ^{A98.1} 15 = Flow Line Rt. of ϕ .
 " " " - ^{A96.1} 35 = " " 20' Lt. of ϕ .

226+29 ϕ Elev. 226+00 - ^{A87.6} 28 = Flow Line Culvert 125' Lt. ϕ .

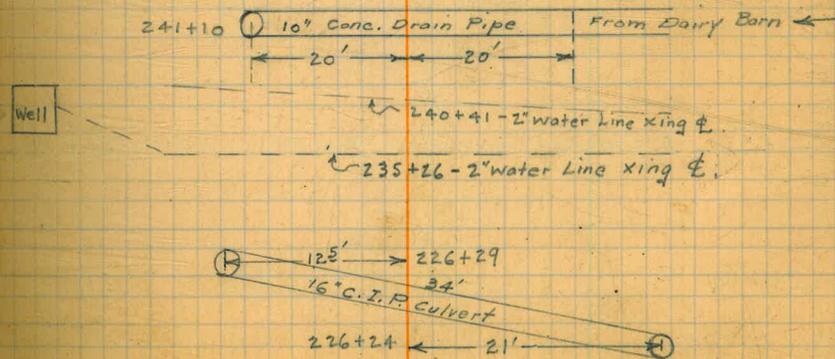
226+24 " " " - ^{A88.6} 10 = " " " 21' Rt. ϕ .

May-8-1935

46



Note: Use Revised Line From Sta. 239+ to Sta. 276+ For Locations And Elevs.



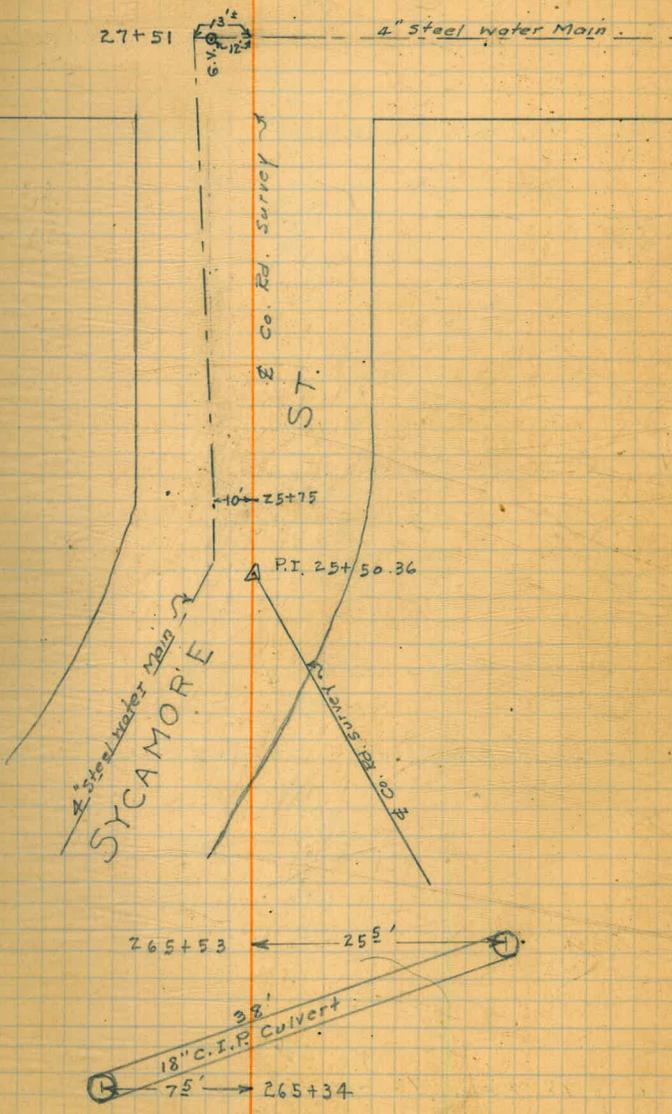
Location And Elev's. of Culverts And Water Lines contd.

27+51 $\frac{1}{2}$ Elev. 27+50 - $1\frac{3}{4}$ = Top of 4" pipe at Gate valve
12' Lf. of $\frac{1}{2}$. 110.6

25+75 $\frac{1}{2}$ Elev. 25+50 - $1\frac{1}{2}$ = Top of 4" Pipe 10' Lf of $\frac{1}{2}$
" " " + $0\frac{1}{2}$ = $\frac{1}{2}$ Elev. (on Road)
100.9
107.9

265+53 $\frac{1}{2}$ Elev. 265+50 - $3\frac{1}{2}$ = Flow Line Culvert 25' Rt. of $\frac{1}{2}$
98.5

265+34 " " " - $3\frac{1}{2}$ " " " 75' Lf. of $\frac{1}{2}$.
98.1



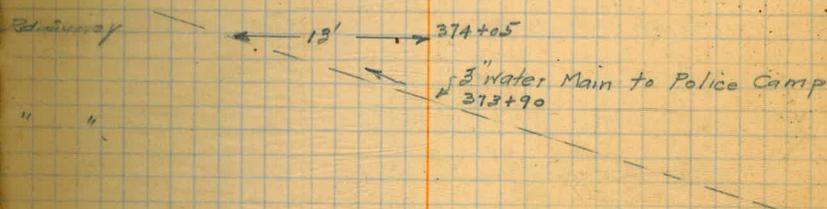
Location And Elev. of Culverts And water Lines Cont'd.

May-13-1935,

48

374+05 \pm Elev. 373+50 - ^{556.1}1⁵ = Top of 2" water Main 13' Lf. of \pm Rd. Survey

373+90 " " " - ^{557.3}0³ = " " " " on \pm " "

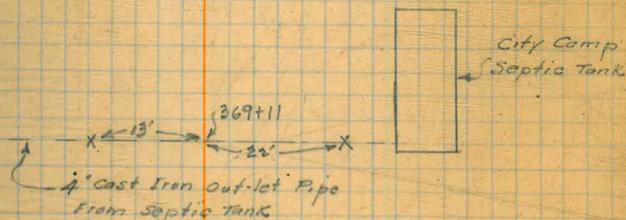


369+11 \pm Elev. 369+00 - ^{550.2}1² = Top of 4" cast Iron Pipe 22' Rht. of \pm Rd. Survey

" " " " - ^{548.8}2⁵ = " " " " " " on \pm " "

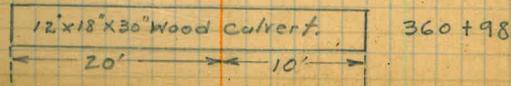
" " " " - ^{544.9}6⁵ = " " " " " " 13' Lf. \pm " "

371+82
3" Pipe Drain from water Main about 1⁵' under road surface (Not in use)



360+98 \pm Elev. 361+00 - ^{540.5}2² = Flow Line of Culvert 10' Rht. of \pm Rd. Survey

" " " " - ^{539.6}3¹ = " " " " " " 20' Lf. " " " "



± Main 7 Woodside to ± R.S. Div. 1 244.5

85.1 to B.C. of curve R. 100 Δ 39°30'15"
158.93 E.C. to B.C. " R. 47.16 Δ 37°00'
174.88 E.C. " " R. 250 Δ 35°00'
85.37 " " " R. $\frac{2}{150}$ Δ $41^{\circ}\frac{23'}{27}$ R
83.8 to N.P.L. Julien

30	220
239.5	130
<u>35</u>	90
304.5	25
60	115
<u>244.5</u>	244.5
	<u>359.5</u>

40'
45.1
85.1

S. 50°25'E. outside arc 126.59

S 9°00'E

41°23'

Survey of $\frac{1}{2}$ of Route 8 Div. 1

EC.

Δ 3700.2

R 971.16

T 187.68

BC.

E.C. 1851

EC.

Δ 3930.15

R 100.0

T 35.90

0485.1 BC.

0400

Hill
Soper
Remmen

10/4/35

50

EC. 220

25.7

Correc
Midpoint

225

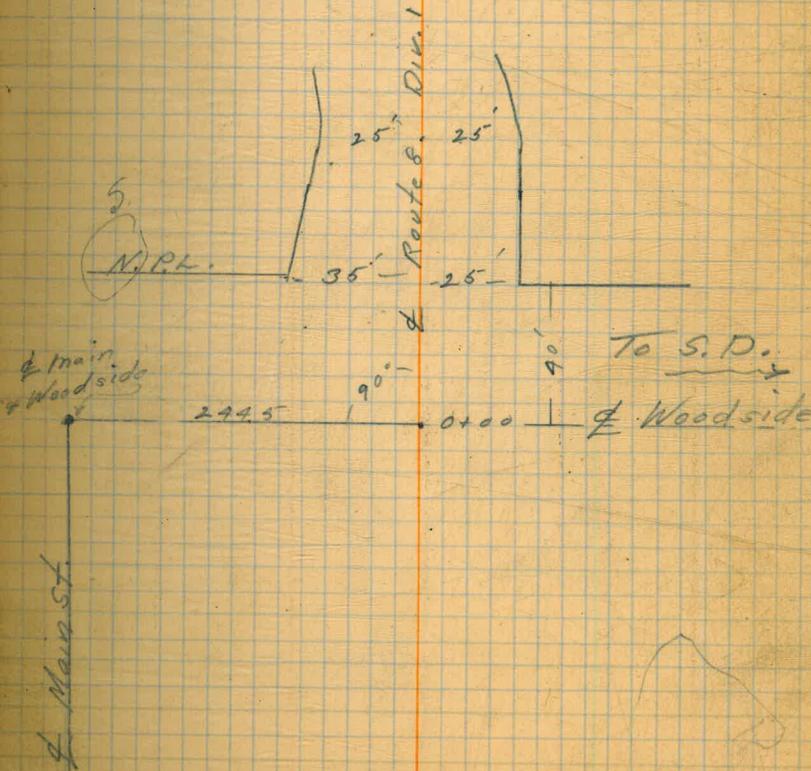
23.5

BC. old prop.
cor. 0

25

E.P.L. 4182305
E.P.L. 10 survey

Note 6" main 15' west
of E.P.L. of route 8



N. P. L. Julien

83.6

E.C.

Δ 11° 27' R
R 150.2
T 56.66

B.C.

88.37

E.C.

Δ 35° R
R 250
T 78.82

B.C.

171.88

E.C.

Note tie to Chestnut St. incomplete on available maps.



B.C.



Revision in pipe location from
Sta. 416+84.49.

436.65 11° 13 1/2' E.C.
 222 9° 16' +25 10° 56'
 150 5° 23' +75 7° 34'
 421 2° 31' +25 4° 12'
 420+82.71 B.C.

751.55 18° 30' E.C.
 750 16° 32' +75 18° 05'
 419 13° 25' +25 14° 59'
 750 10° 19' +75 11° 52'
 418 7° 12' +25 8° 45'
 750 4° 05' +75 5° 38'
 417 0° 58' +25 2° 31'
 416+84.19 B.C.

P.I. 421+50.84
 Δ 23° 27' R
 R 425.
 T 89.20
 L 173.94

P.I. 416+36.11
 Δ 36° 59' 30" R
 R 160.
 T 163.92
 L 297.06
 d' 3.737
 465 1° 33.417

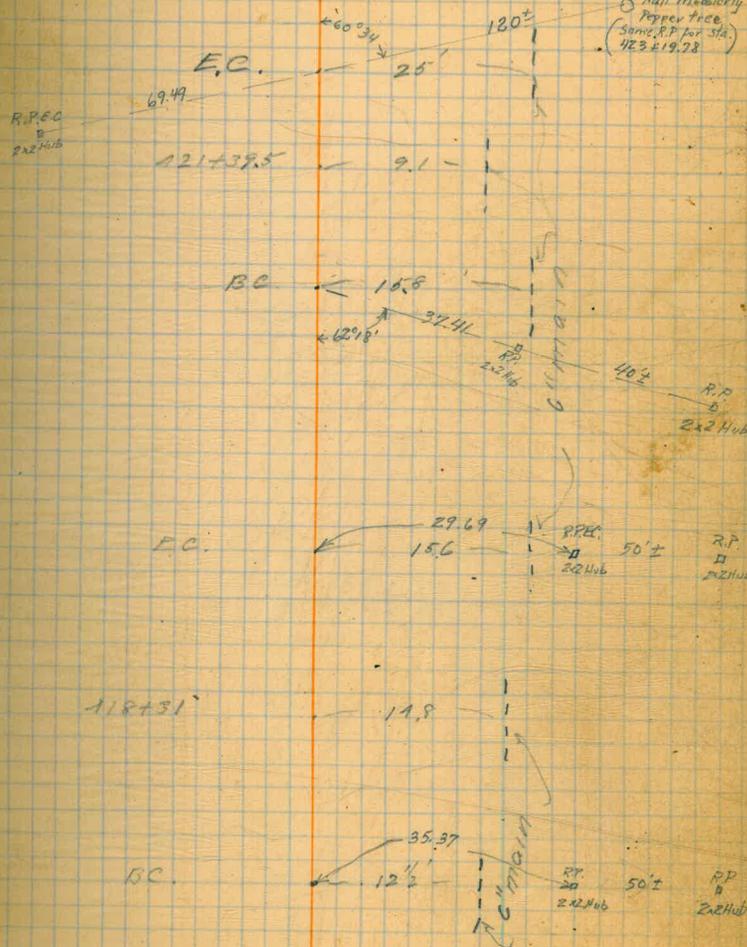
Hill
 Soper
 Remmen

10/9/35

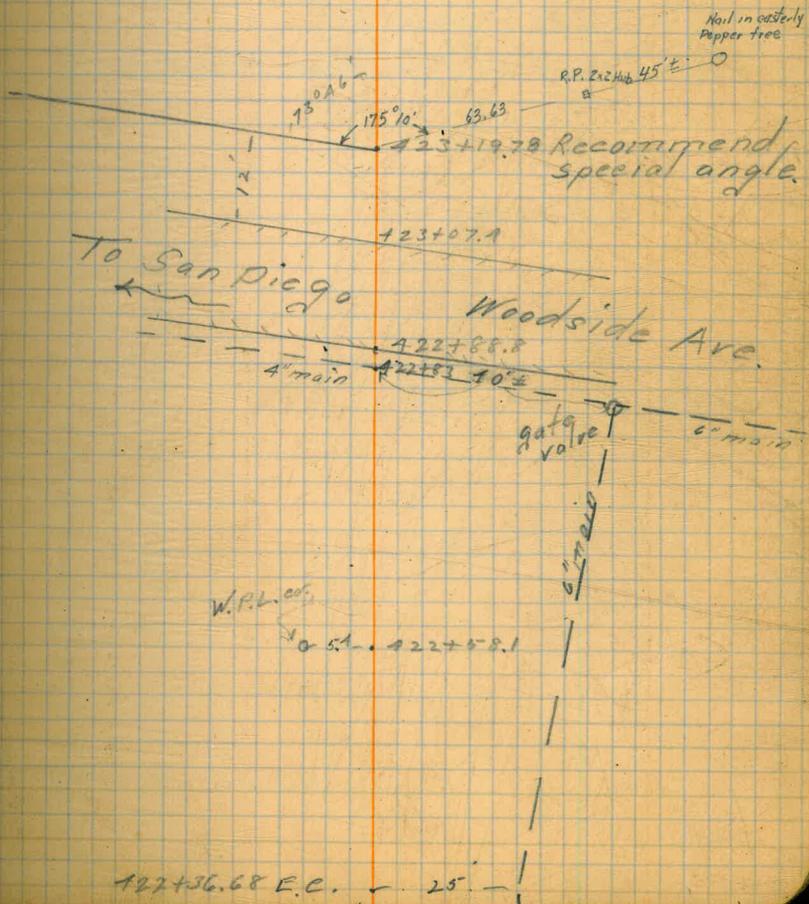
52

Note 6" main 15' west
 of E.P.L. Route 8 D.I.

Nail in Eastern
 Pepper tree
 (Same R.P. for Sta.
 423 & 19.78)



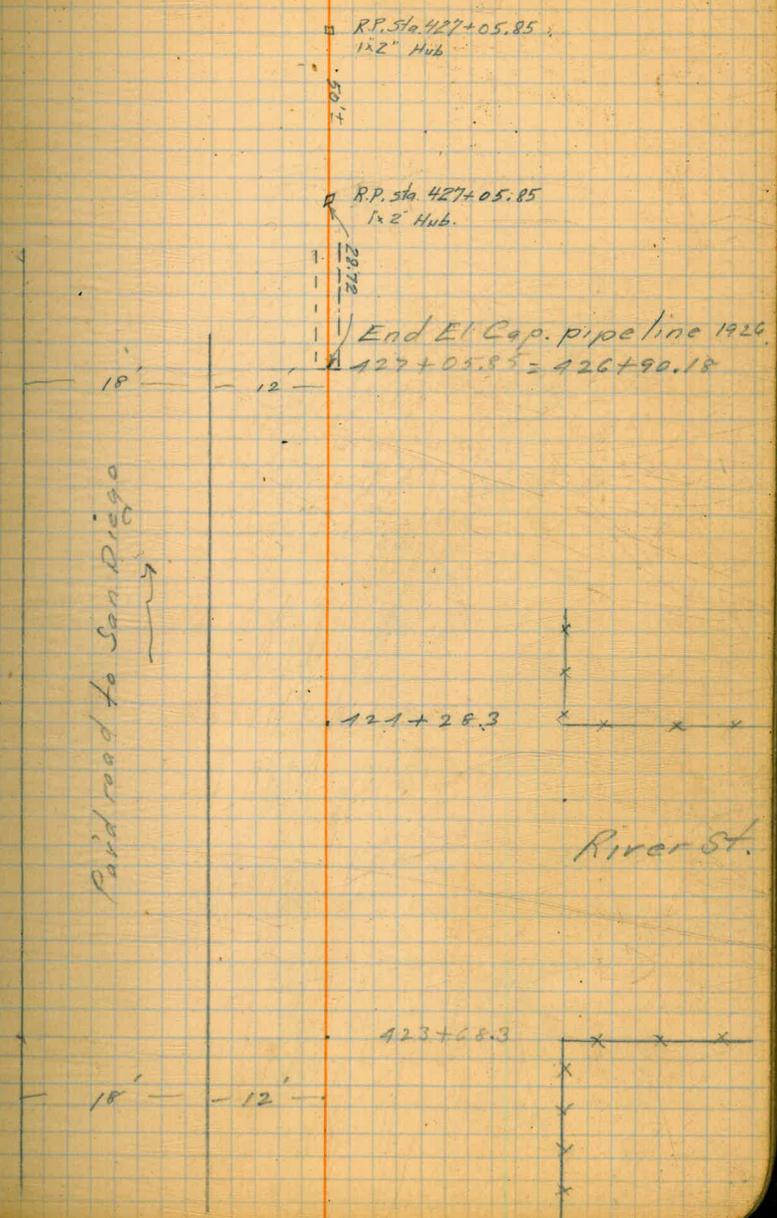
423+1978. 73°46' L



422+36.68 E.C.

422+36.68 E.C. 25°

418+00.00 Route thru park.
 =
 426+90.18 Before revision
 =
 427+05.85 End El Capitan Pipe Line



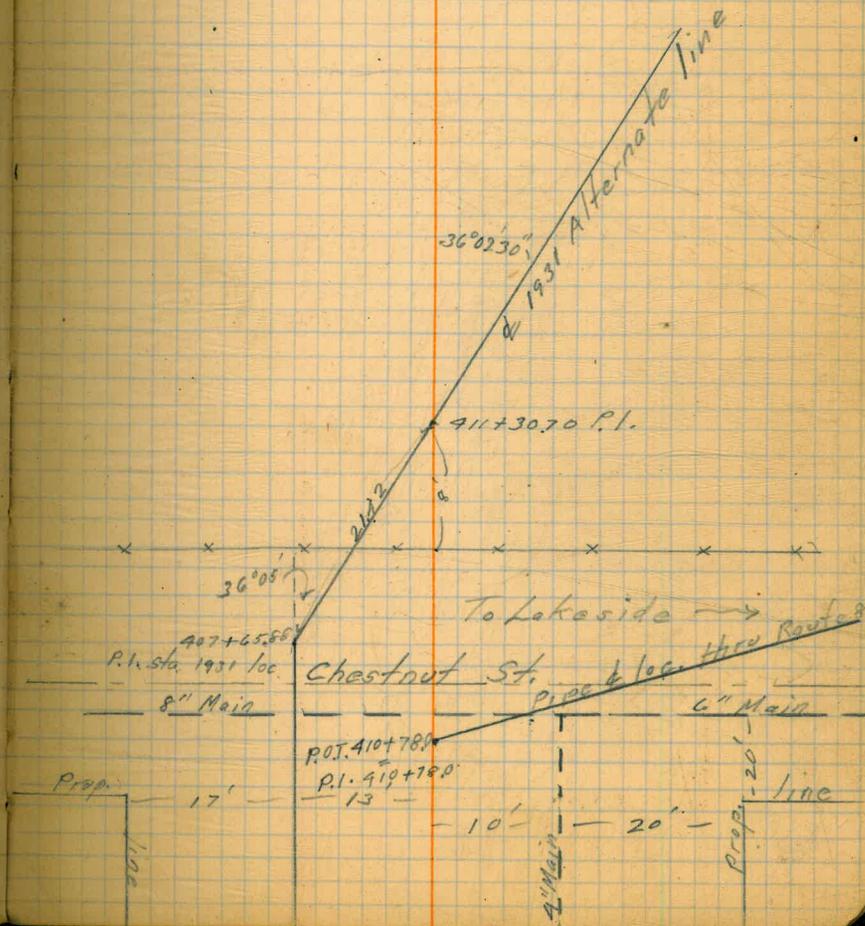
Tie to Alternate Line of
1931 Pipe Line Survey.

Hill
Sapor
Remmen

10/5/35

55

797.62	18°01'	EC.	P.I. 411+30.70
775	15°06'		Δ 36°02'30" R
750	11°50'		R. 220
725	8°35'		T. 71.57
411	5°20'		L. 138.39
775	2°04'		
410+59.13	BC.		



Line revision at Co. road & Elm St.

Line 13' N of E of Final Road location

351+52.00

351+41.80 27°29½' E.C.

351 26°17'

+50 24°50'

350 23°23'

+50 21°56'

349 20°28'

+50 19°01'

348 17°34'

+50 16°07'

347 14°40'

+50 13°13'

346 11°46'

+50 10°19'

345 8°52'

+50 7°25'

344 6°58'

+50 4°31'

343 3°04'

+50 1°36'

342 0°09'

341+94.64 B.C.

Hill
Saper
Remmen

10/10/35

56

Copied into Book # 501 page 34

1/4/36

P.I.

Δ 54°59' R

R 987

T 513.62

L 997.16

Blotted
Profile
m.

(cont. from page 56)
 Levels on Line 13' N of $\frac{1}{2}$ Road Location

B.M.	6.97	483.20	176.23
341+21.64		1.4	478.8 ✓
342+20		2.1	481.1 ✓
+50		2.3	480.9 ✓
343		4.8	478.1 ✓
+50		7.5	475.7 ✓
344		8.8	474.4 ✓
+50		9.6	473.6 ✓
345		8.7	474.5 ✓
+50		8.5	474.7 ✓
346		7.8	475.4 ✓
+50		7.4	475.8 ✓
347		7.1	476.1 ✓
+50		7.7	475.5 ✓
348		8.4	474.8 ✓
T.P.		8.20	475.00 ✓
	1.47	476.47	
+50		3.0	473.5 ✓
349		4.3	472.2 ✓
+50		5.7	470.8 ✓
+96		7.6	468.9 ✓
350		11.8	464.7 ✓
+50		12.7	463.8 ✓
351		14.6	461.9 ✓
+41.80		10.5	460.0 ✓
		12.7	463.8 ✓

57

Power pole Rt. of sta. 68+00 (Carried sta.)

Check on $\frac{1}{2}$ sta. course Co. road survey El. 463.7

*Checked by
 Prof. W.*

Line change near El Monte Park.

Sta. Detloc. Bearing

Curve Data

Cont'd on page 63

N. 17° 31' 20" E

+01.2212° 55' 45" E.C.

254

+50° 11' 28"

255

10° 22'

+50° 8' 36"

254

7° 10'

+50° 5' 44"

253

40° 18'

+50° 2° 52'

252

1° 26'

251 + 49.91 B.C.

N. 43° 22' 50" E

Hill
Soper
Remmen

11/26/35 clear.

58

265+12 22.5 @ 4' oak

3 1/2 oak
26 - 264+80

264+55 21.5 @ 2 1/2' oak

264+43 21 @ 4' oak

264+15 18 @ clump 3 oaks
about 20' dia.



P.I. 253+79.47

Δ 25° 51' 30"

R. 1000.

T. 229.56

L. 451.31

271+17.52 P.O.T.

Void - see page 63

+39.79 1°24' EC.

266 0°59'

+50 0°30'

265 0°01½'

264+97.11 B.C.

A 2°43.36R

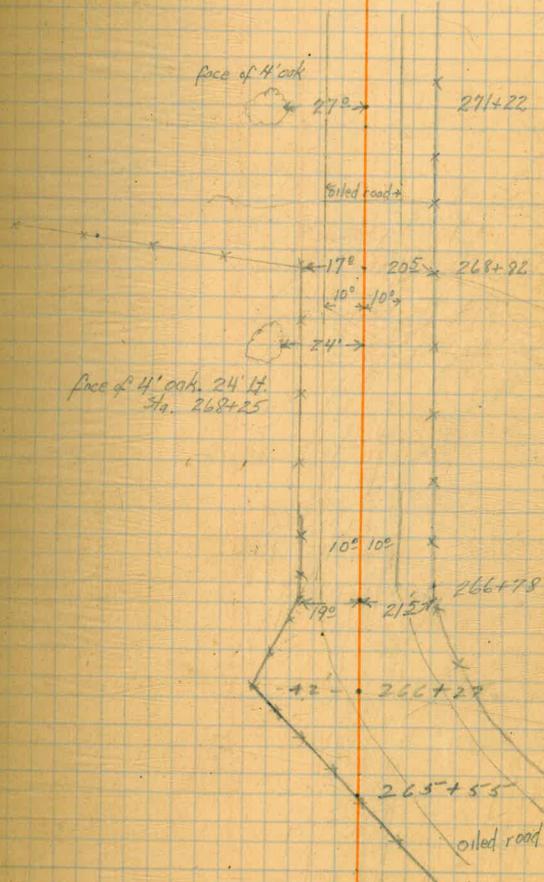
P.I. 265+68.45

R. 3000.

T 71.37

L. 142.68

59



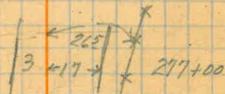
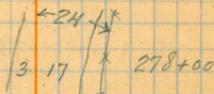
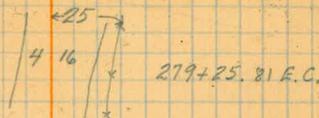
279+68.09
276+76.72

+25.81	29° 53' E.C.
279	58° 41'
+50	76° 23'
278	24° 04'
+50	21° 46'
277	19° 27'
+50	17° 08'
276	14° 50'
+50	12° 31'
275	10° 12'
+50	7° 54'
274	5° 35'
+50	3° 17'
273	0° 58'
272+79.07	B.C.

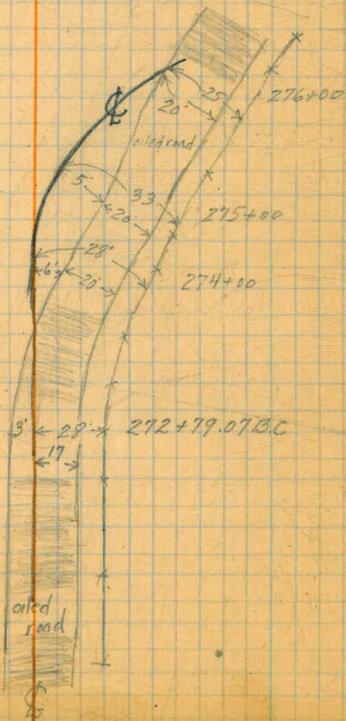
Void see page 63

P.I. 276+35.33
Δ 59° 46'
R 620
T 356.28
K 646.74

⊕



⊕



Revision of Pipe Line Alignment, at Pumping Plant
Elevations and Sta. of crosspipes Book 509 page 76

Copied into

Book 500 page 36

316+00 P.O.T
316+05.13 P.I

314+04.76 P.I. $3^{\circ} 02' 30''$ Lt.

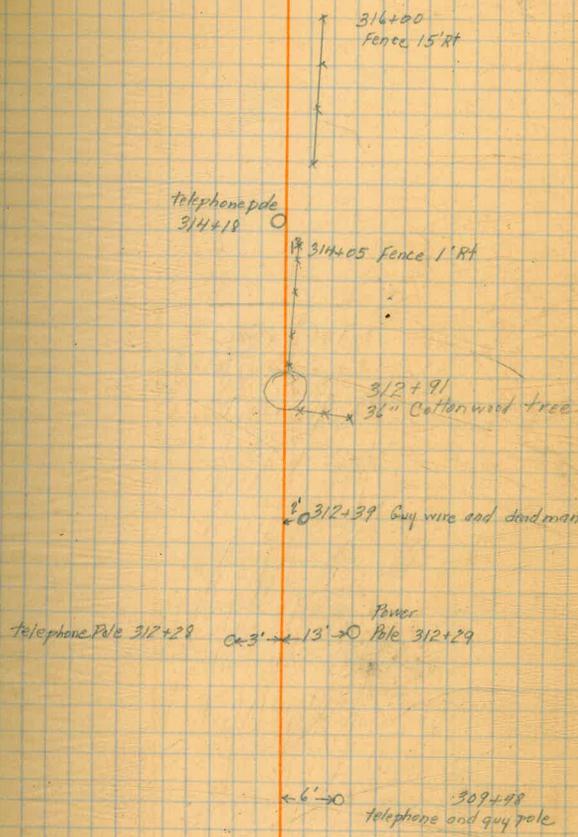
$S 47^{\circ} 57' 30''$ W.

EC. +77.96 $17^{\circ} 32'$
+50 $15^{\circ} 32'$
311 $11^{\circ} 57'$
+50 $8^{\circ} 22'$
310 $4^{\circ} 47'$
+50 $1^{\circ} 13'$

$\Delta = 35^{\circ} 04' 30''$ Lt.
 $R = 400'$
 $T = 126.41$
 $L = 244.87$
P.I. = 310+59.50

BC 307+33.09

$S 83^{\circ} 02''$ W



Road
E

8' x 6' Cattle pass under road at Foster Prop.

237+82
Pipeline Sta.Road sta.
173+34
Concrete walls237+90
Pipeline Sta.

1/2:1 Slope

17'

173+26
Road Sta.

17'

1/2:1 Slope

237
237+50Elevation
469.3
468.2

238+00

467.8

238+30

467.4

Co. Road Line Revision at El Monte Park

Jan 8 1936

Hill
Soper
Remmen

63

268+25.70 P.O.T

N 20°38'20"E

265+78.90 E.C. 1°33'30"

Δ 3°07'RT

R. 3000'

+50 1°17'

T 81.60

L 163.19

265 0°48'

d1 00.57295

d50 28.6475

+50 0°20'

P.I. 264+97.11

264+15.51 B.C.

N 17°31'20"E

Cont'd from page 58

Cont'd on page 27

279+08.09 ahead

279+23.63 Back

279+21.56 EC 29° 40' 45"

279 28° 39'

+50 26° 16'

278 23° 53'

+50 21° 29'

277 19° 06'

+50 16° 43'

276 14° 20'

+50 11° 56'

275 9° 33'

+50 7° 10'

274 4° 47'

273+50 2° 23'

272+99.96 B.C.

Δ 59° 21' 30" RT

R. 600'

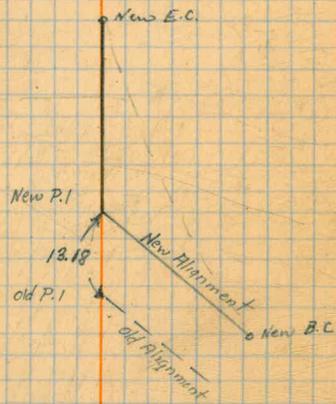
T. 341.94

L. 621.60

di 2.865

ds 2° 23' 239

P.I. 276+41.90



Road location - Alternate Line #2

Copied from J.W. Williams's loose-leaf book. Nov. 27, 1934
 HFS
 This line change accepted by County.

102+21.27 EC

100+88.20 P.I.

99+45.79 BC

$$\Delta = 35^{\circ} 04' 30'' \text{ R}$$

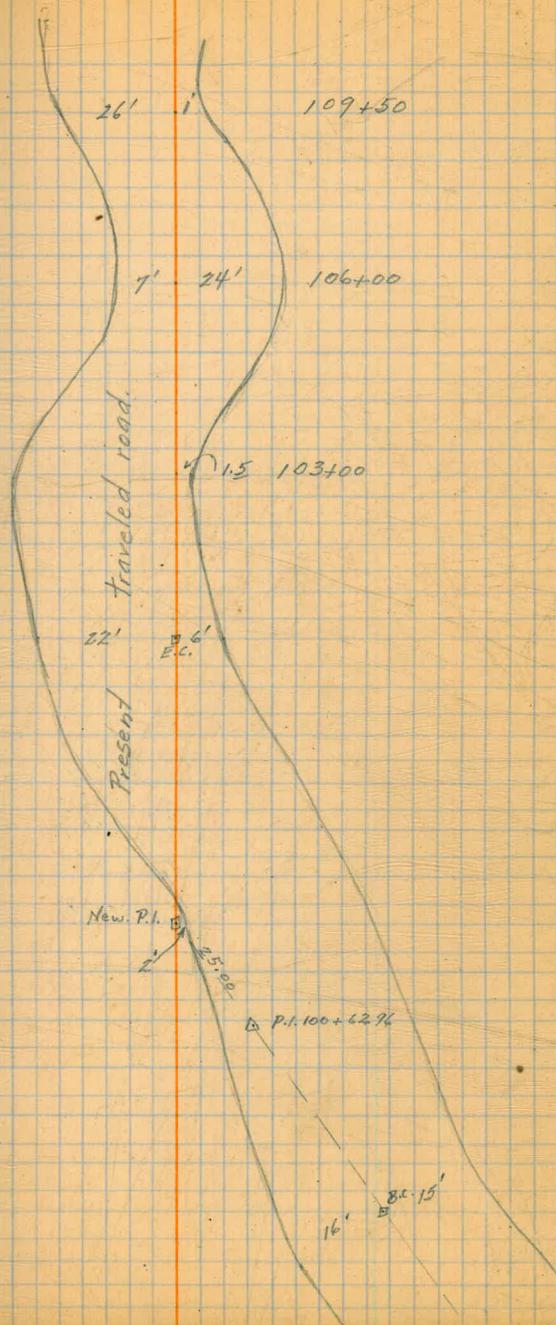
$$R = 450'$$

$$T = 142.21$$

$$L = 275.48$$

May 1, 1935
 Hill - Simpson
 Super - Remmen

65



Cont'd. on page 19

124+72.44 E.C.
=
125+28.78 P.O.T.

123+04.36 E.C.

119+15.26 P.I.

$\Delta = 42^\circ 36' 45''$ L.A.
 $R = 1100'$
 $T = 429.00$
 $L = 818.10$

114+86.26 B.C.

E.C. on original location
124+72.44 E.C.
=
125+28.78 P.O.T.

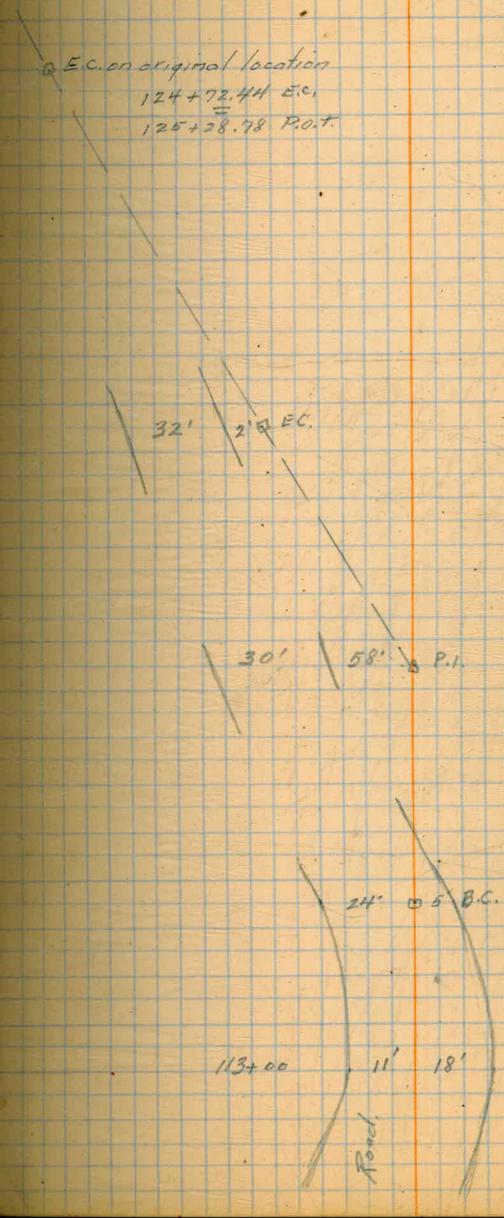
32' 2' E.C.

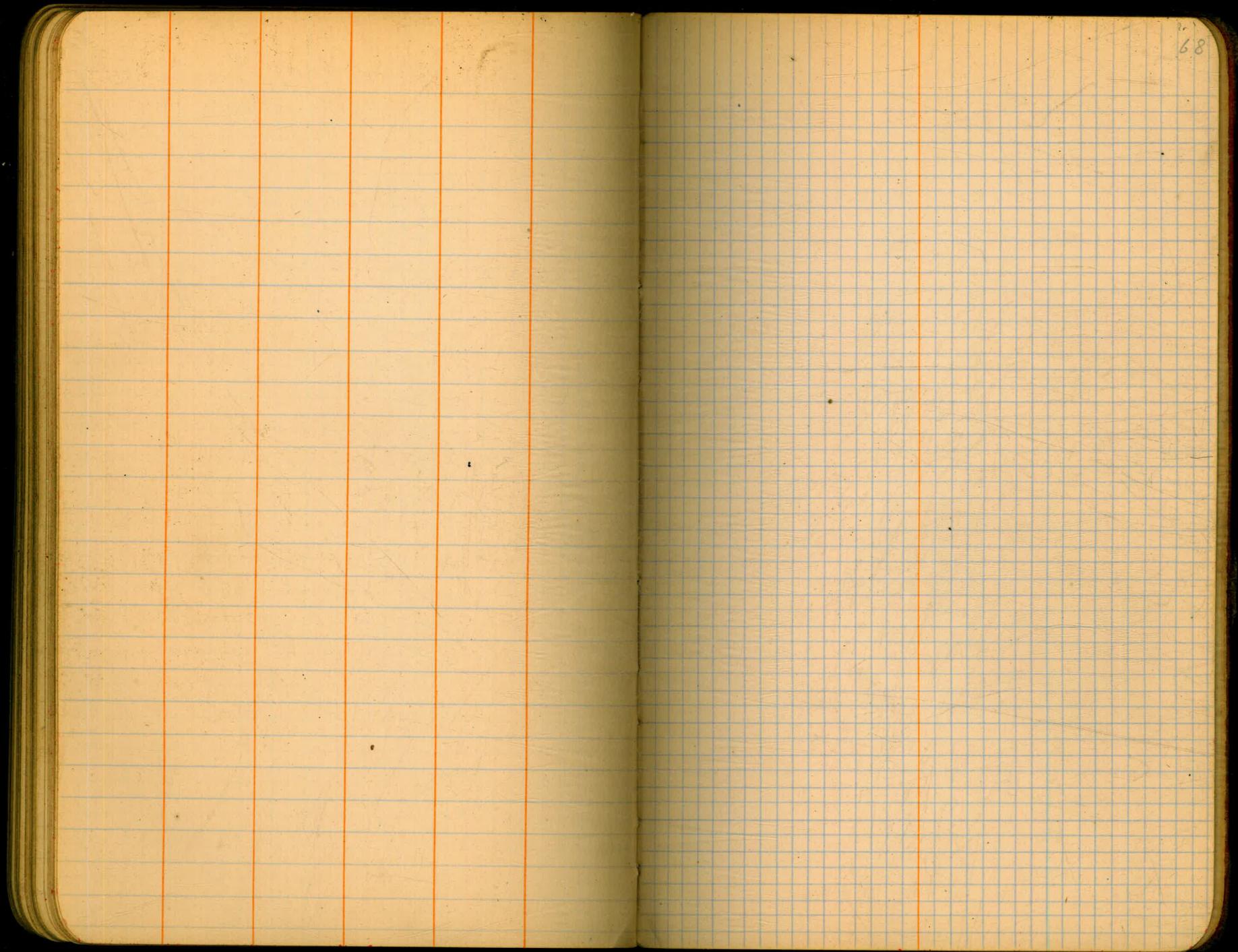
30' 58' P.I.

24' 5' B.C.

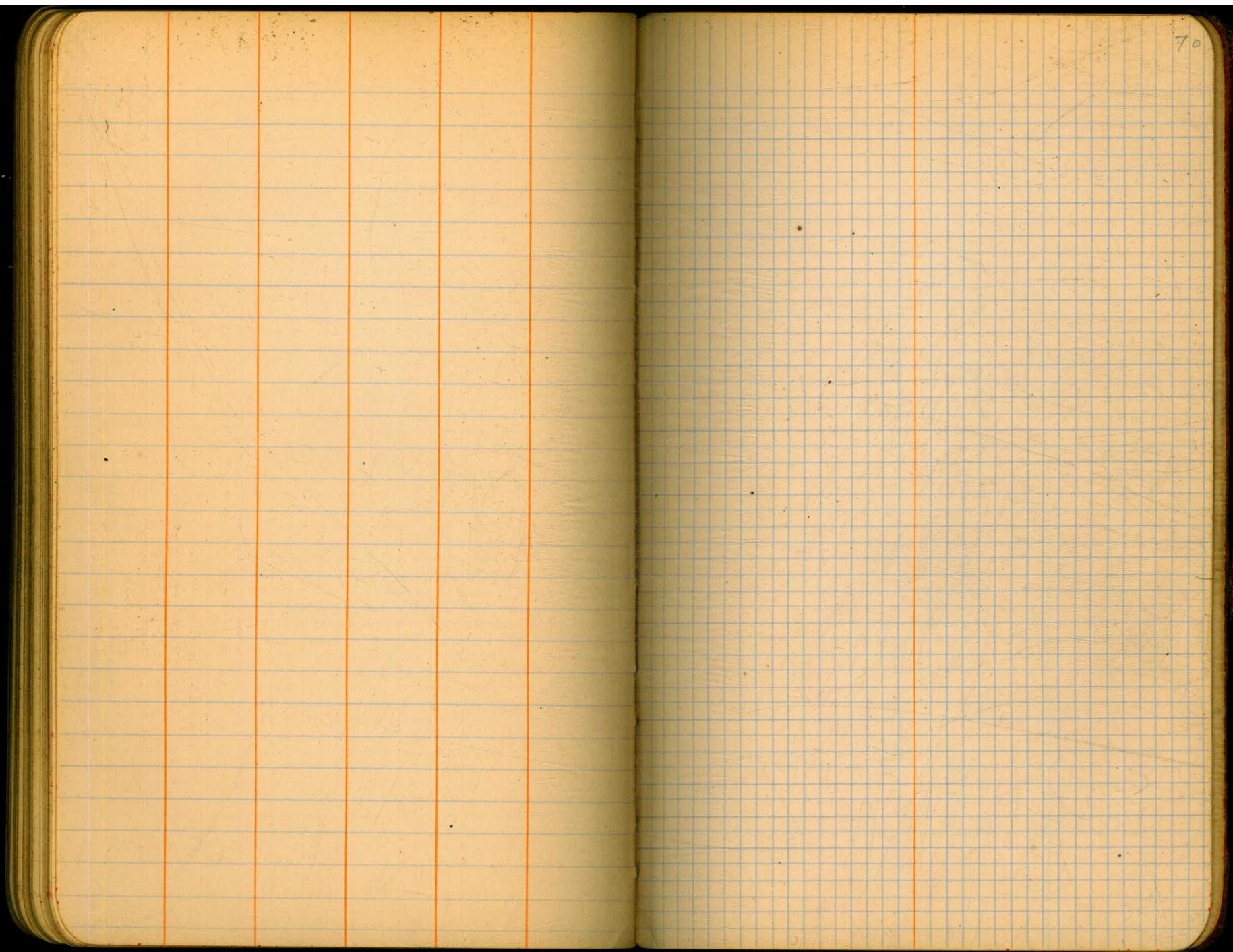
113+00 11' 18'

Road





68



684.60 from 8+15.6 = 0+00

0-2.35 face of plug

0+00 N. 36" pipe face of flange

0+00.12 S " " " "

Width of 36" pipe 3.86

0.75 bet. flanges 36"

0.86 " " 36" + 48"

4.11 dia. 48"

0.50 bet. 48"

317.48 hub at portal to 8+17.15

2.50

2.38

0.12

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in the column and top row. The number in body of table in same row and column gives distance level estimate the difference in elevation between the side stake and the lower target by this amount if cut, elevate if fill. Add this amount to cut or fill at side stake. If it does not make the right adjustment target.

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find T tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

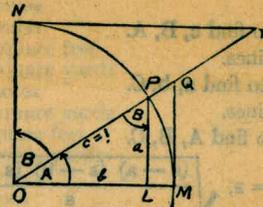


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

220
19.28
36.22

5-96
8860
684460

8+156 8
6846
1+31.0

8+17.15
6846
2.15

8+176
6846
1+330
23

8+17.15
6846
132.50

16.84
15.29
1.554

20462.71
19481.55
11.19

30.29
17.29
30

19.8
48.5
68.3

0.50
32.83
8+17.17

4+20.59
1+33.35
287.24

8+17.15
1+33.35
6+83.80
347.98

10+31.28
215.76
1247.03

21035
4370

308.2930
1.2123
30950.53

239.5
35.0
274.5

6
239.5
30
209.5
30.0
239.5

271.22

27.46

38.20